

# Transmitter Pre-Compensation for 320 MB/sec SCSI

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- Look at two forms of transmitter pre-compensation that might be used for 320 MB/sec SCSI
  - Mathematically model timing pre-compensation
    - How does timing pre-compensation help:
      - Isolated pulses
      - High frequency patterns (0, 1, 0, 1, etc.)
  - Use experimental data to examine amplitude pre-compensation using real cables with real loads.
    - How much does amplitude pre-comp improve signal integrity?
    - How much amplitude pre-comp is required for:
      - short cables?
      - long cables?
    - Determine the optimum value for amplitude pre-comp

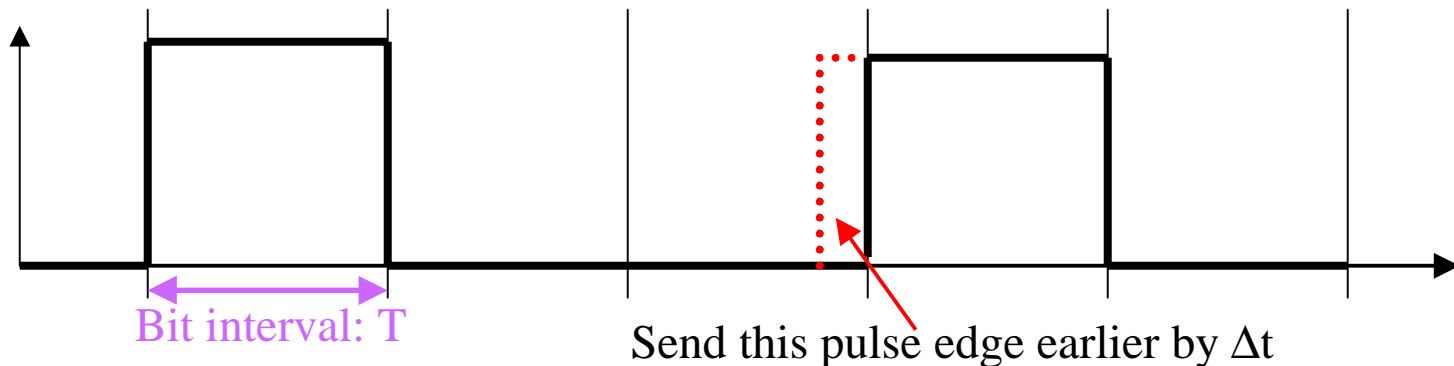
# Transmitter Pre-Compensation for 320 MB/sec SCSI

## Part I Timing Pre-Compensation Study

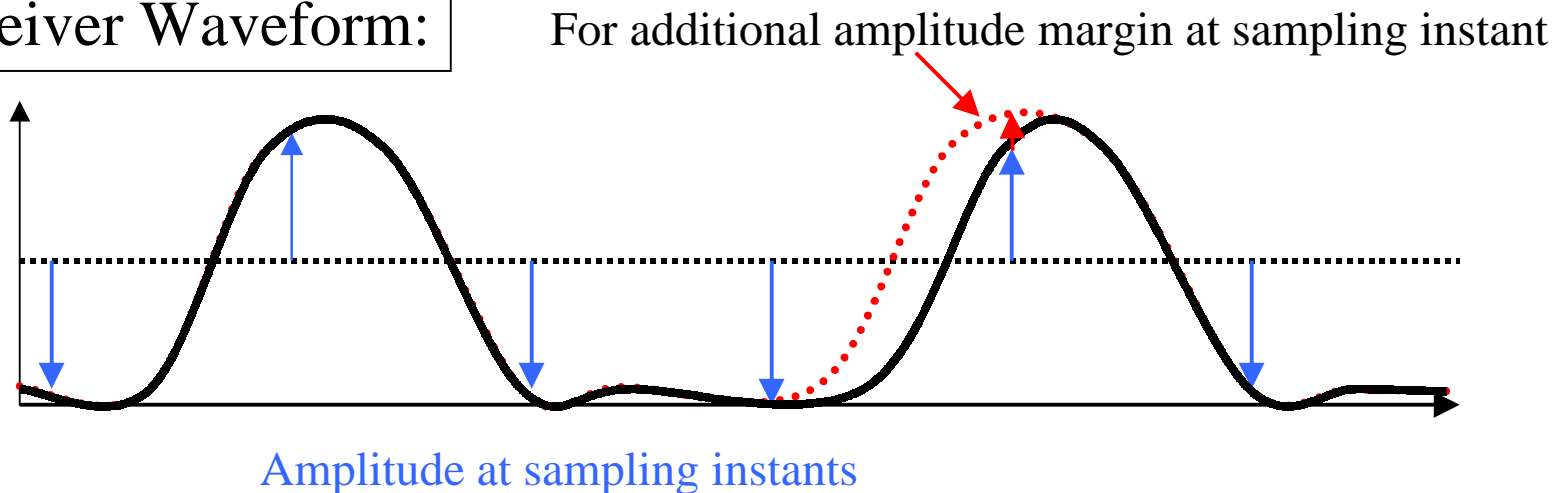
- All data collected in this section of the presentation is based on a simple *optimistic* model for SCSI signals.
- Real factors such as DC attenuation, reflections, offsets, frequency dependent skew, differential skew, etc. will degrade performance even more than suggested.
- This simple model is used to facilitate the analysis and to gain some insight into what can be expected in actual practice.

- Adjust the timing of pulse edges to improve receiver amplitude noise margin and set-up time.
- If the pulse is sent earlier, then response will rise further past the threshold.
- If the pulse is earlier, there is more set-up time, and less hold time for the previous bit.
- Timing pre-comp has largest effect for an isolated pulse.
- Timing pre-comp has *no effect* for high-frequency patterns ( 0, 1, 0, 1, etc.).

## Simplified Transmitter Waveform:



## Receiver Waveform:



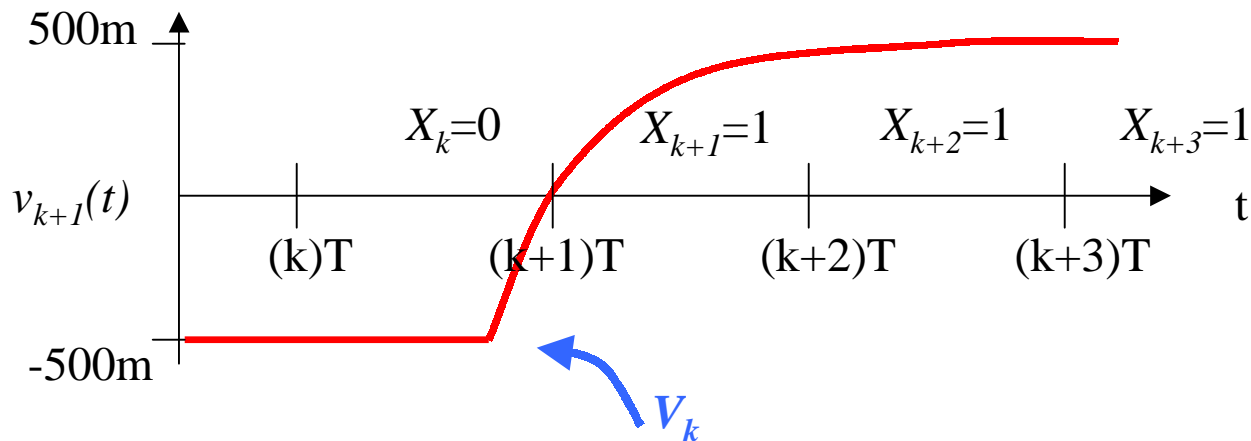
- Assuming a first order model for cable the received waveform during bit interval  $(k+1)$  can be expressed as:

$$v_{k+1}(t) + 500mV = \begin{cases} X_{k+1} = 0 & V_k \exp(-t / \tau) \\ X_{k+1} = 1 & 1000mV - (1000mV - V_k) \exp(-t / \tau) \end{cases}$$

- Where:

- $X_{k+1}$ : is the bit sent during interval  $(k+1)$
  - $V_k$ : is the amplitude at the end of bit interval  $(k)$
  - $\tau$ : is the dominant first-order time constant of the cable
  - $v_{k+1}(t)$ : is receiver waveform during bit interval  $(k+1)$
- This model assumes a zero-delay, just a first-order amplitude roll-off with frequency and normalized peak-to-peak amplitude of 1000mV

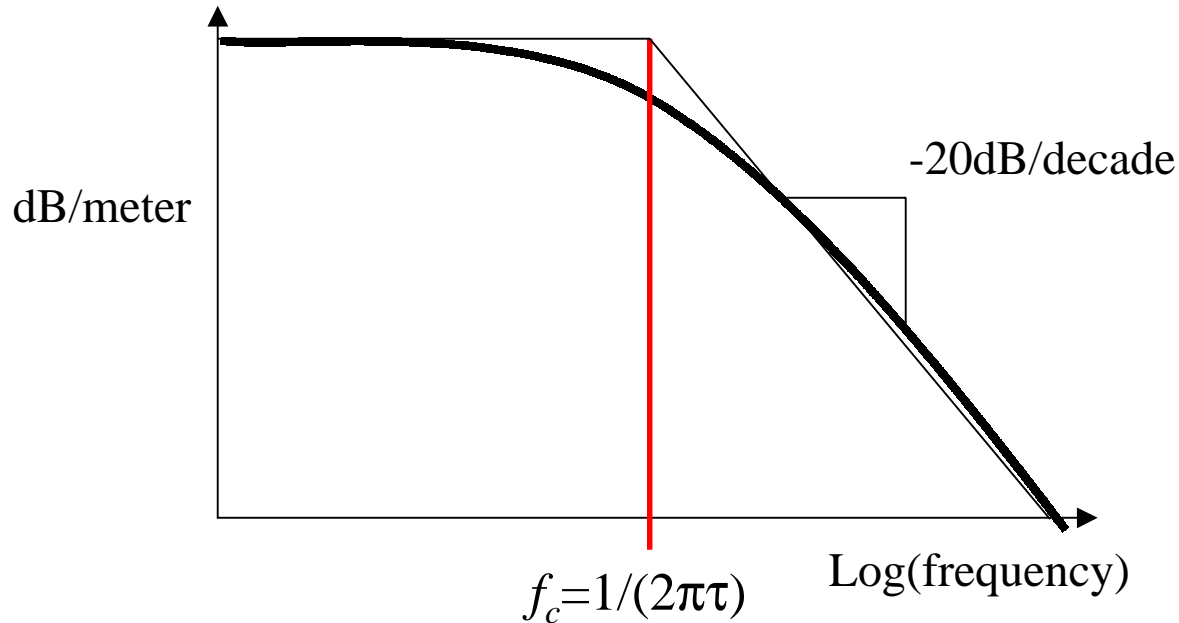
$$v_{k+1}(t) + 500mV = \begin{cases} X_{k+1} = 0 & V_k \exp(-t/\tau) \\ X_{k+1} = 1 & 1000mV - (1000mV - V_k) \exp(-t/\tau) \end{cases}$$



- This assumes several optimistic scenarios:
  - input is an ideal square wave
  - no frequency dependent time skew in cable
  - Output has a voltage swing of 1V (no attenuation in the cable)



- First order cable model:
  - attenuation versus frequency
  - characterized by a single pole roll-off



- Receiver input is sample of waveform at the sampling instant ( $T_{sample}$ )
- Sampling instant defined by position of zero crossings for high frequency pattern (de-skew).

$$v_{k+1}(T_{sample}) + 500mV = \begin{cases} X_{k+1} = 0 & V_k \exp(-T_{sample} / 2\tau) \\ X_{k+1} = 1 & 1000mV - (1000mV - V_k) \exp(-T_{sample} / 2\tau) \end{cases}$$

- For worst case (isolated bit) we have:

$$X_{k-N}, \dots, X_k = 0, X_{k+1} = 1, X_{k+2} = 0 \therefore V_k = 0.$$

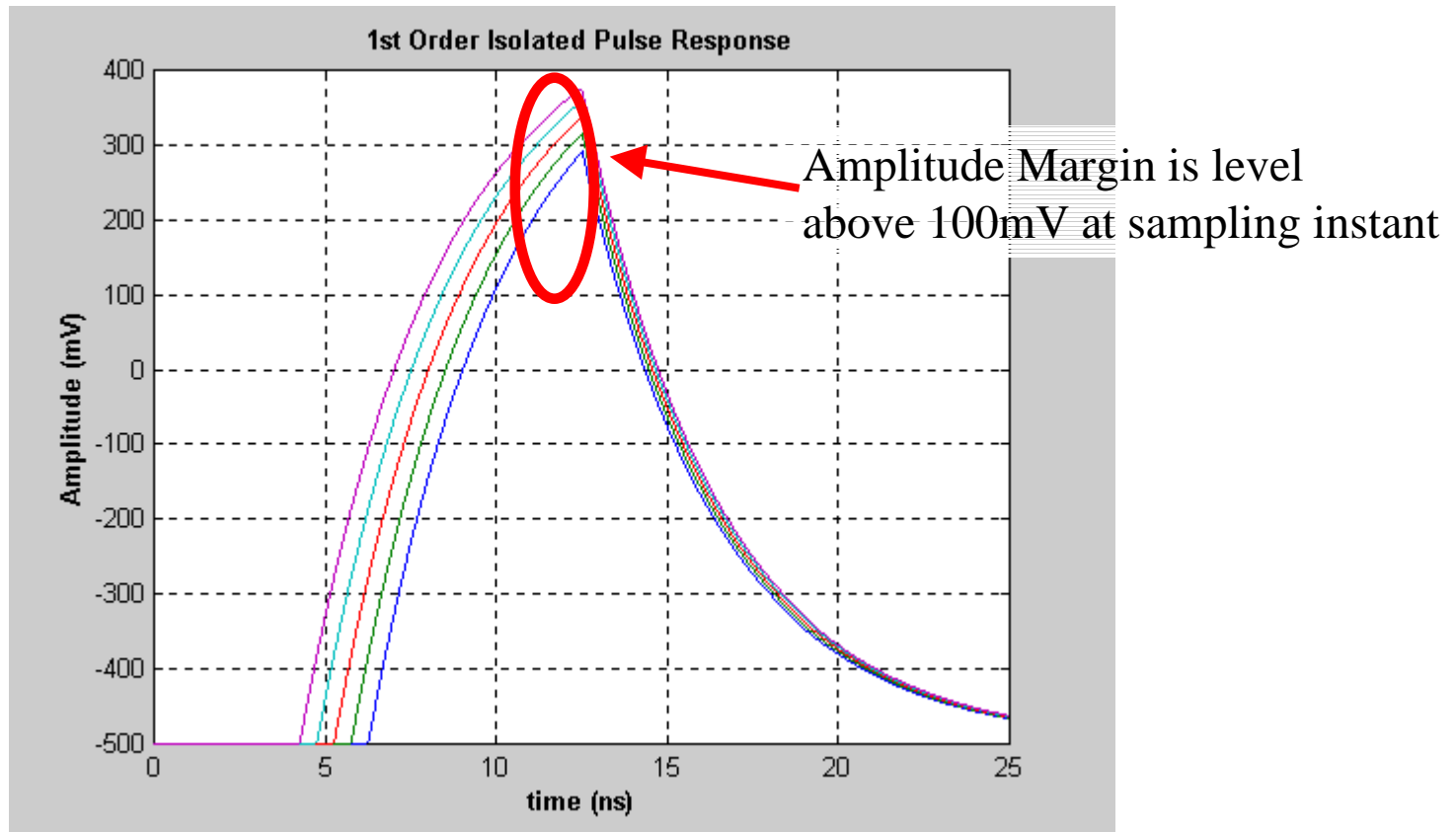
- Without pre-compensation the amplitude is:

$$v_{k+1}(T_{sample}) = (1000mV - 1000mV \exp(-T_{sample} / 2\tau)) - 500mV$$

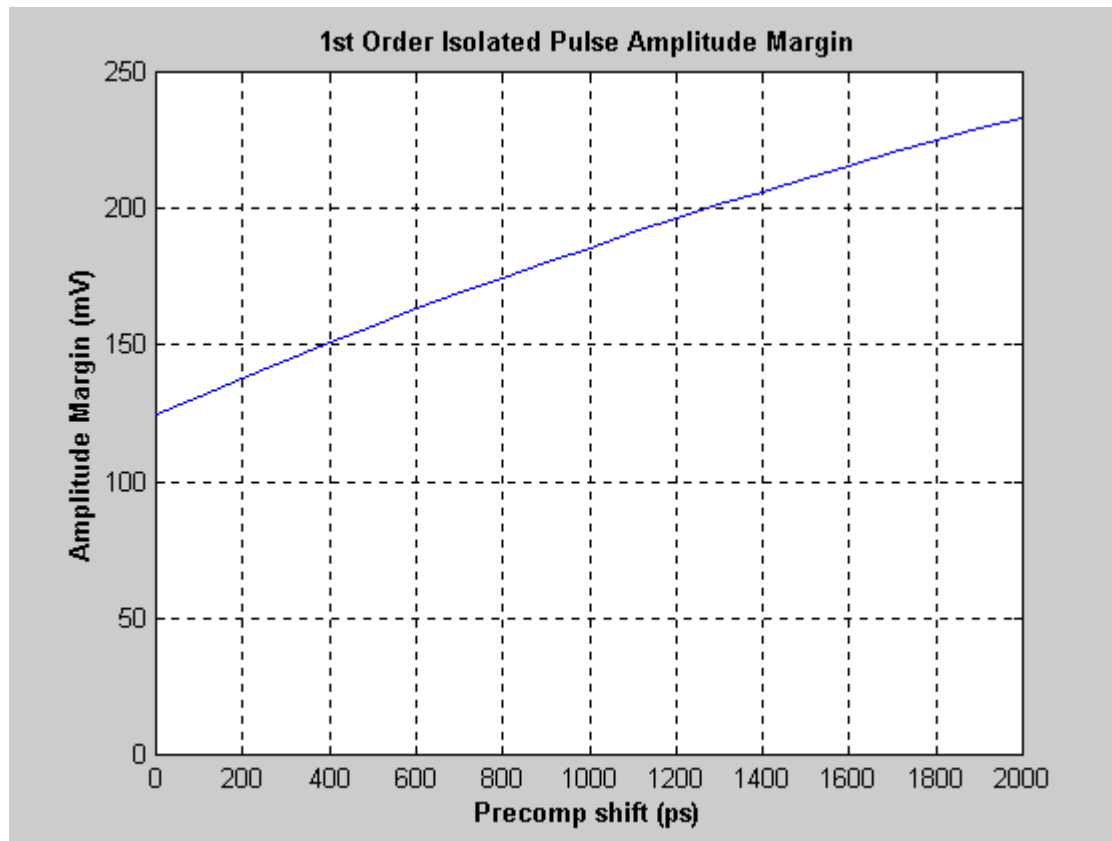
- With timing pre-comp shift ( $\Delta t$ ) the amplitude is:

$$v_{k+1}(T_{sample}) = (1000mV - 1000mV \exp(-(T_{sample} + \Delta t) / \tau)) - 500mV$$

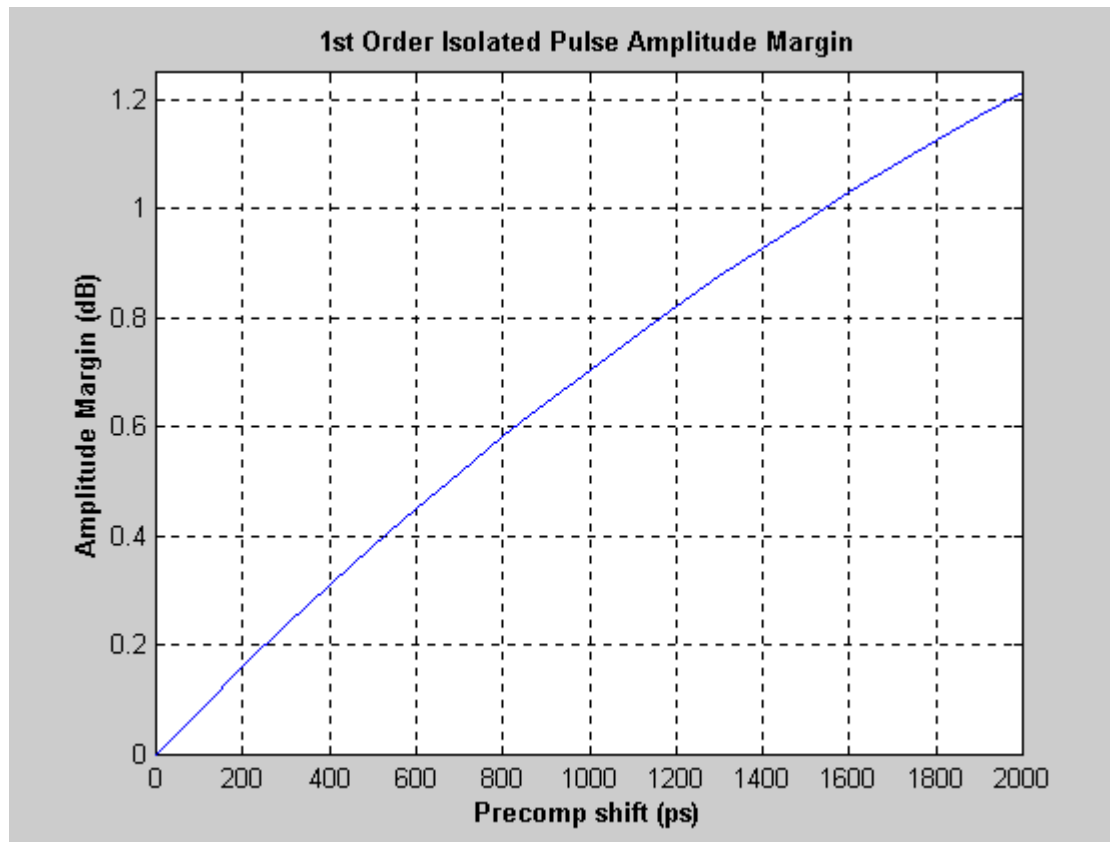
- Numerical calculations for isolated pulse:
  - $\tau \approx 1 / (2 \pi 40 \text{ MHz})$ ,  $\Delta t = 0\text{ps} \rightarrow 2\text{ns}$  by  $500\text{ps}$



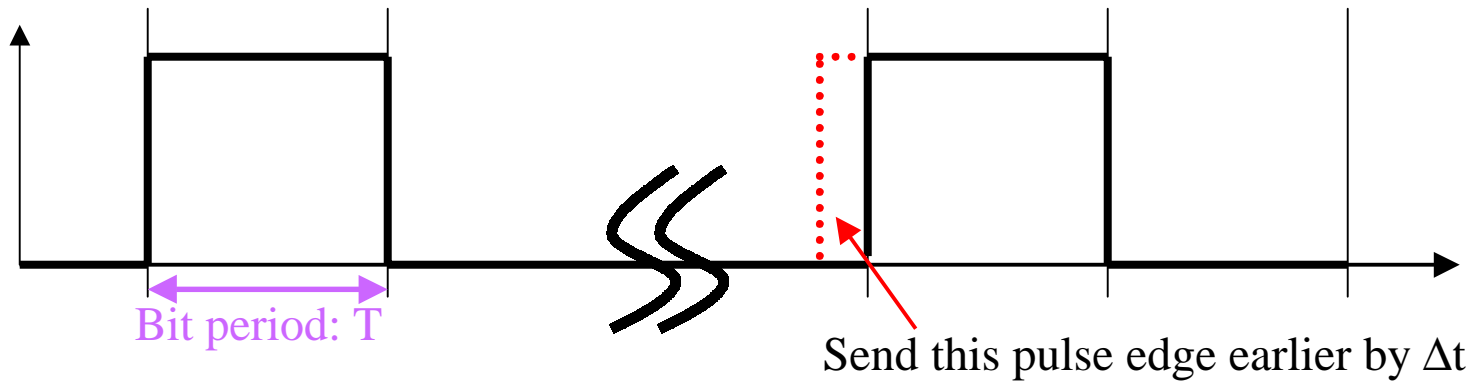
- Amplitude margin vs. timing pre-comp shift ( $\Delta t$ ) for  $f_c = 40\text{MHz}$ :



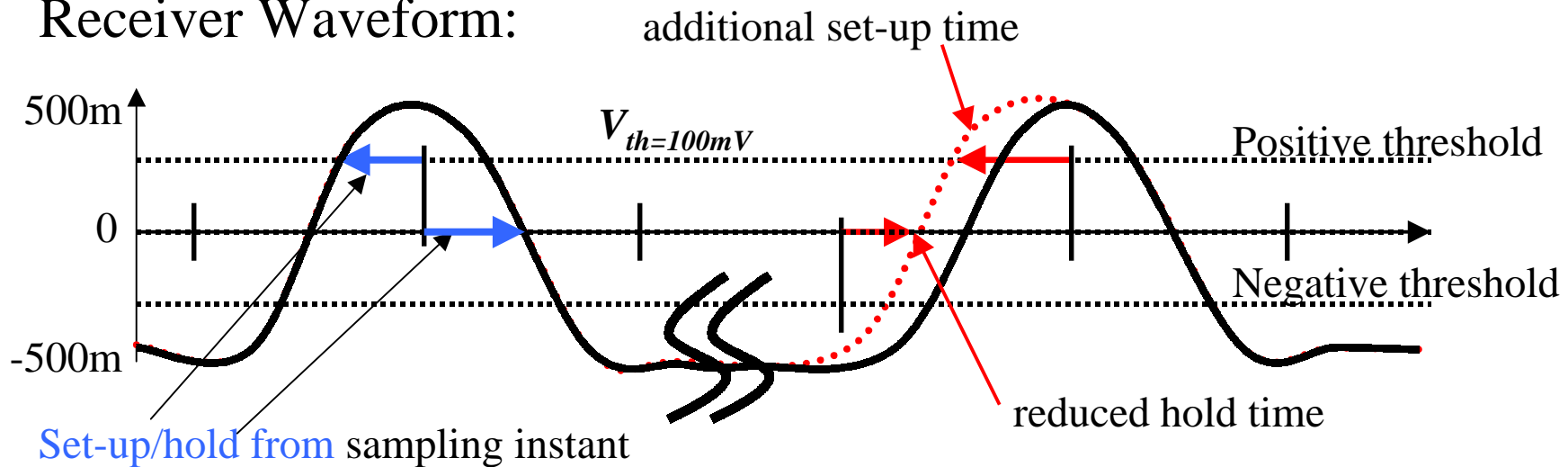
- Improvement in amplitude margin with timing pre-comp shift  $\Delta t$  for  $f_c = 40$  MHz:



Transmitter Waveform:



Receiver Waveform:



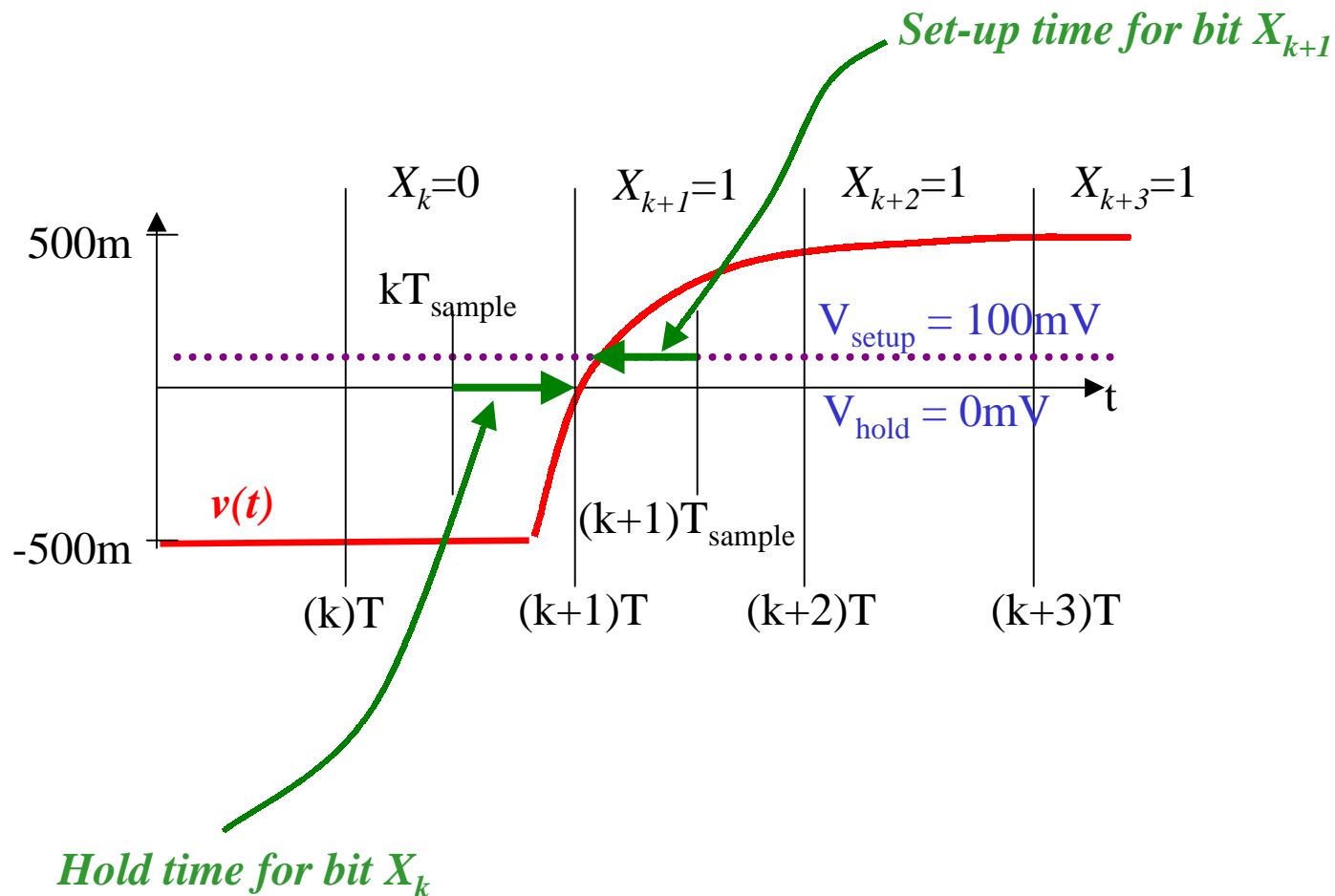
- Time before sampling instant ( $T_{sample}$ ) that waveform passes positive threshold ( $V_{setup}$ )

$$t_{su}(V_{setup}) = T_{sample} + \Delta t + \tau \ln\left(\frac{500mV - V_{setup}}{1000mV}\right)$$

- Set-up time for current bit linearly increases with pre-comp shift ( $\Delta t$ )
- Hold time for previous bit linearly decreases with pre-comp shift ( $\Delta t$ )

$$t_h(V_{hold}) = T_{sample} - \Delta t - \tau \ln\left(\frac{500mV - V_{hold}}{1000mV}\right)$$

- Isolated bit set-up/hold times calculated assuming that the starting voltage  $V_k = 0$  (ISI voltage)

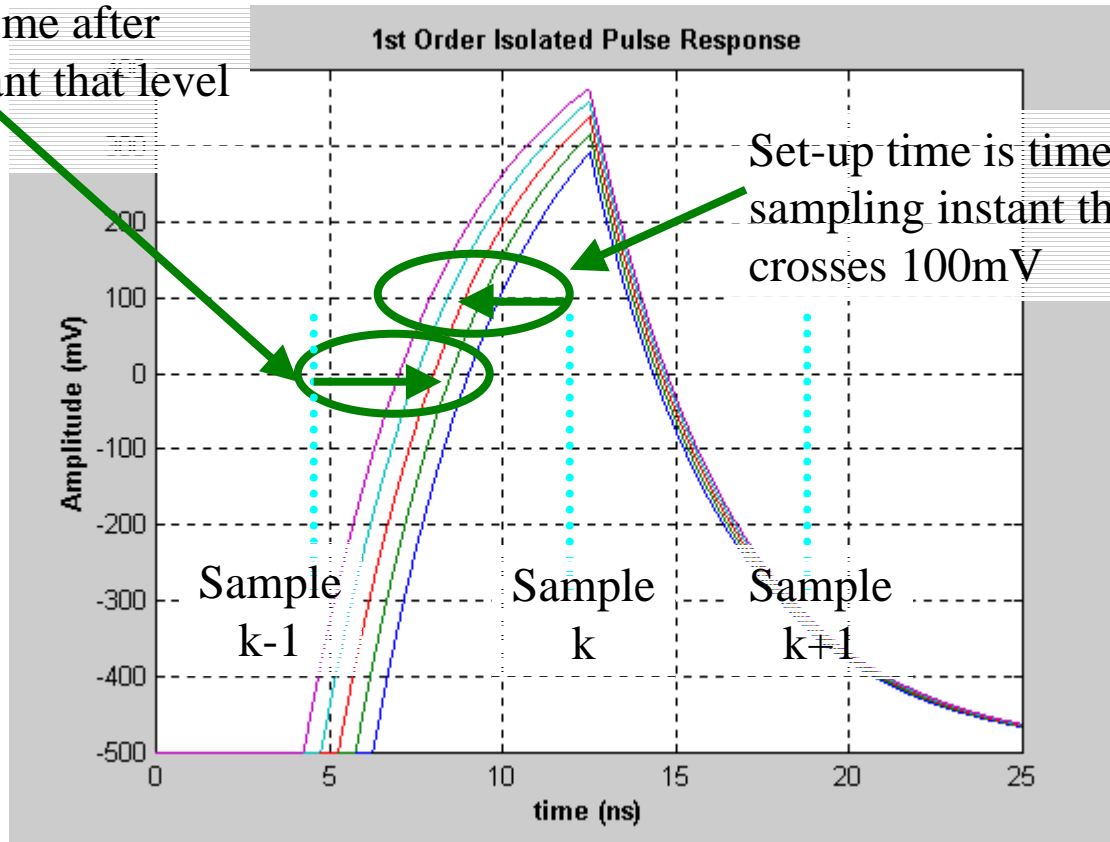




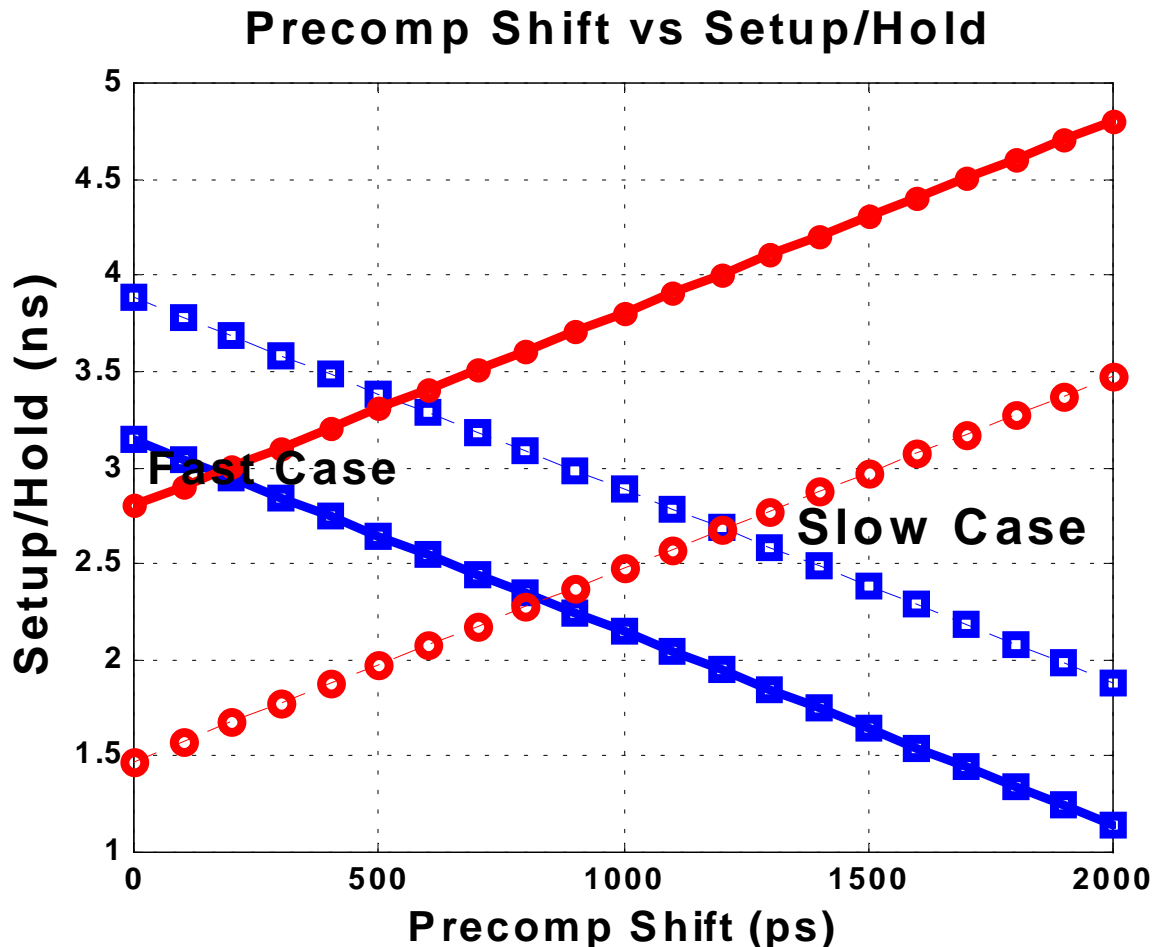
- Numerical calculations for isolated pulse:

$$\tau \approx 1 / (2 \pi 40 \text{ MHz}), \Delta t = 0ps \rightarrow 2ns \text{ by } 500ps$$

Hold time is time after sampling instant that level crosses 0mV



- Numerical calculations for isolated pulse:
  - slow case cable:  $\tau \approx 1 / (2 \pi 40 \text{ MHz})$ ,  $\Delta t = 0 \text{ ps} \rightarrow 2 \text{ ns}$  by 100ps (dashed)
  - fast case cable:  $\tau \approx 1 / (2 \pi 120 \text{ MHz})$ ,  $\Delta t = 0 \text{ ps} \rightarrow 2 \text{ ns}$  by 100ps (solid)

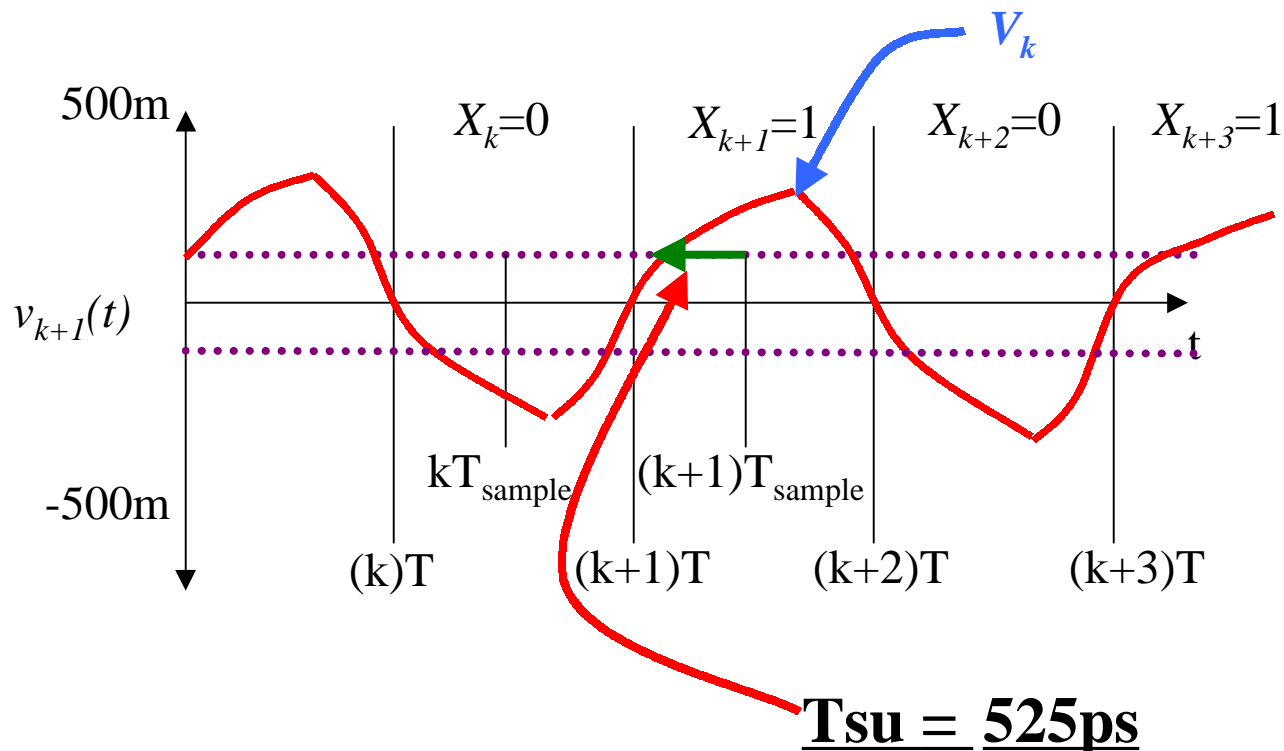


- For the high-frequency pattern, shifting each edge by  $\Delta t$  is the same as no pre-comp; all edges move over by the same amount (i.e., timing pre-comp just defeats de-skew)
- What is the set-up/hold time for the high frequency pattern.
- The first-order waveform equation in bit interval  $(k+1)$ :

$$v_{k+1}(t) + 500mV = \begin{cases} X_{k+1} = 0 & V_k \exp(-t / 2\tau) \\ X_{k+1} = 1 & 1000mV - (1000mV - V_k) \exp(-t / 2\tau) \end{cases}$$

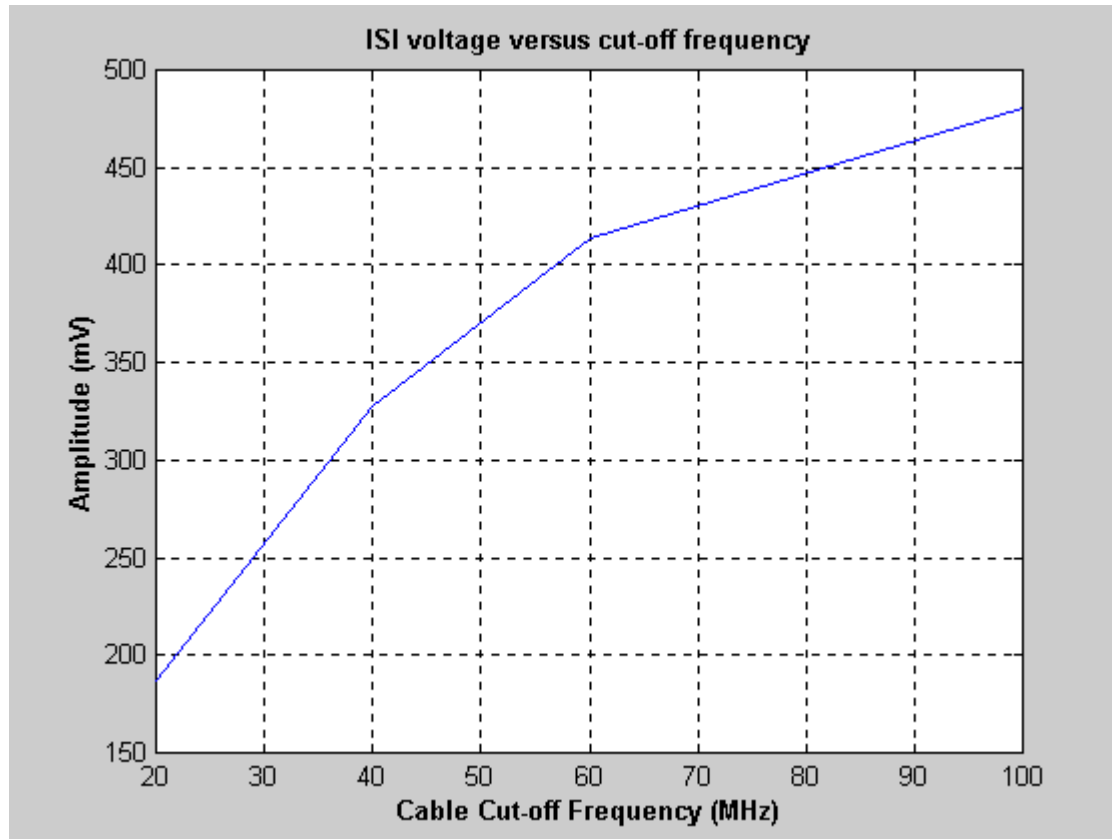
- Where  $V_k$  is the amplitude at the start of bit interval  $(k+1)$  (i.e., ISI)
- Can calculate  $V_k$  for  $\{X_k, X_{k-1}, X_{k-2}, \dots\} = \{\dots, 1, 0, 1, 0, \dots\}$

- The residual ISI voltage ( $V_k$ ) for a high frequency pattern is the peak voltage of the high frequency waveform.



Assuming you have skew compensated perfectly!

- The residual voltage ( $V_k$ ) for a high frequency pattern depends on the cable cut-off frequency and the total receiver amplitude.
- At  $f_c = 40\text{MHz}$   $V_k = 330\text{mV}$  for a  $1V_{\text{pk-pk}}$  signal swing

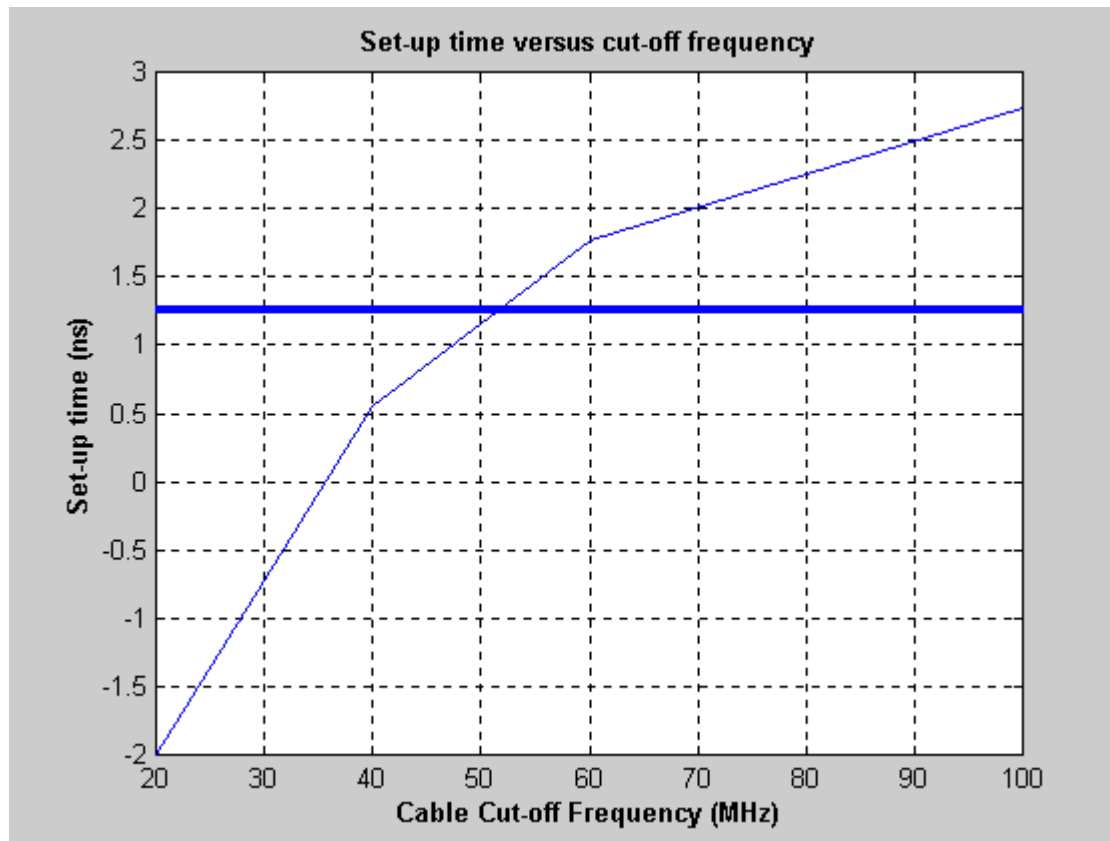


- With signal starting from ISI residual voltage the set-up time is:

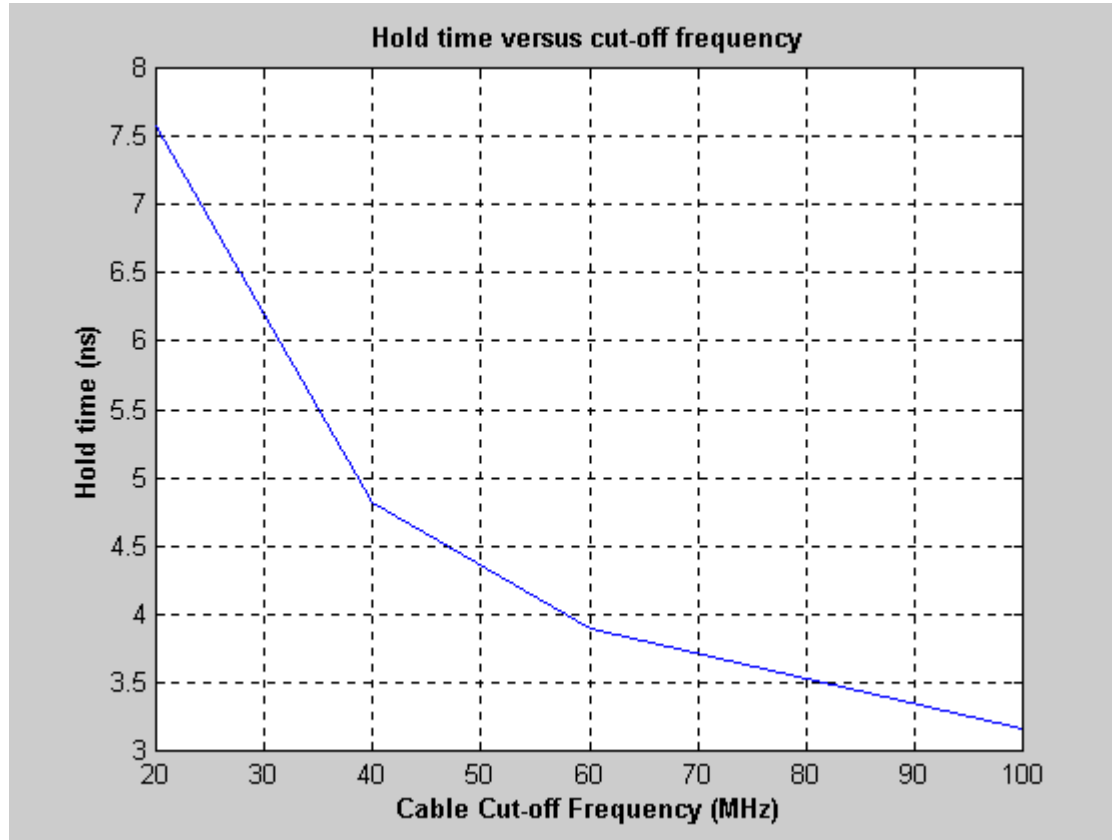
$$t_{su}(V_{setup}) = T_{sample} + \tau \ln\left(\frac{500mV - V_{setup}}{1000mV - V_k}\right)$$

- The threshold voltage ( $V_{setup}$ ) is specified at 100mV.

- Set-up time versus cable cut-off frequency.
  - For  $f_c = 60\text{MHz}$  ( $=1/2\pi \tau$ ), set-up time = 1.75ns
  - For  $f_c = 40\text{MHz}$  ( $=1/2\pi \tau$ ), set-up time = 525ps



- Hold time versus cable cut-off frequency



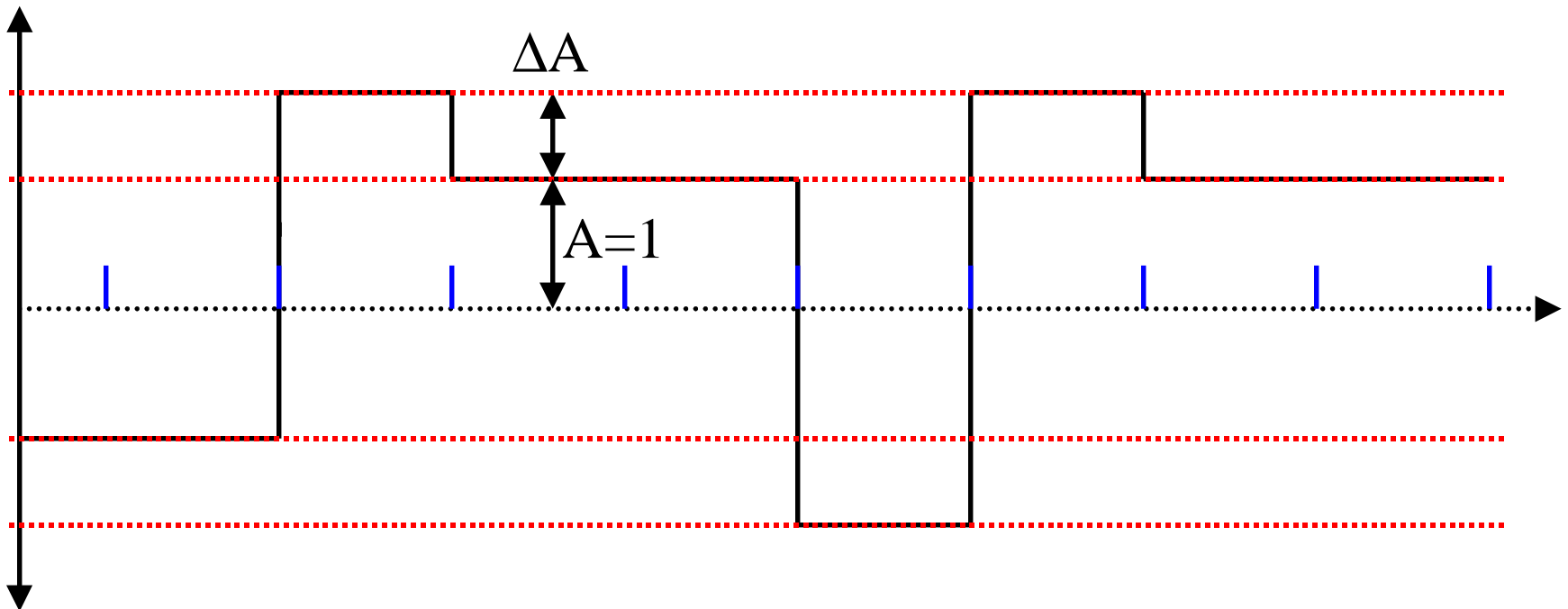


- Quantum believes that timing pre-compensation alone is insufficient to compensate for ISI at 320 MB/sec SCSI transfer rates

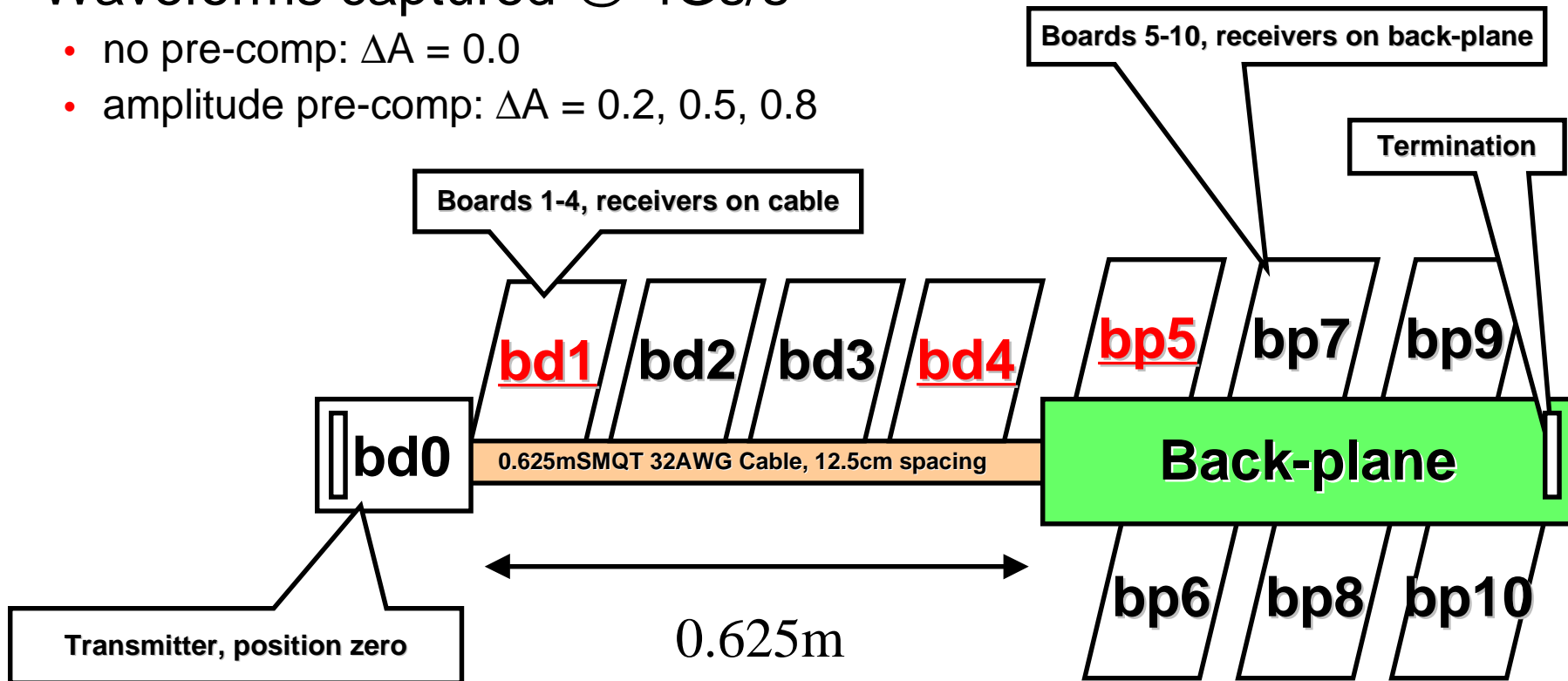
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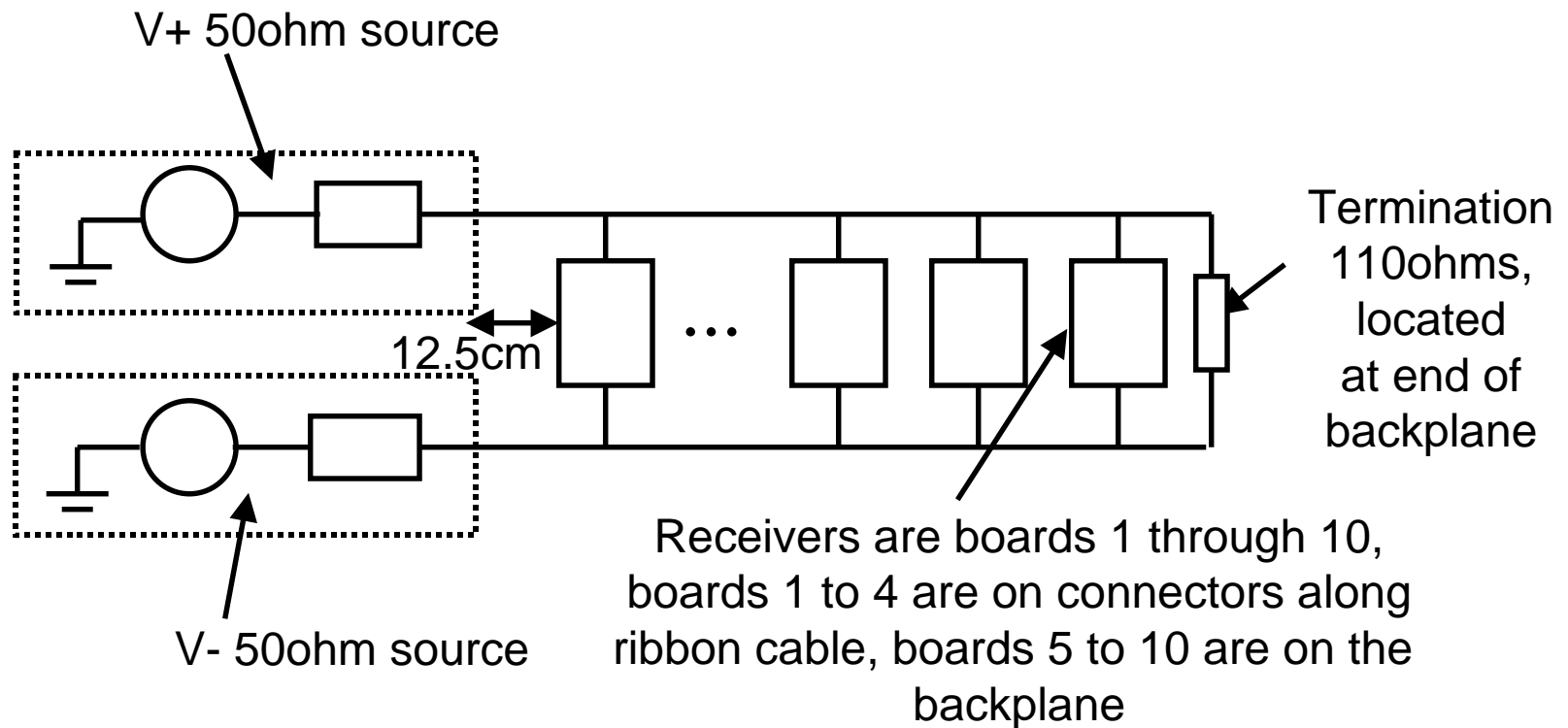
## Part II Amplitude Pre-Compensation Study

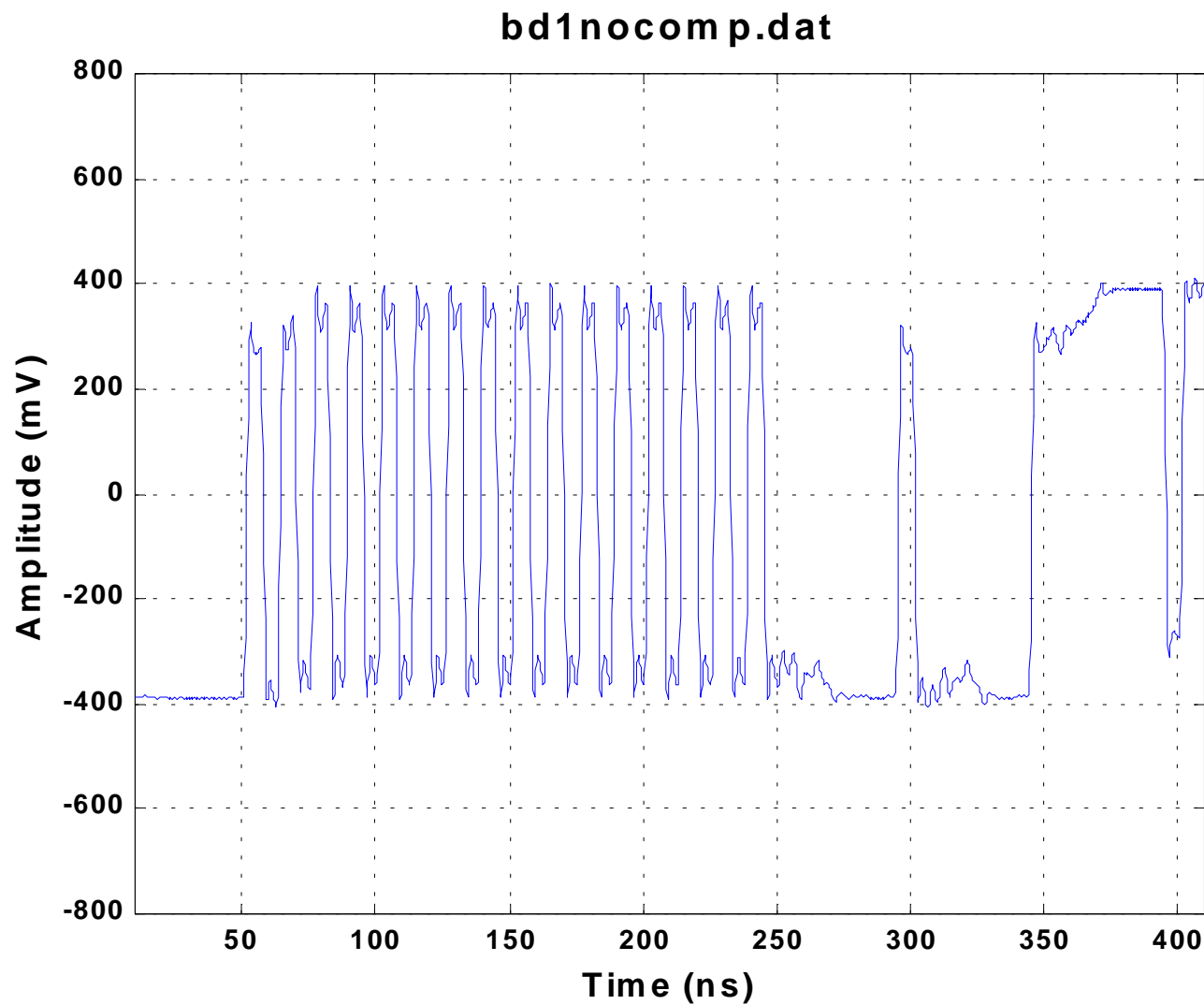
- Increase the amplitude of transmitted signal on signal transitions
- If there is no transition, return amplitude to nominal level (normalized to 1)
- $\Delta A$  - amplitude increase is design parameter

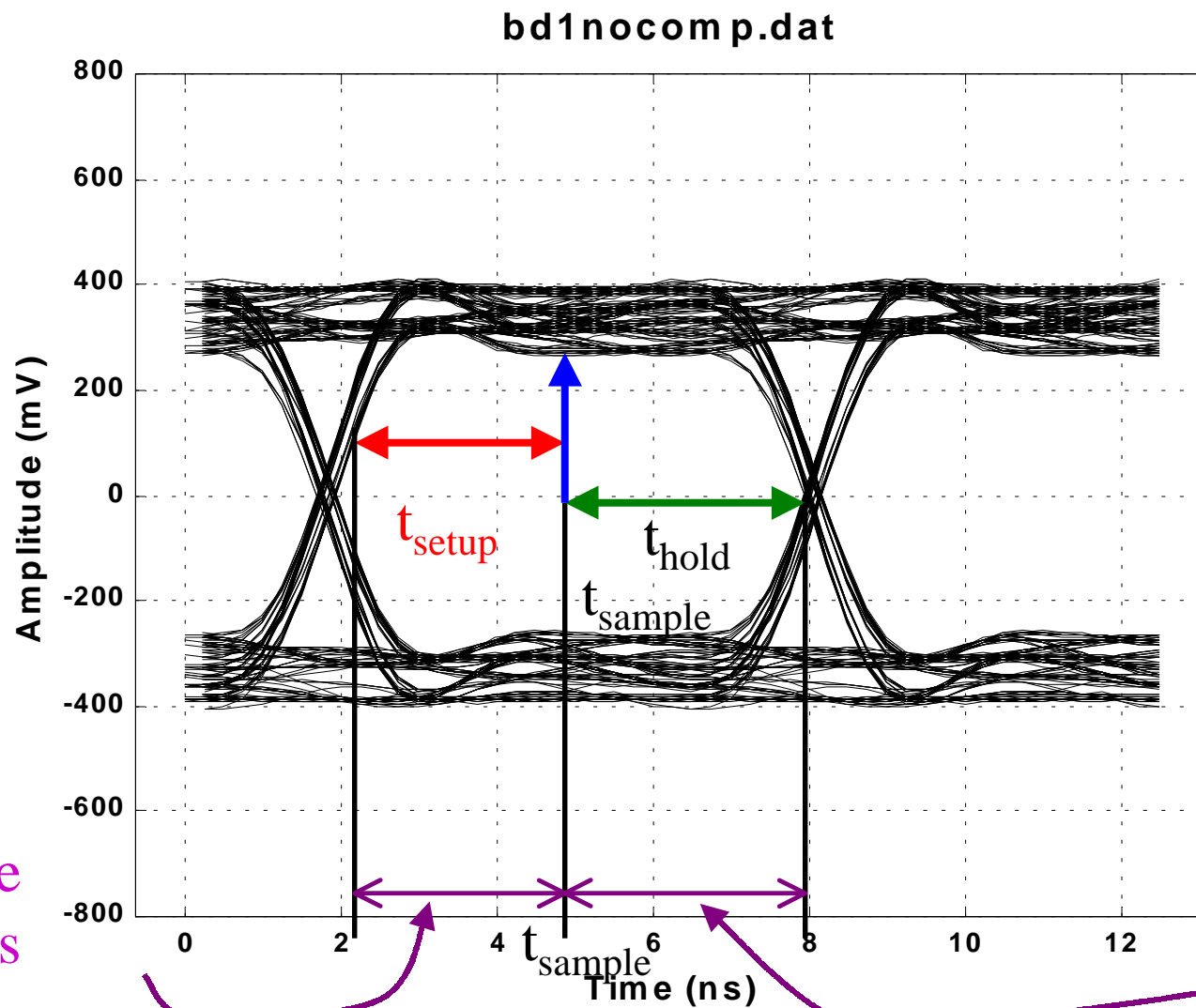


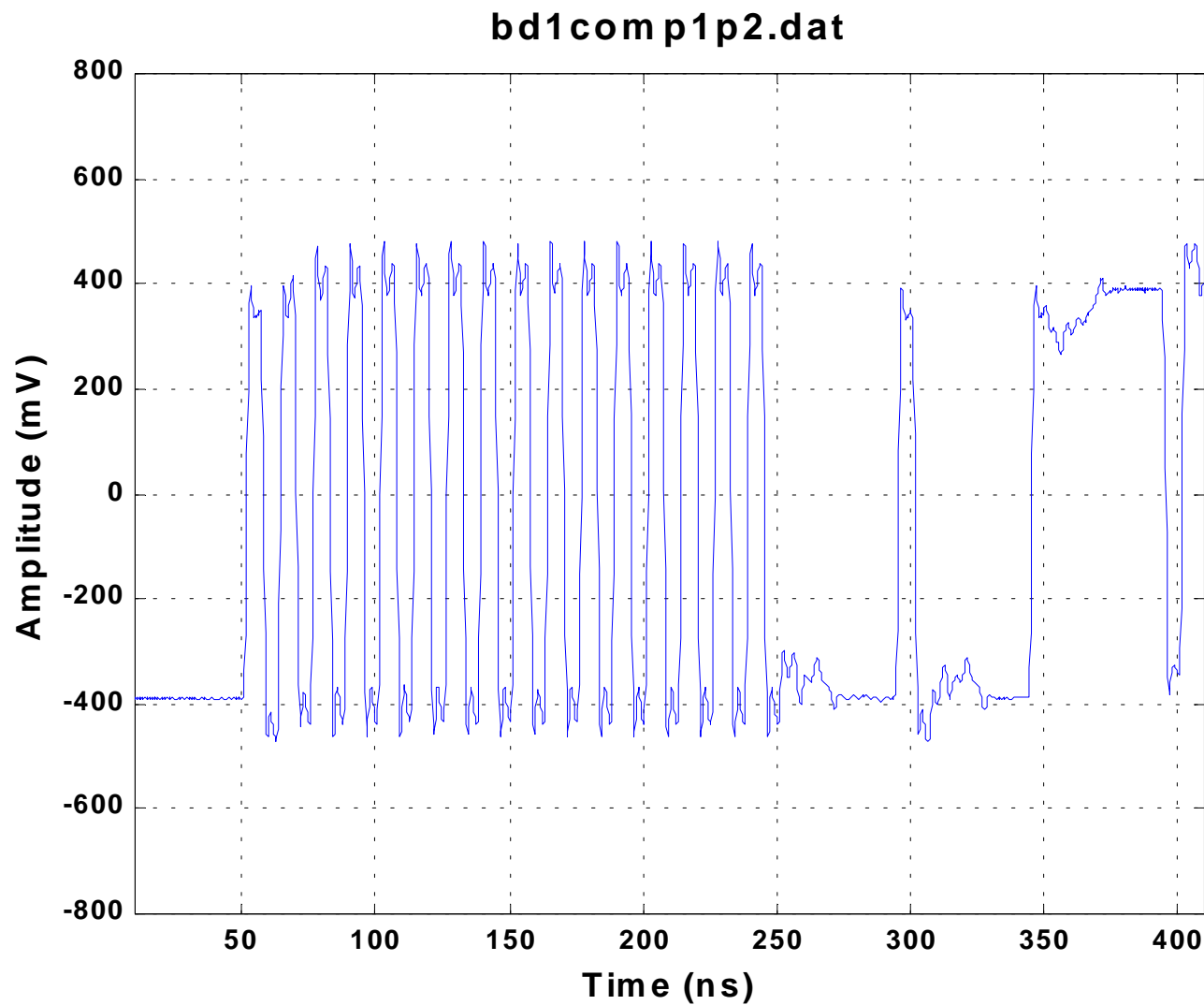
- Hitachi 0.625 meter, 32AWG twisted-flat ribbon cable, 12.5cm load spacing, plus 6-slot back-plane.
- Waveforms captured @ 4Gs/s
  - no pre-comp:  $\Delta A = 0.0$
  - amplitude pre-comp:  $\Delta A = 0.2, 0.5, 0.8$



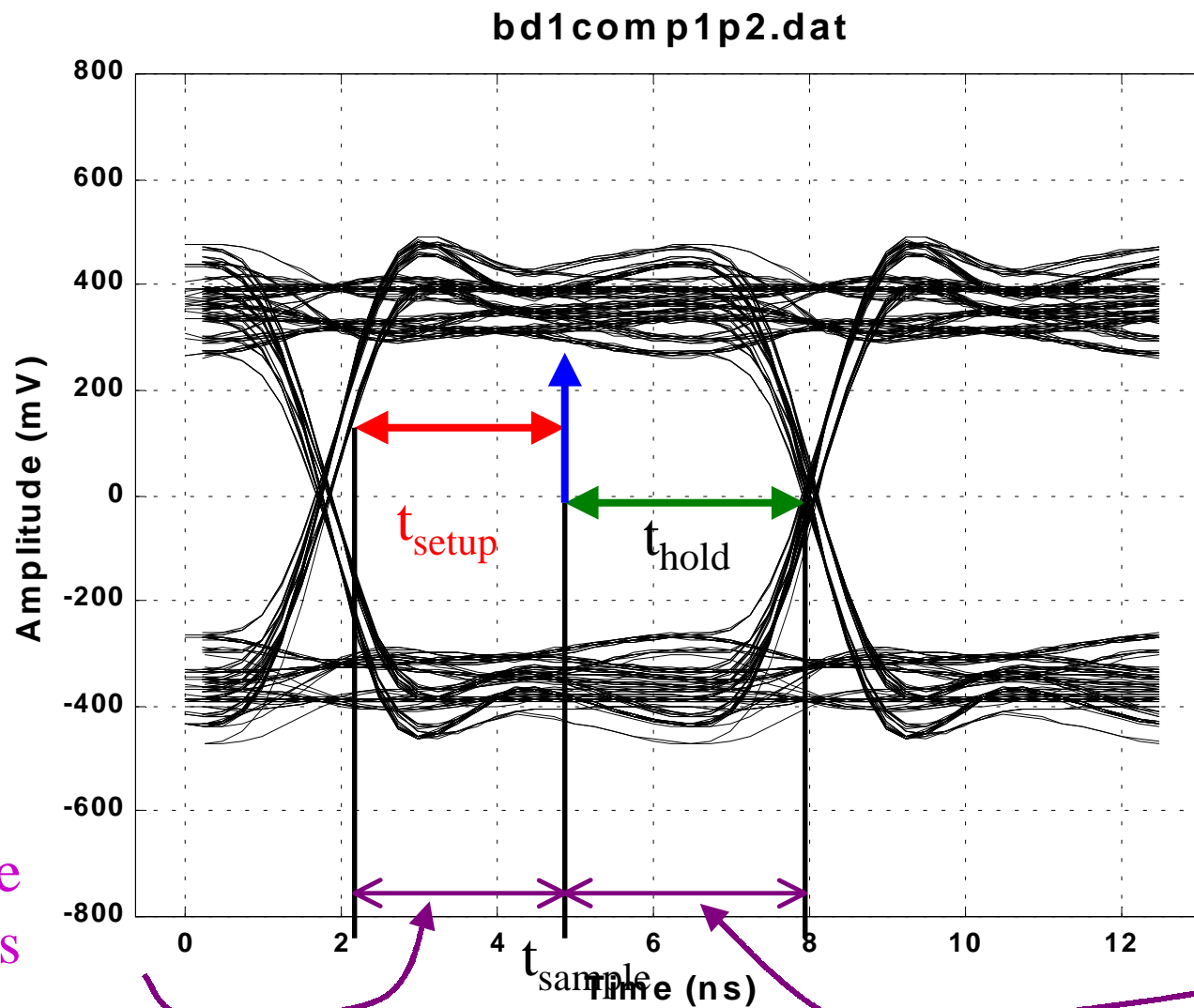






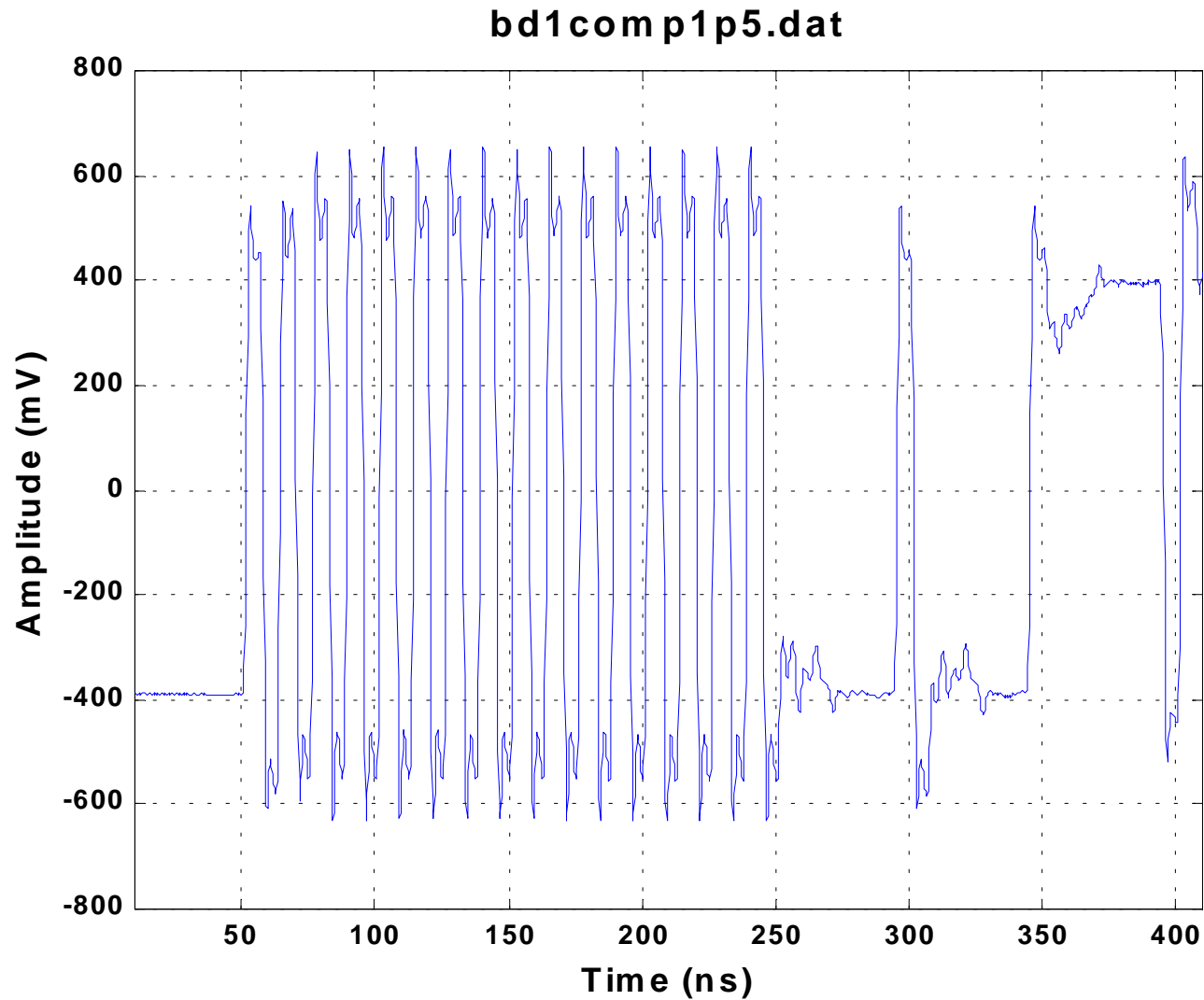


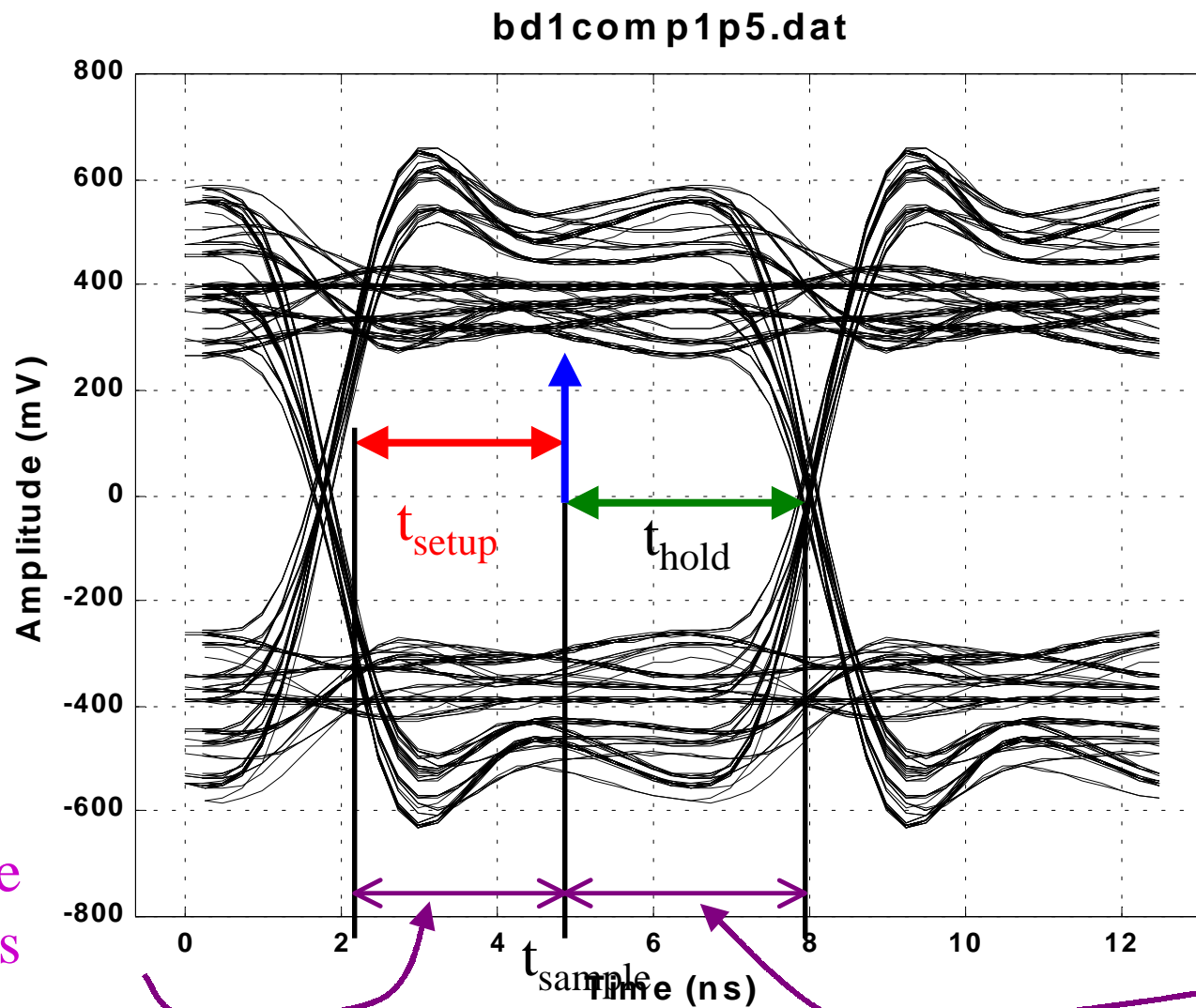




setup time  
~2.8ns

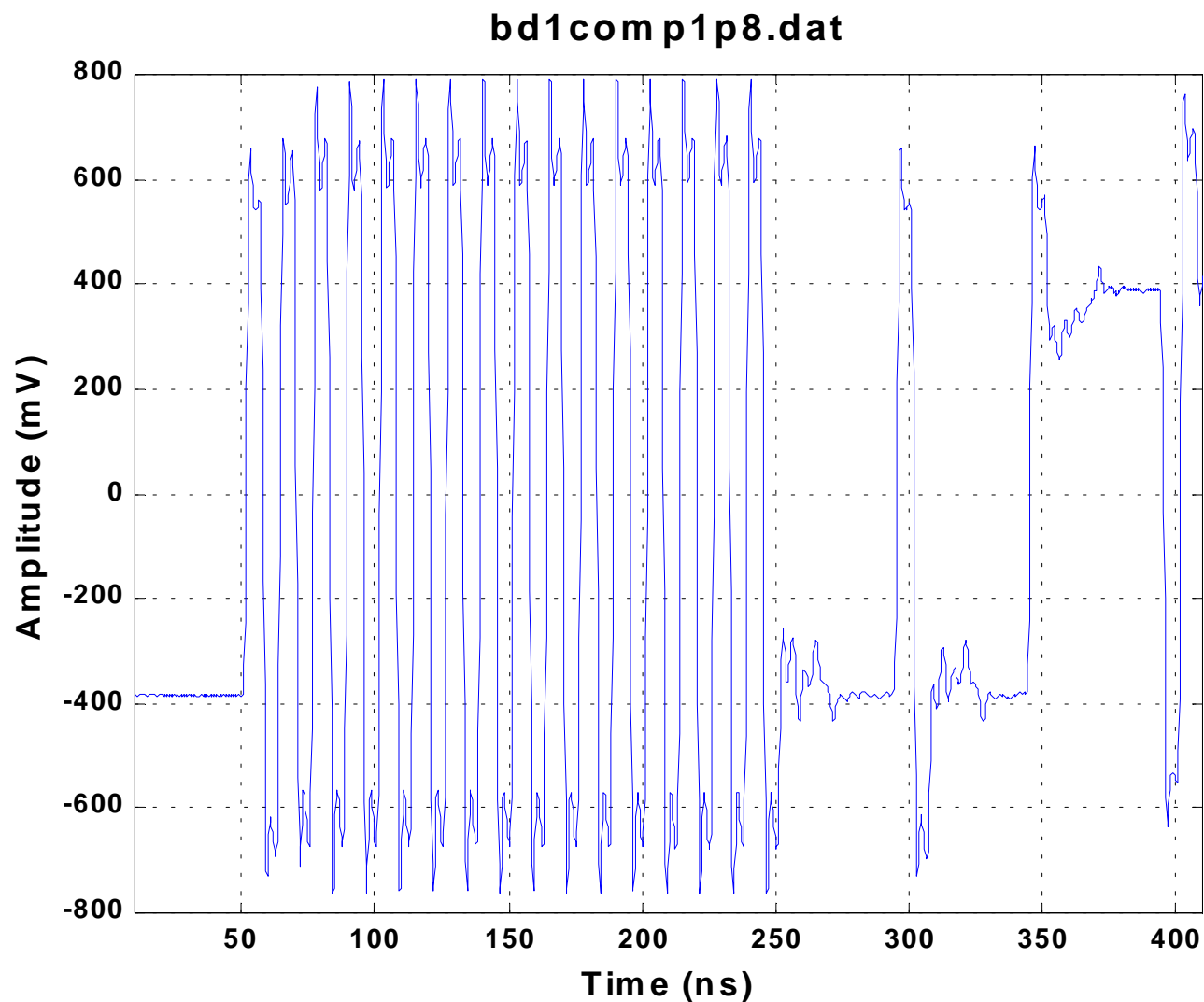
hold time  
~3.2ns

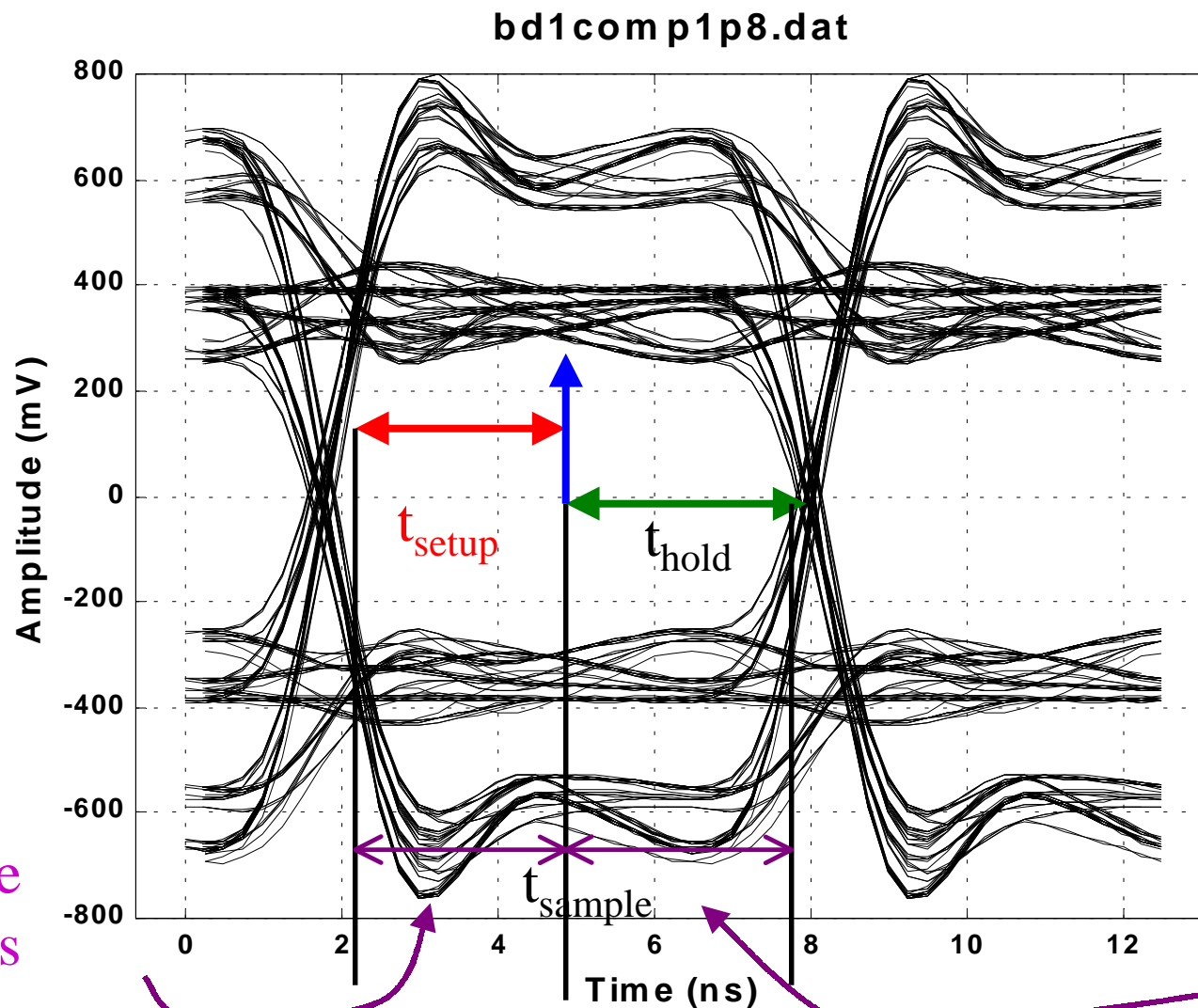




setup time  
~2.8ns

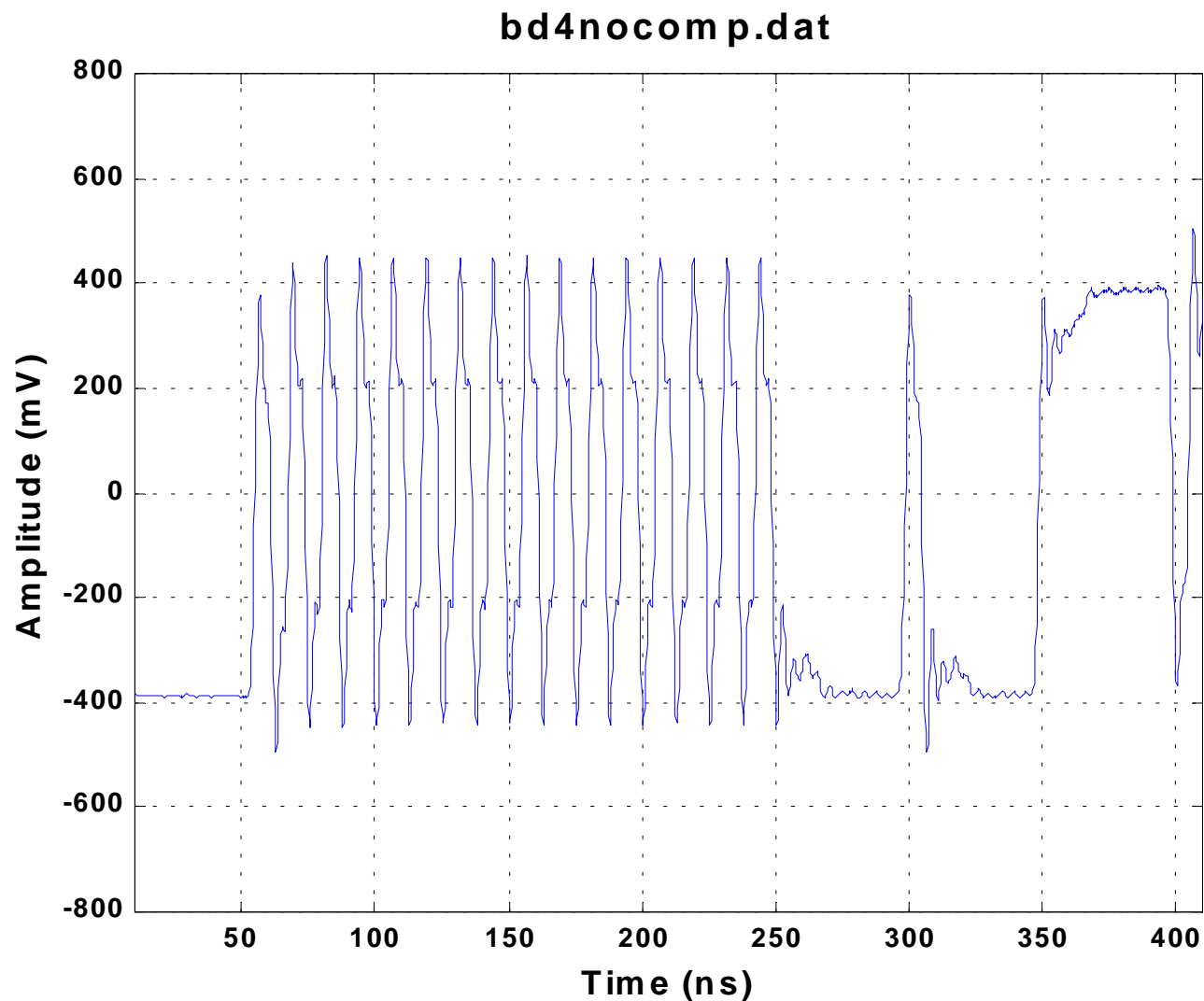
hold time  
~3.2ns

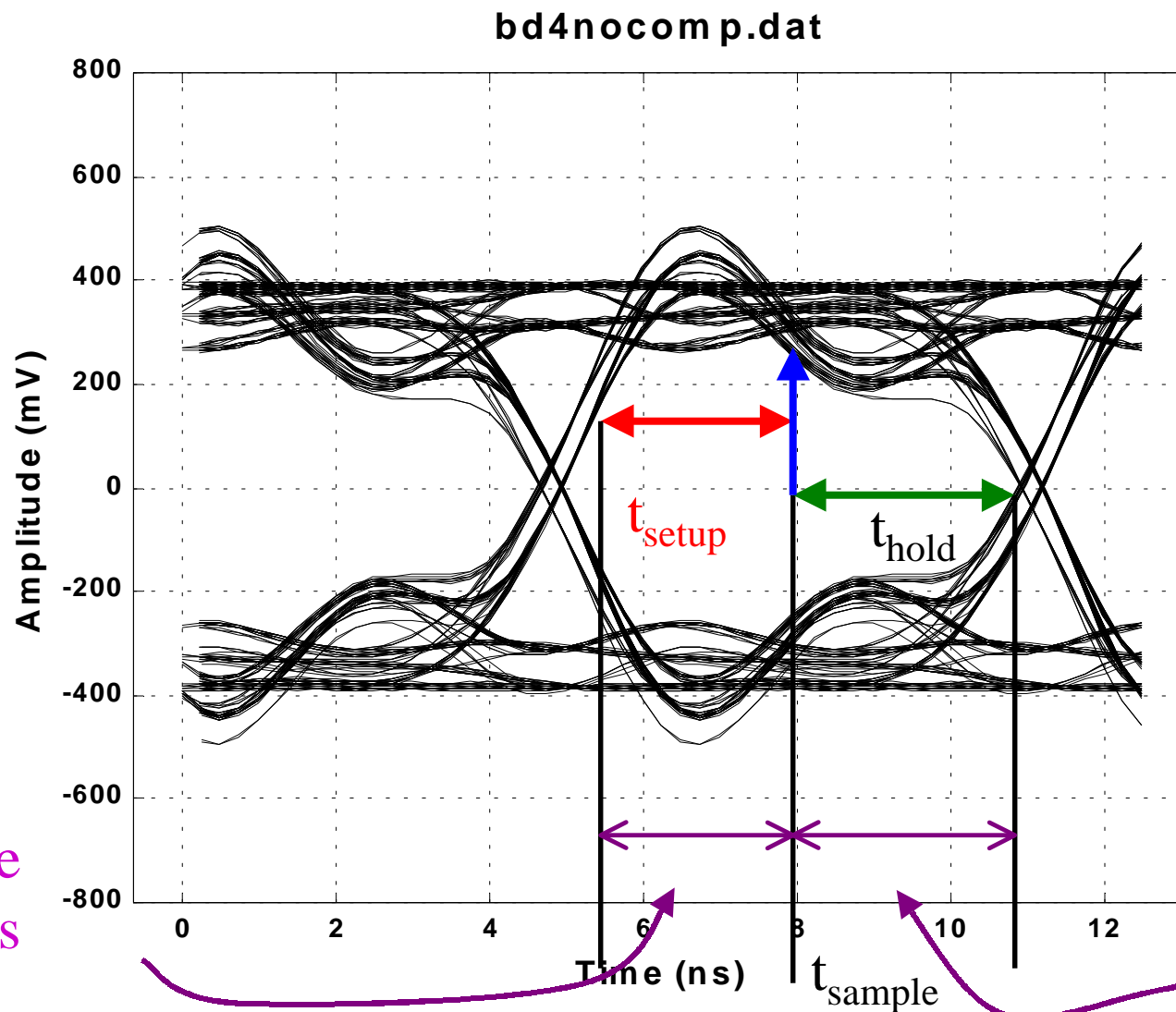




setup time  
~2.8ns

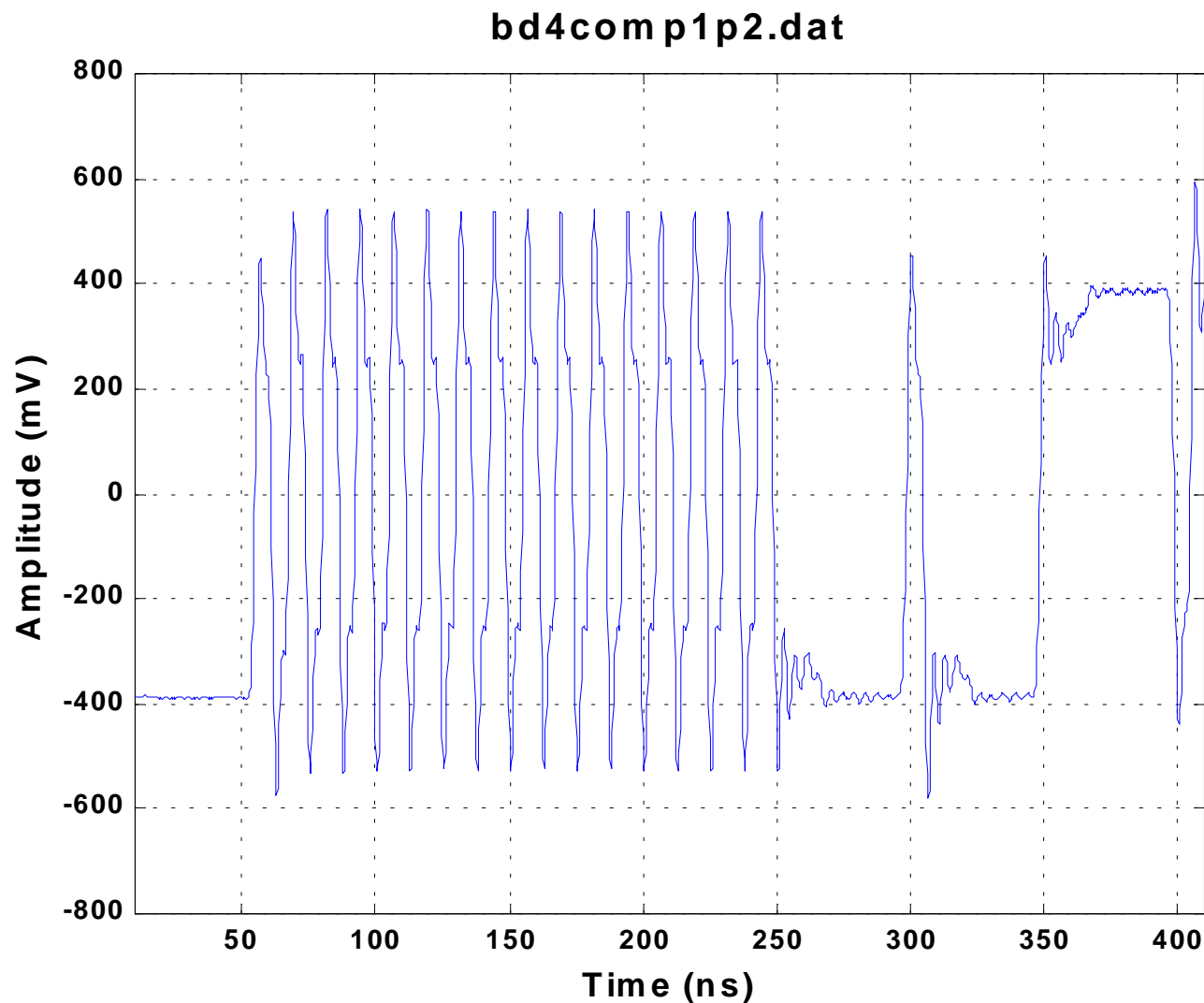
hold time  
~3.0ns



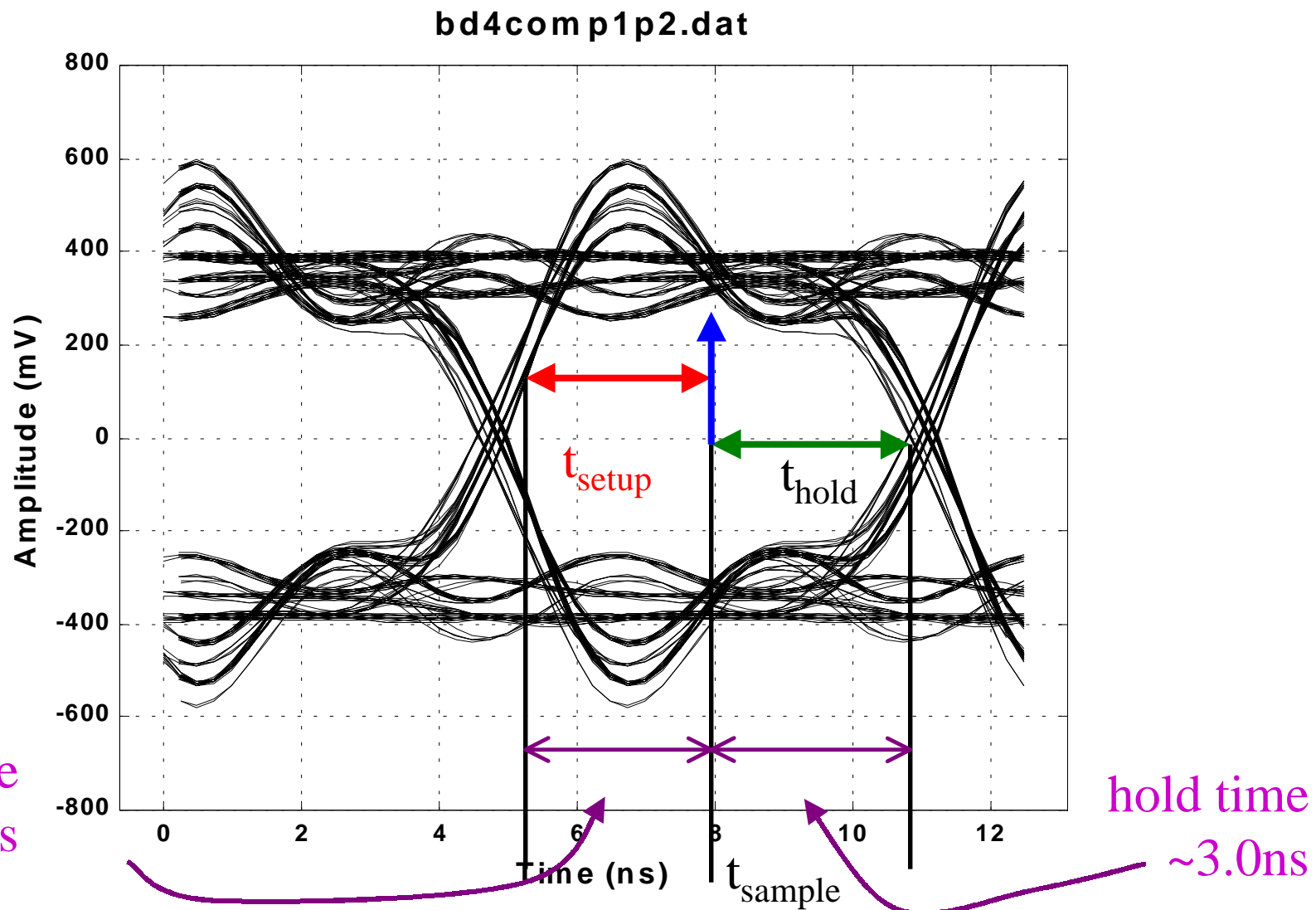


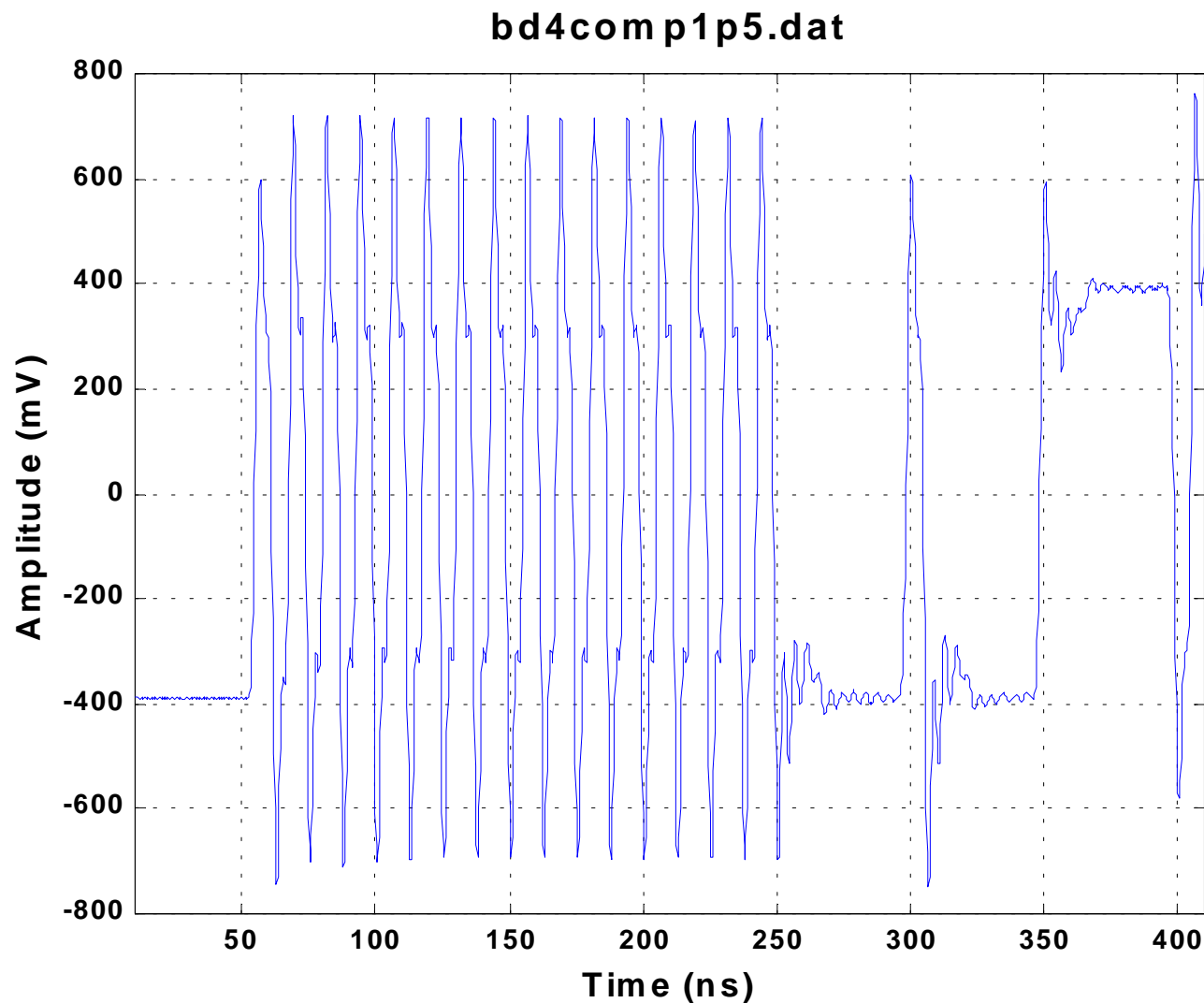
setup time  
~2.6ns

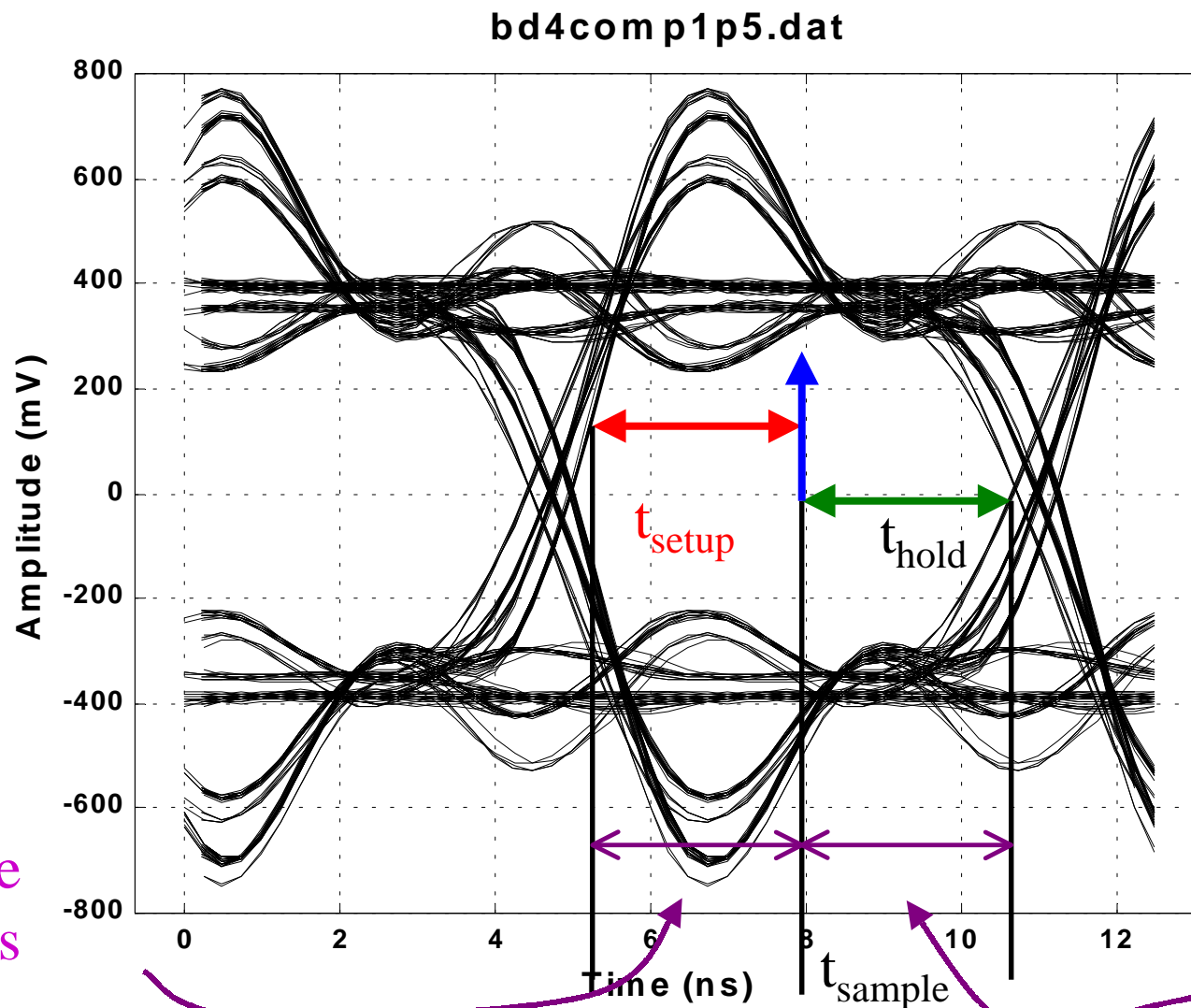
hold time  
~3.0ns





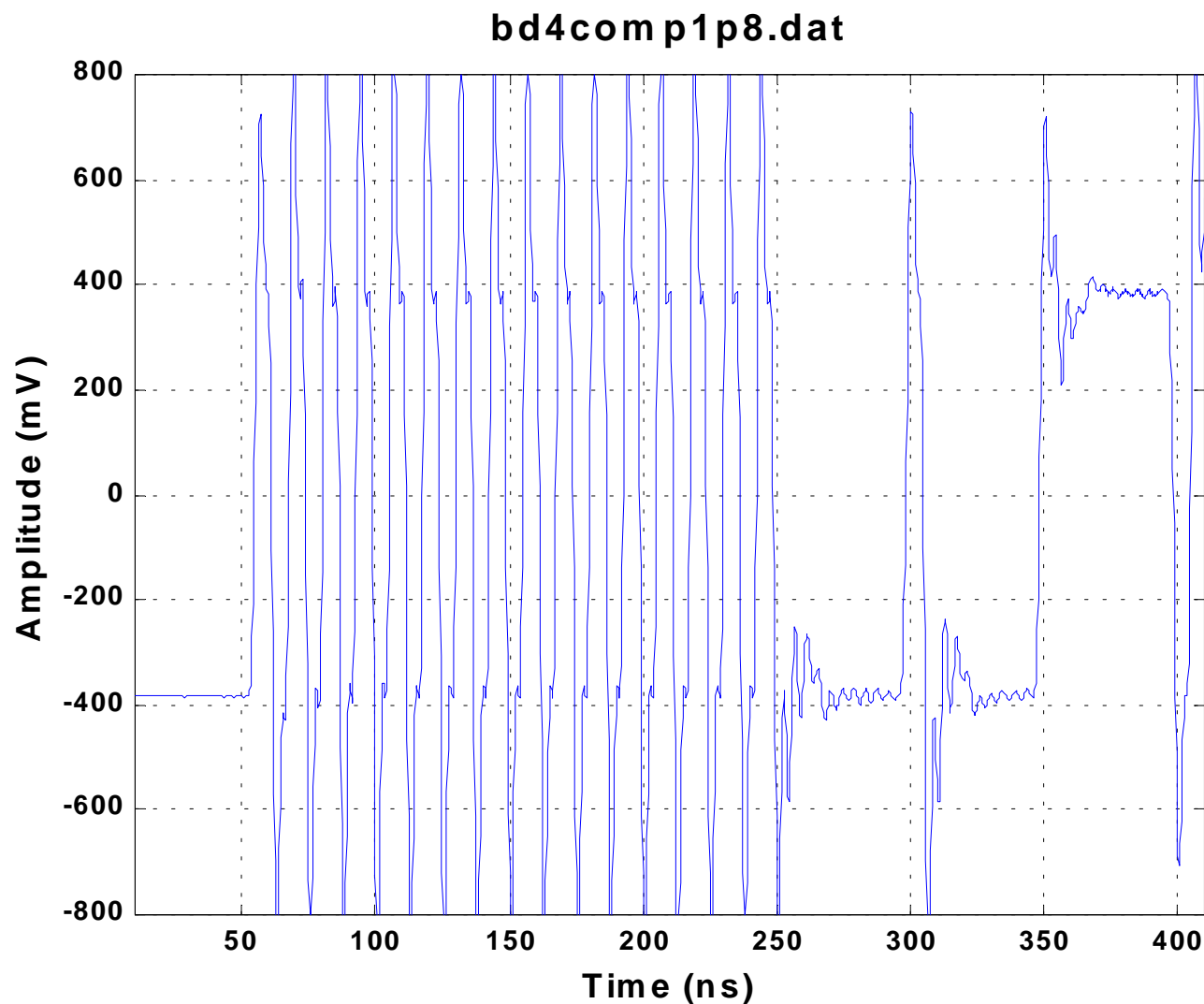


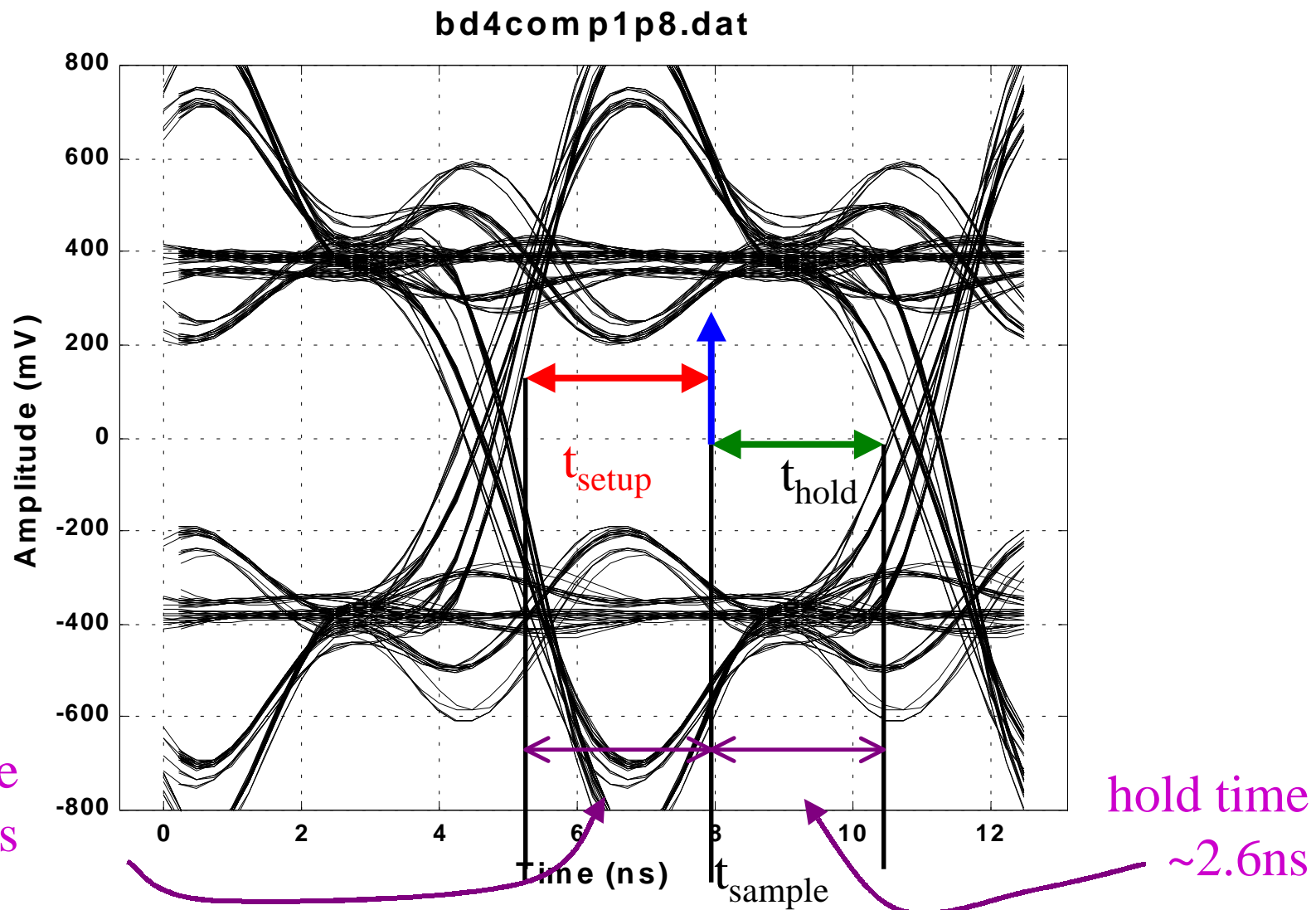


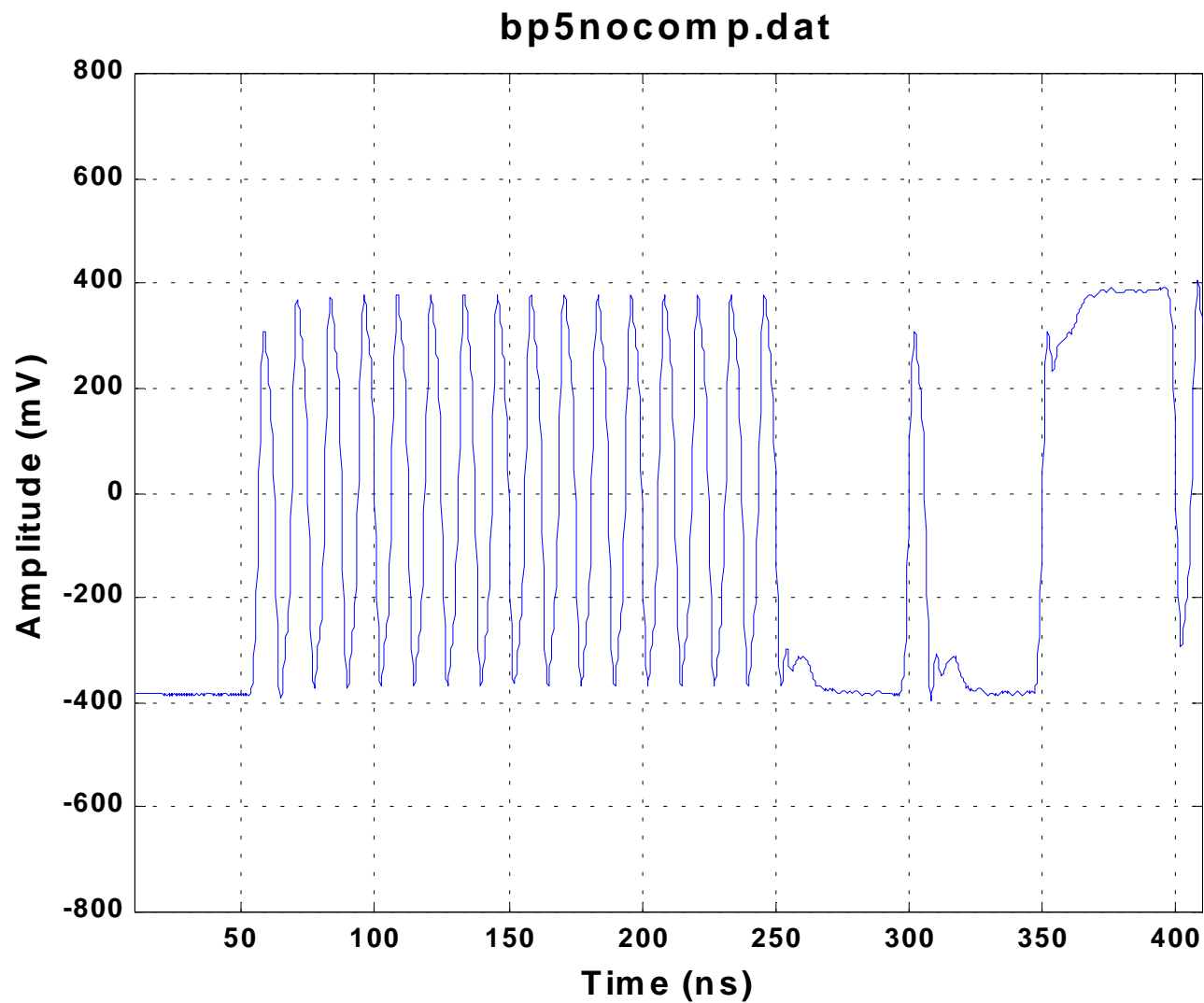


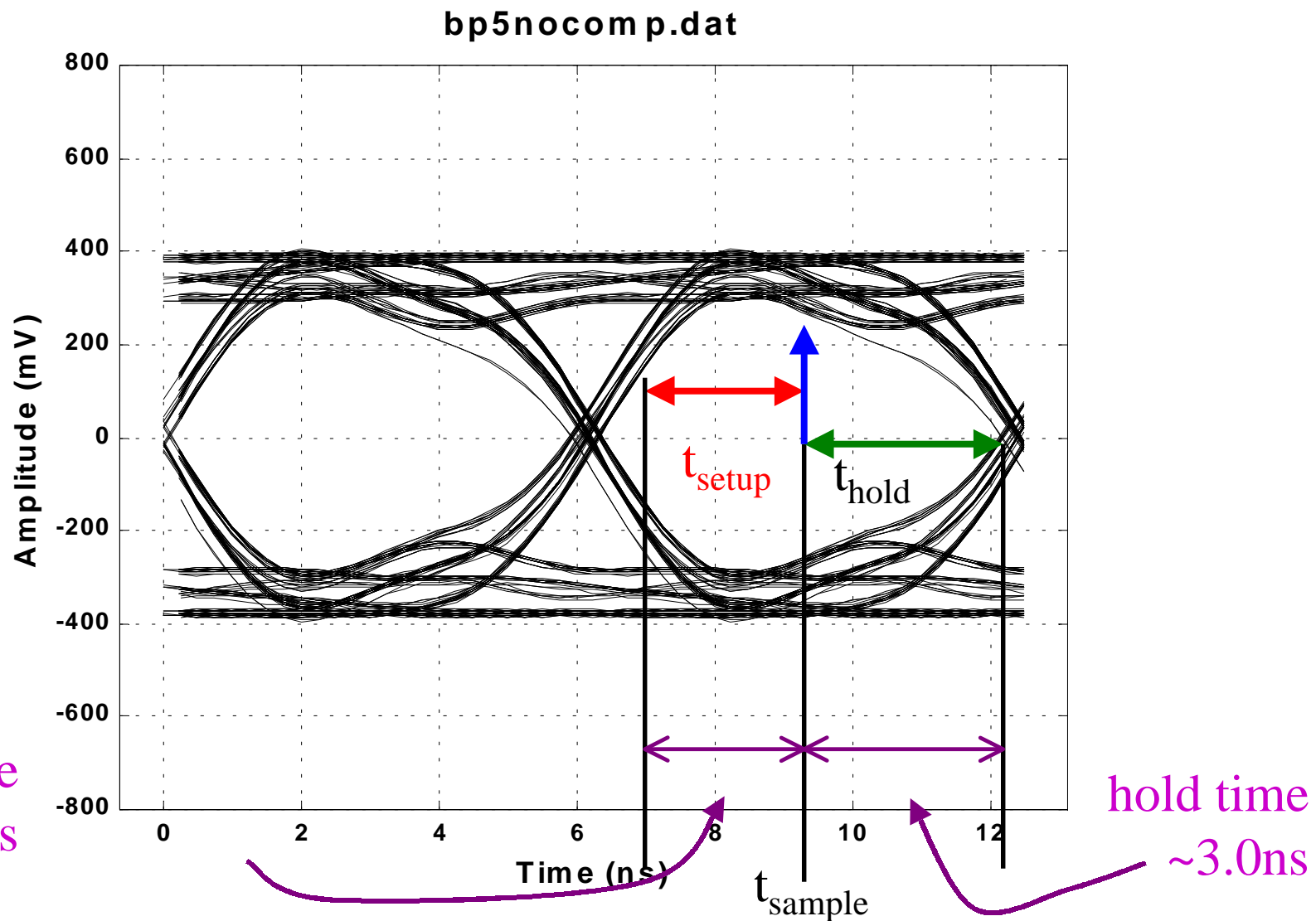
setup time  
~2.8ns

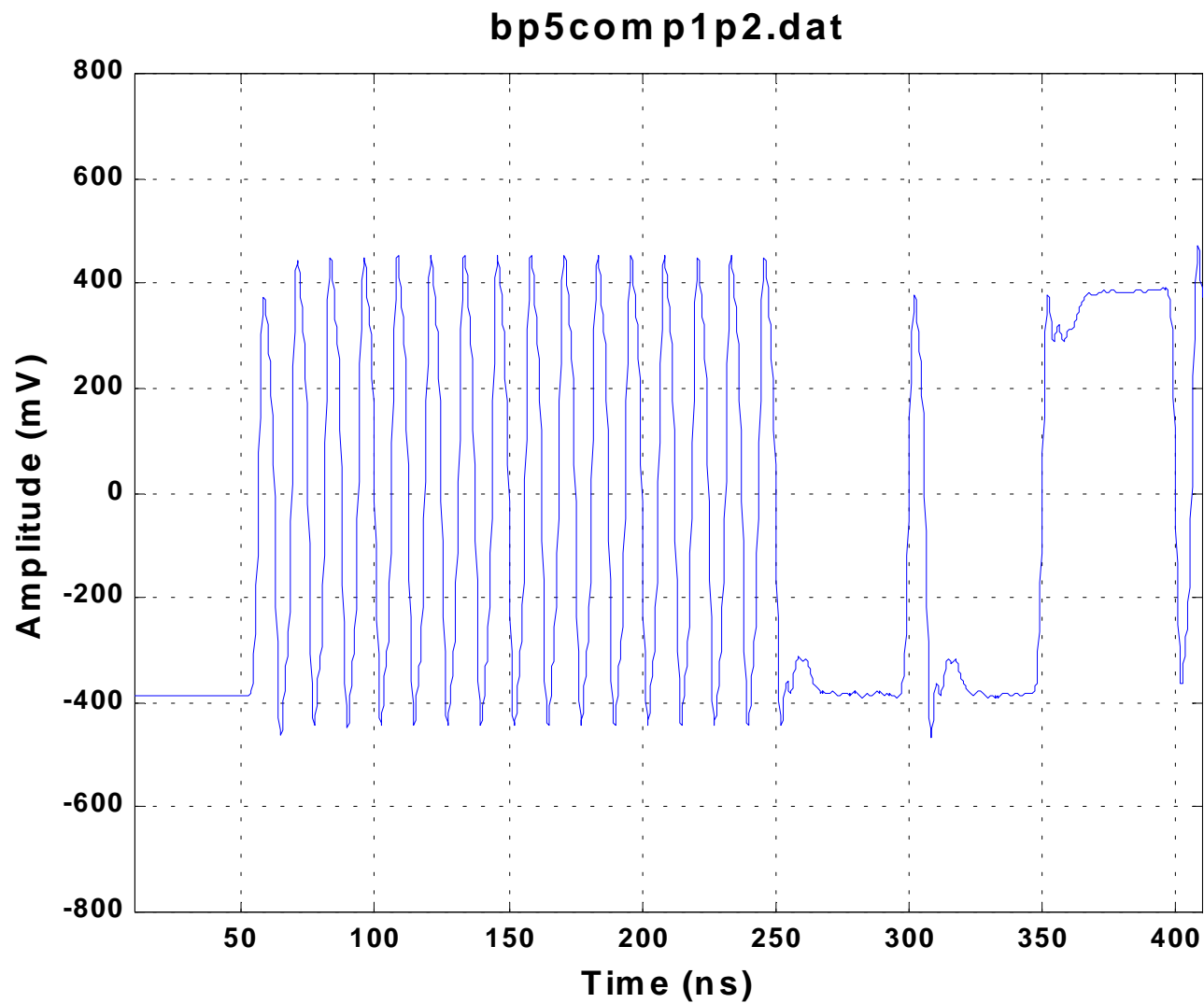
hold time  
~2.8ns



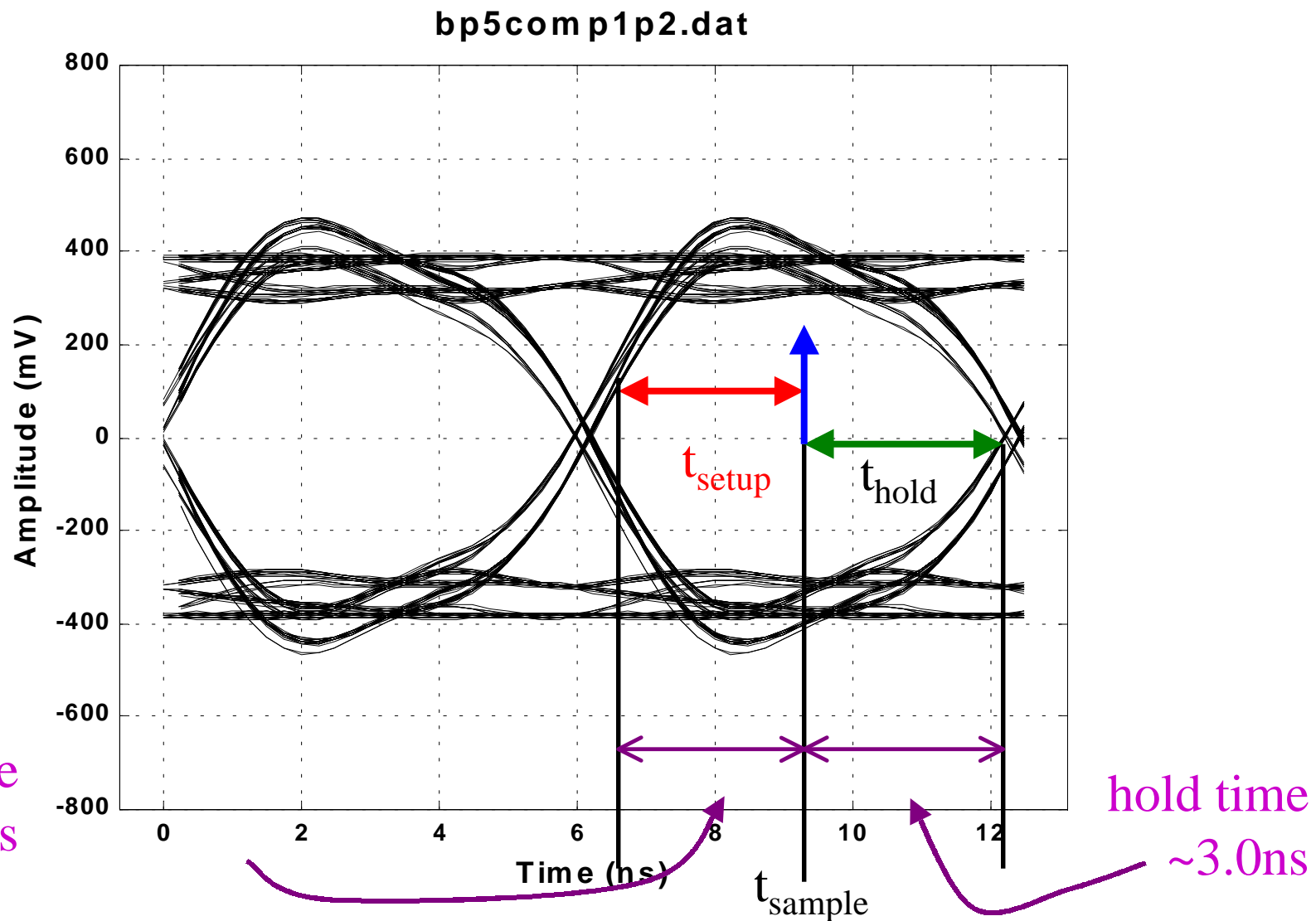


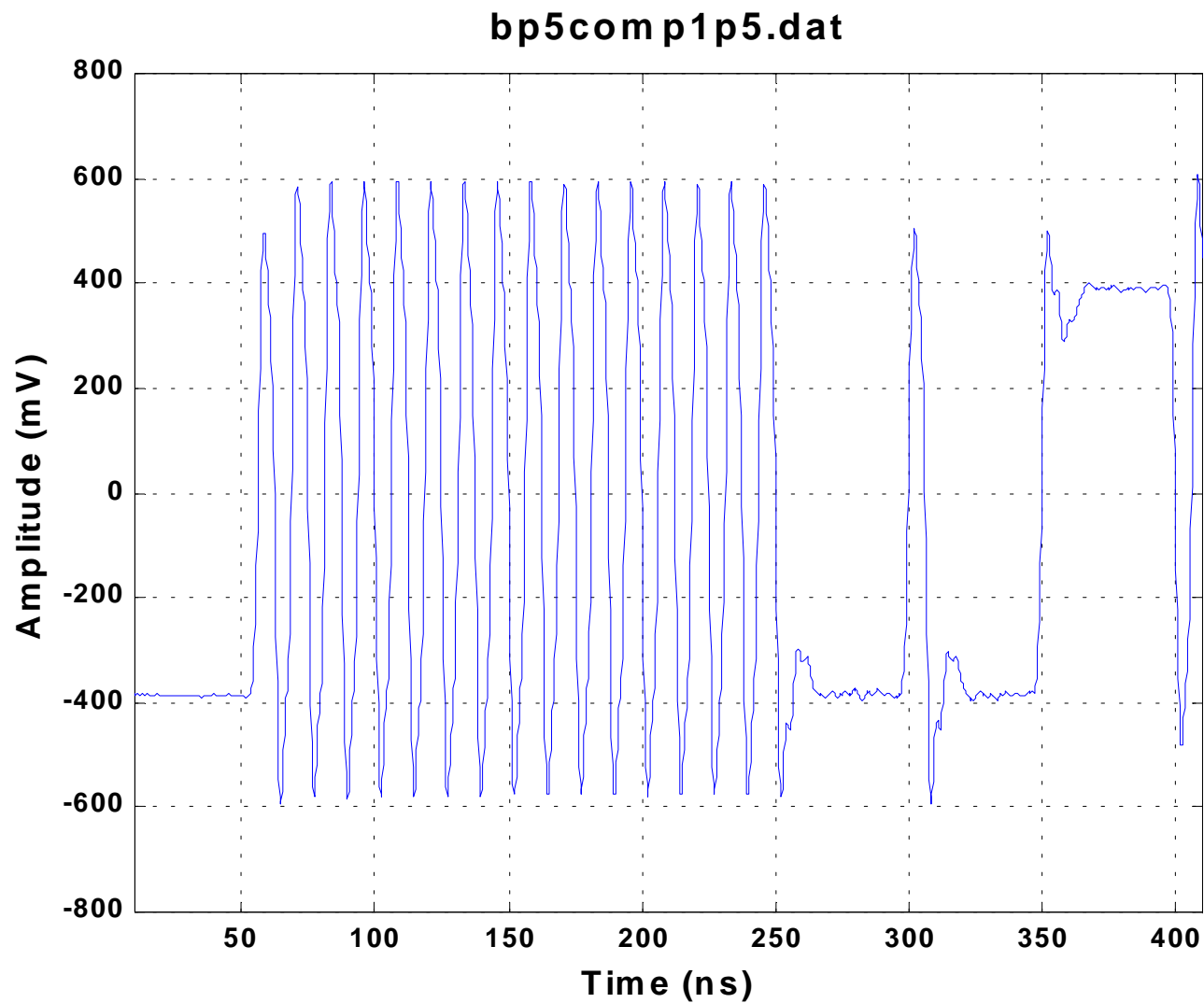


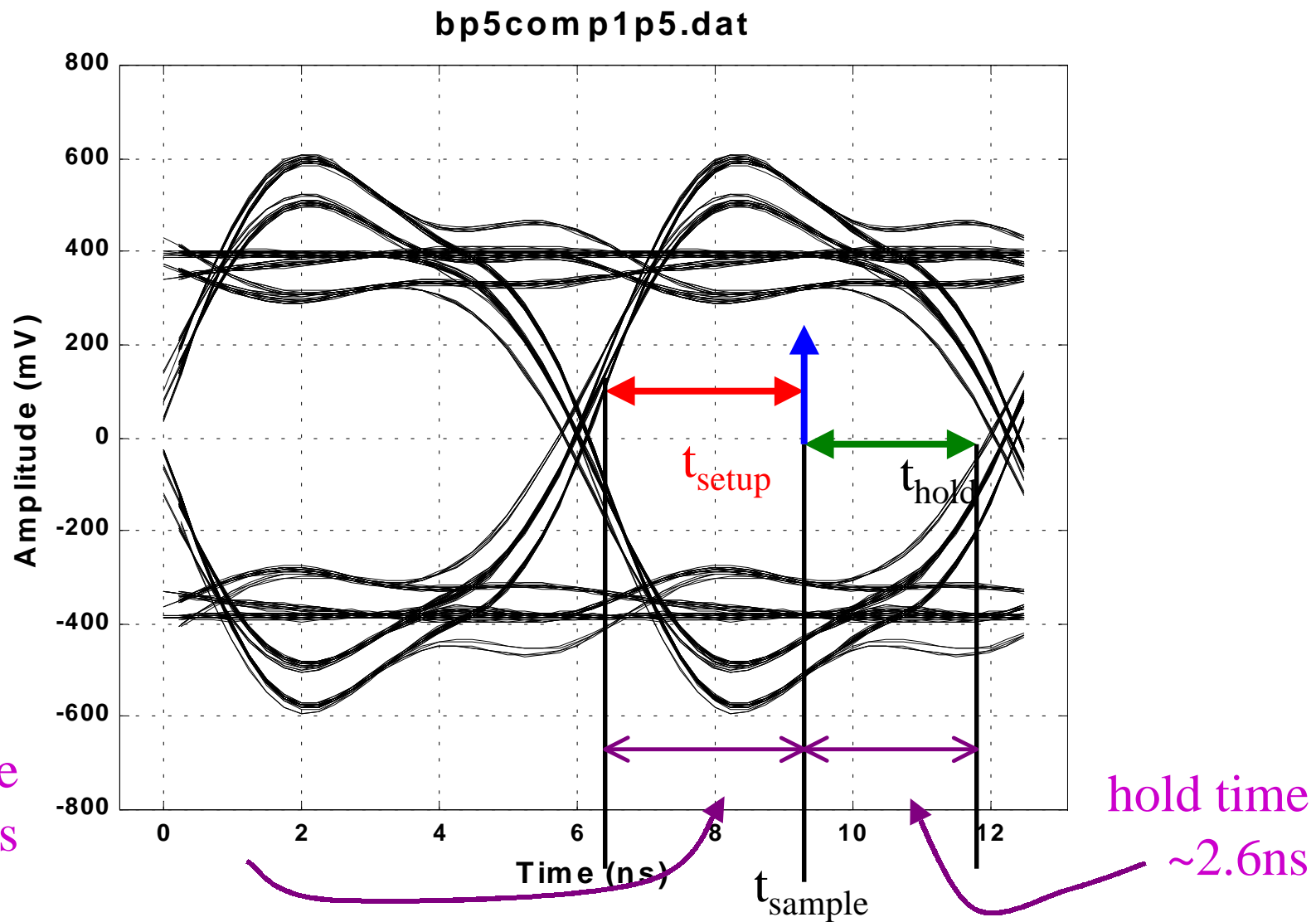


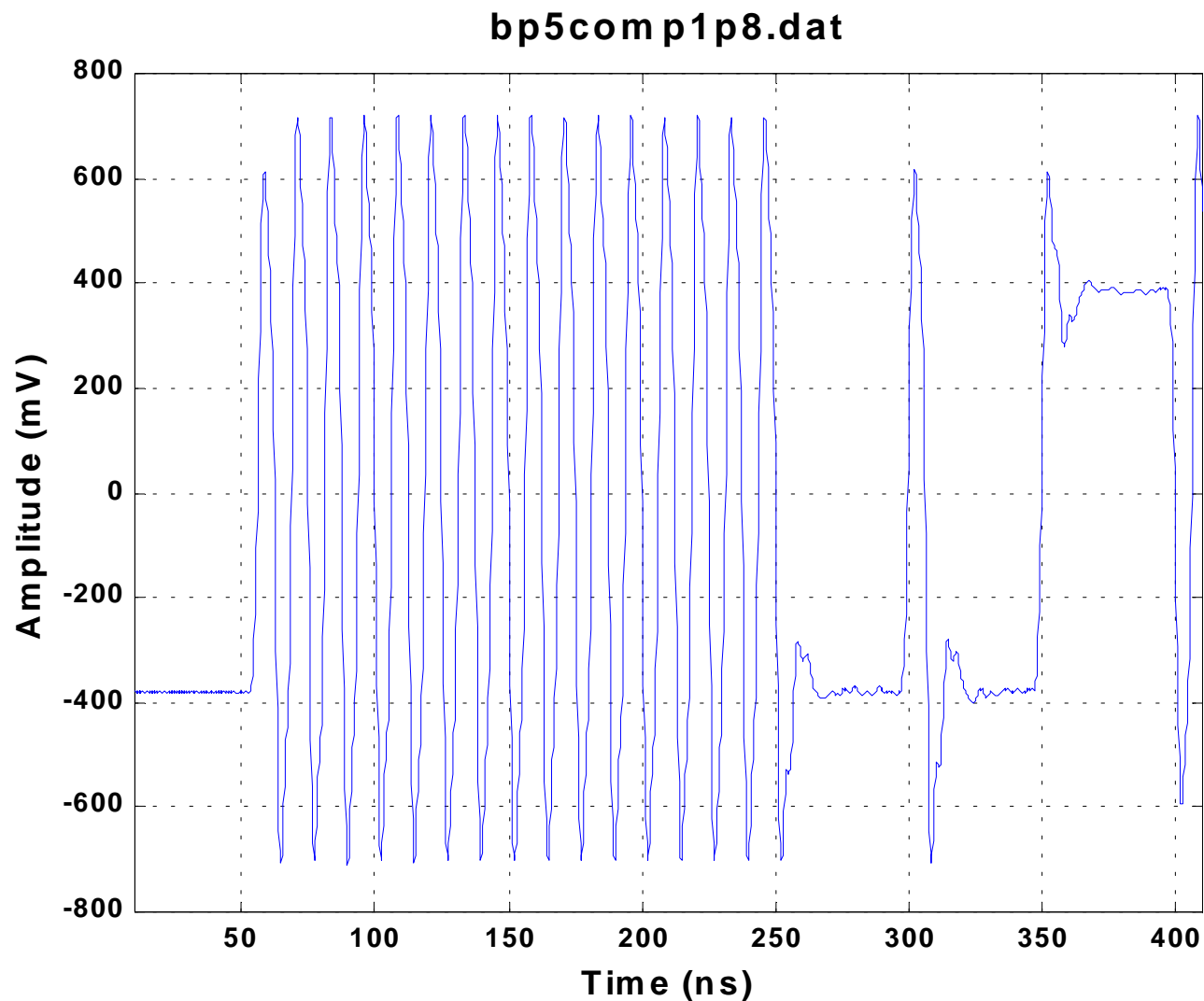


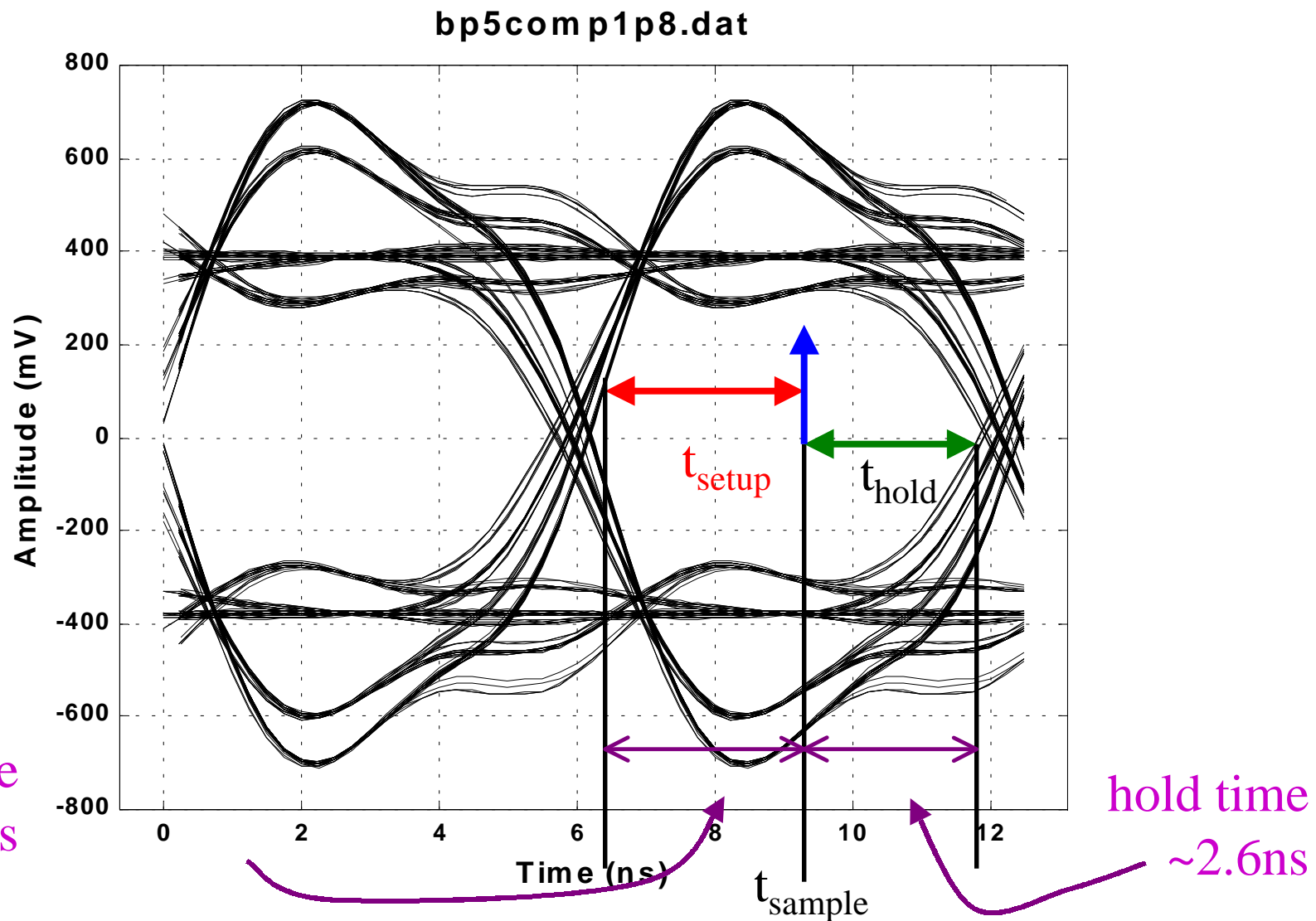




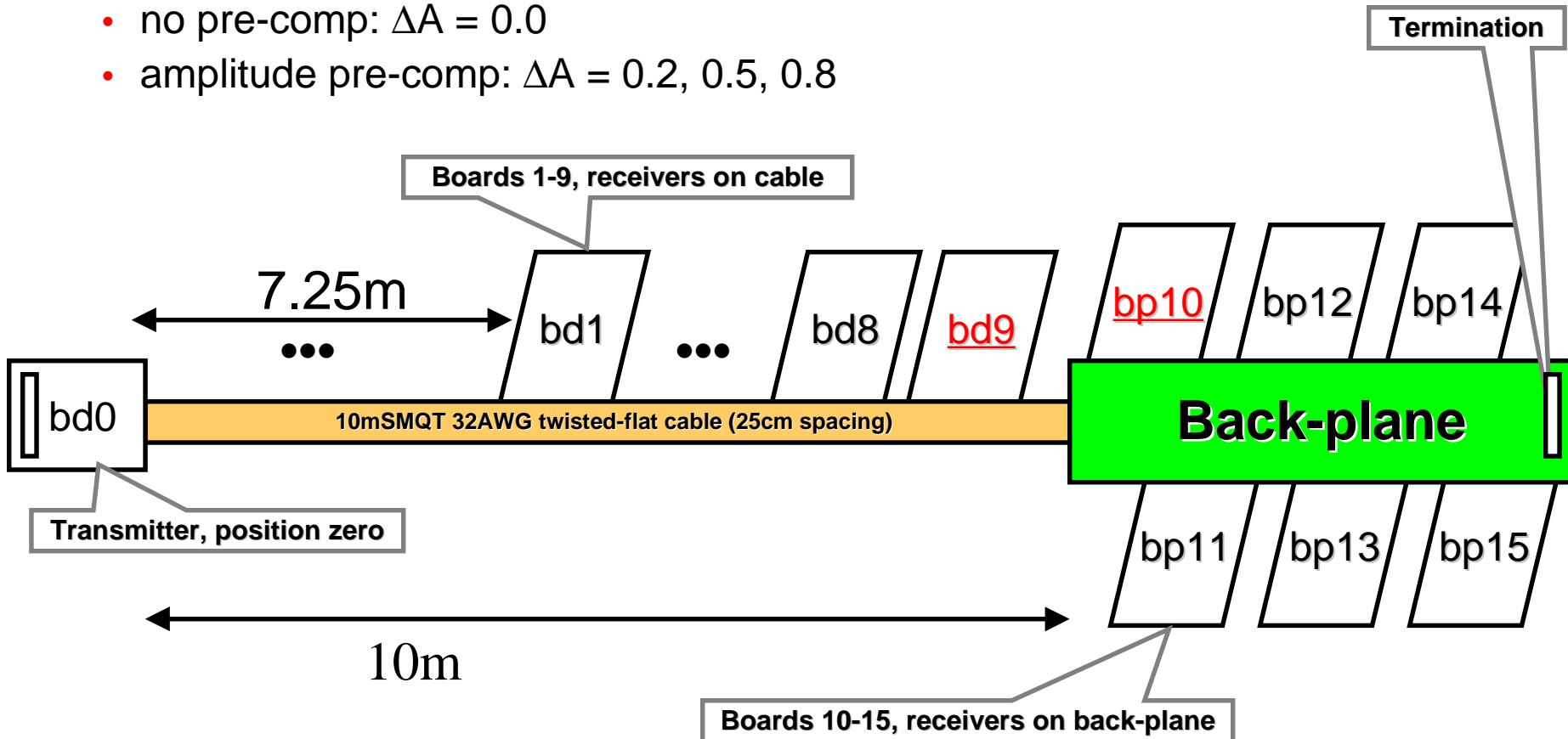


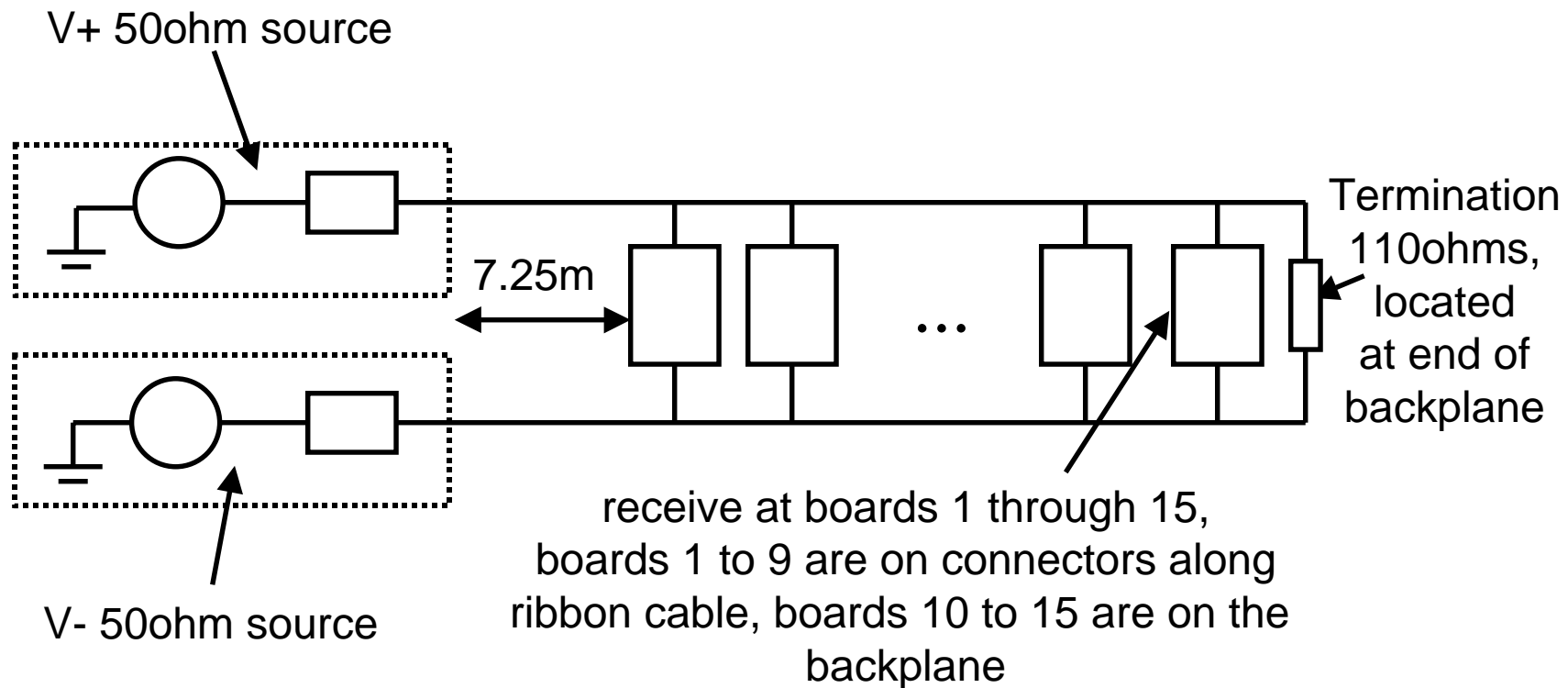


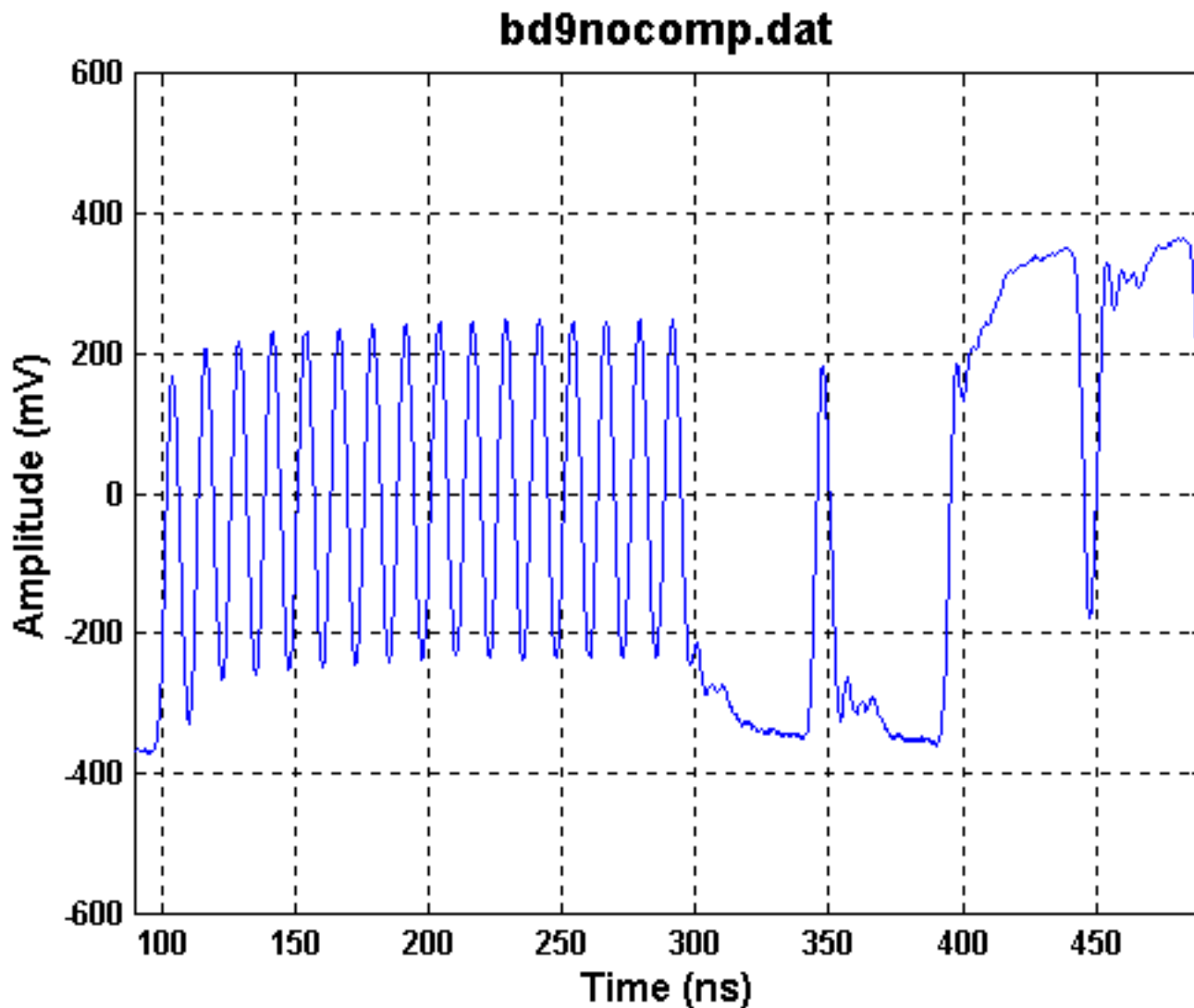




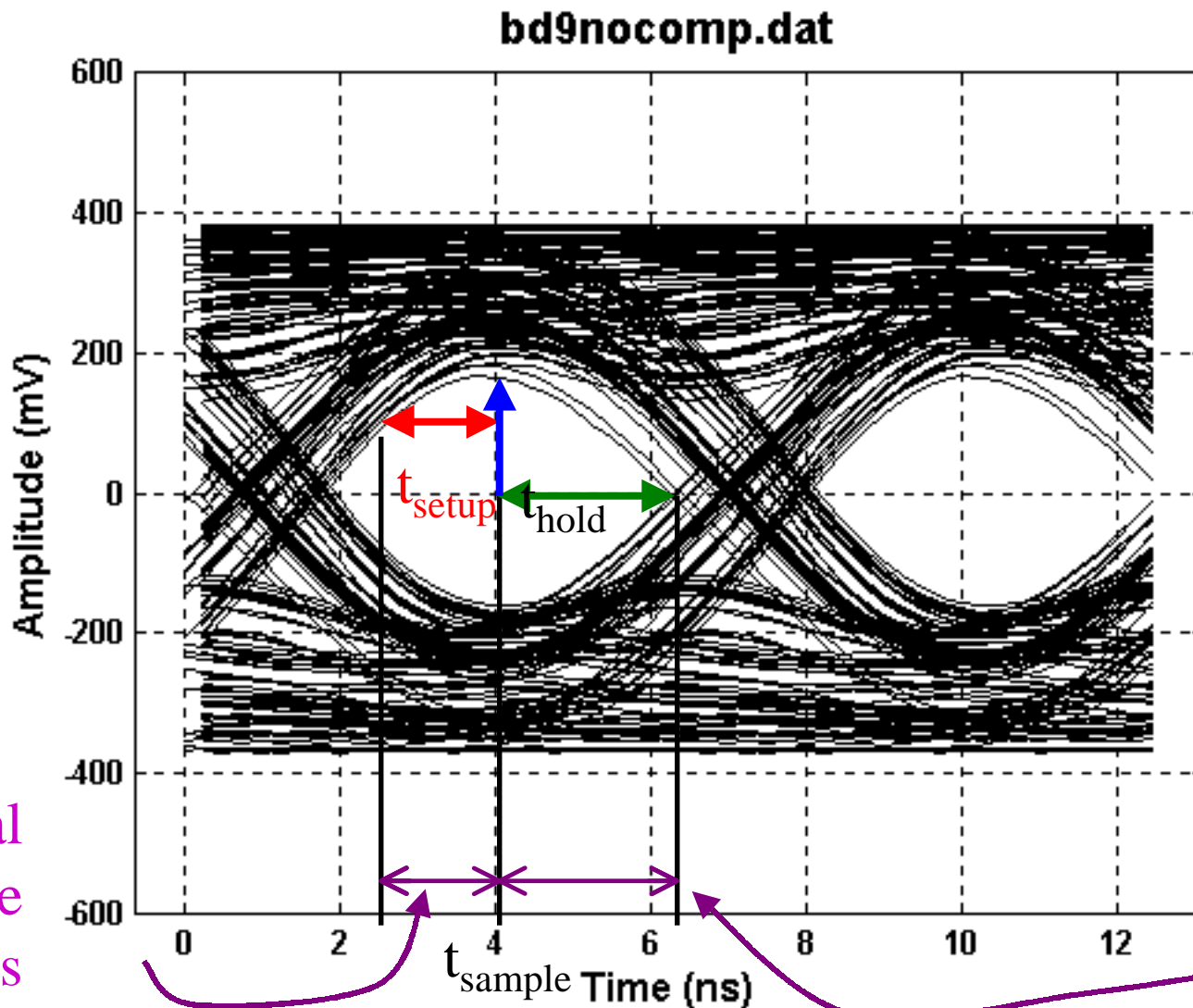
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- Waveforms captured @ 4Gs/s:
  - no pre-comp:  $\Delta A = 0.0$
  - amplitude pre-comp:  $\Delta A = 0.2, 0.5, 0.8$





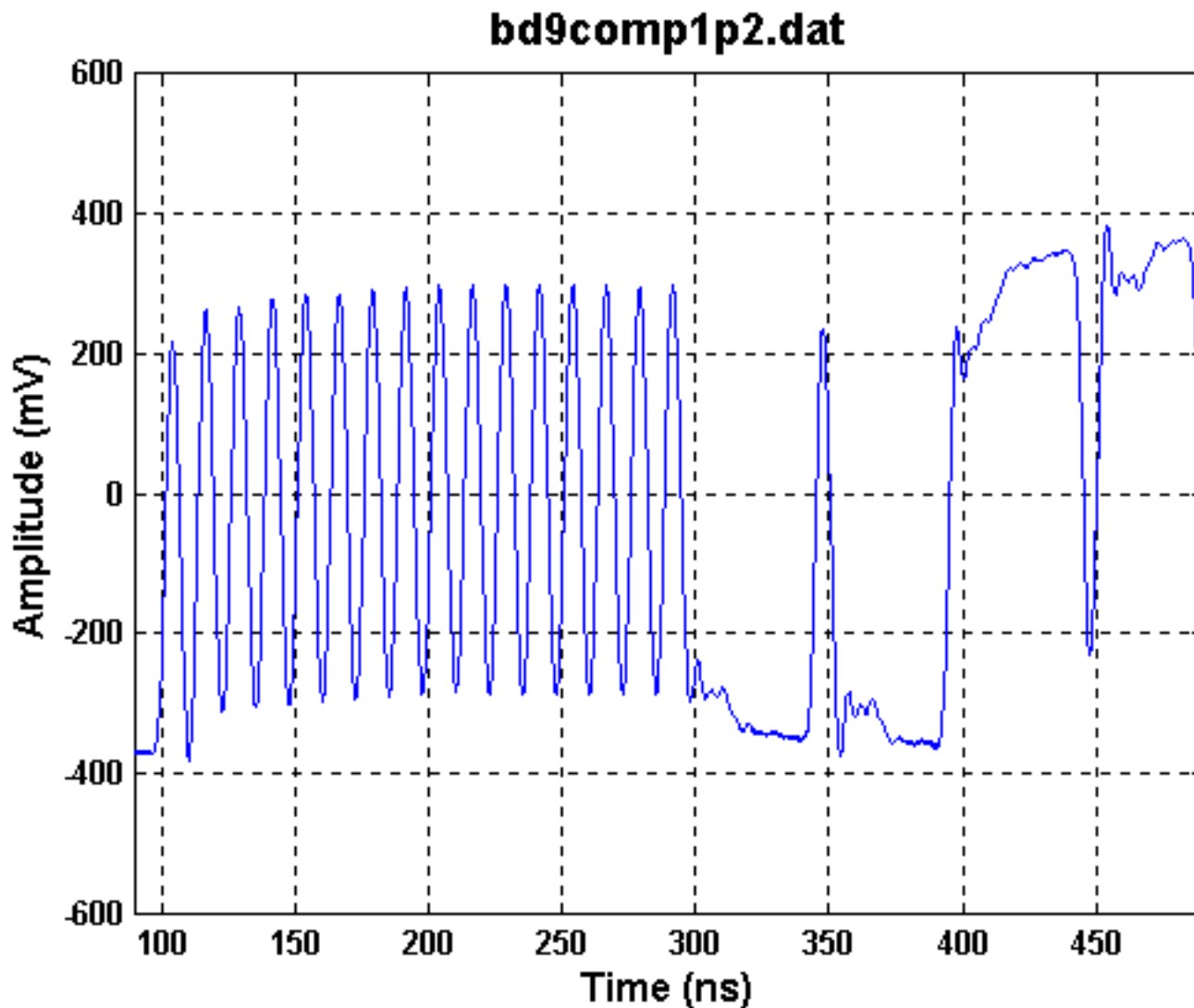


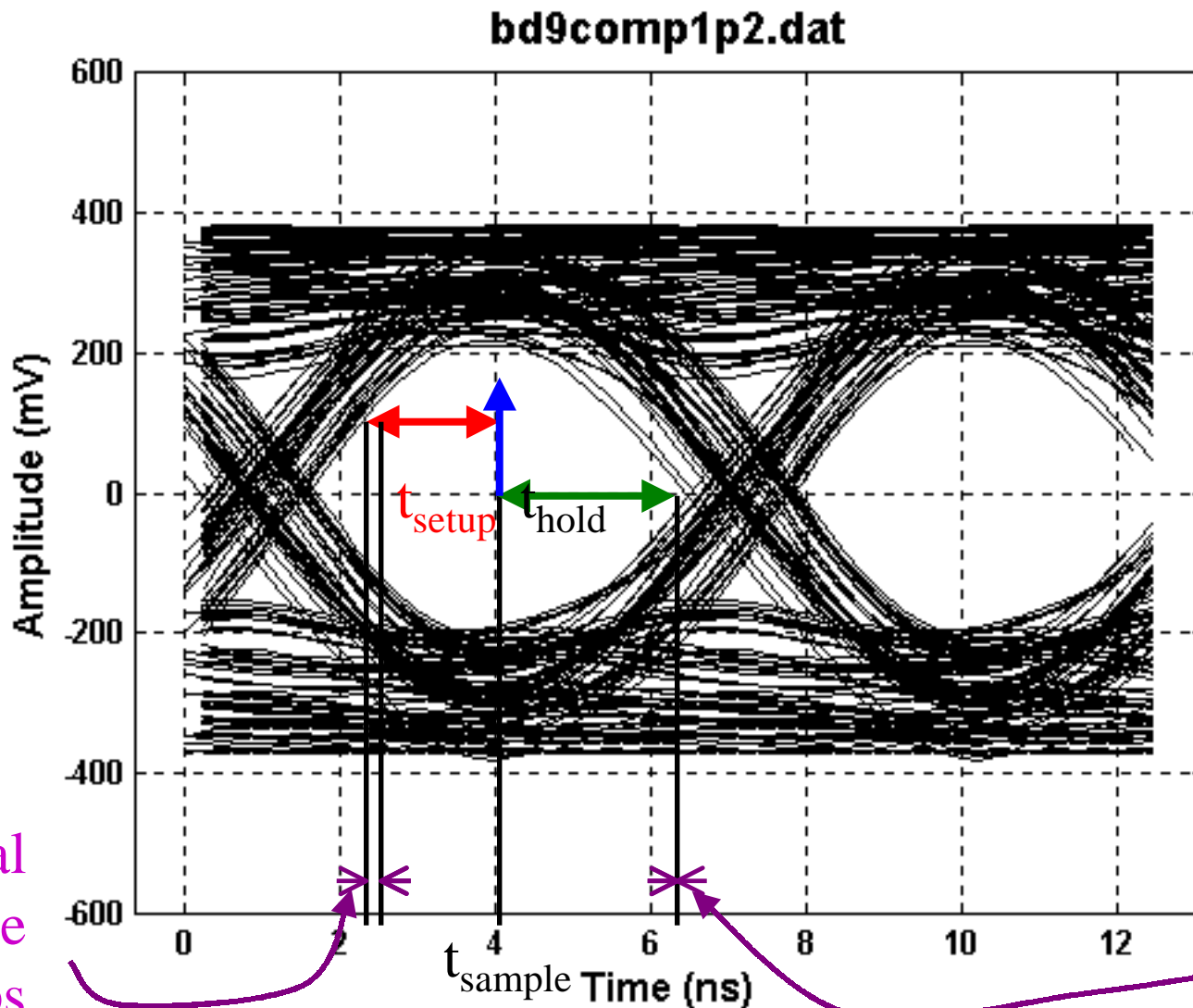




Nominal  
setup time  
~1.6ns

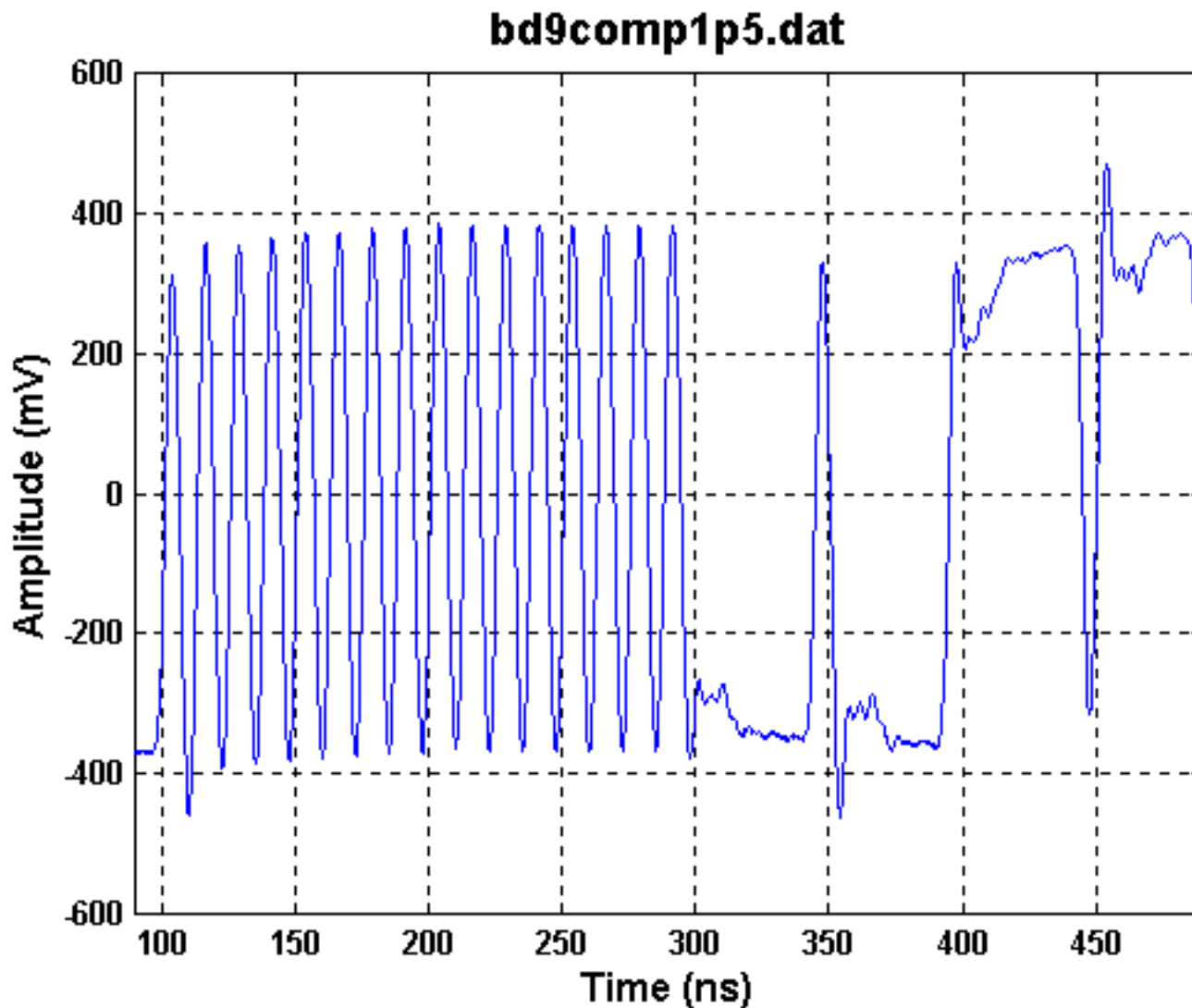
Nominal  
hold time  
~2.4ns

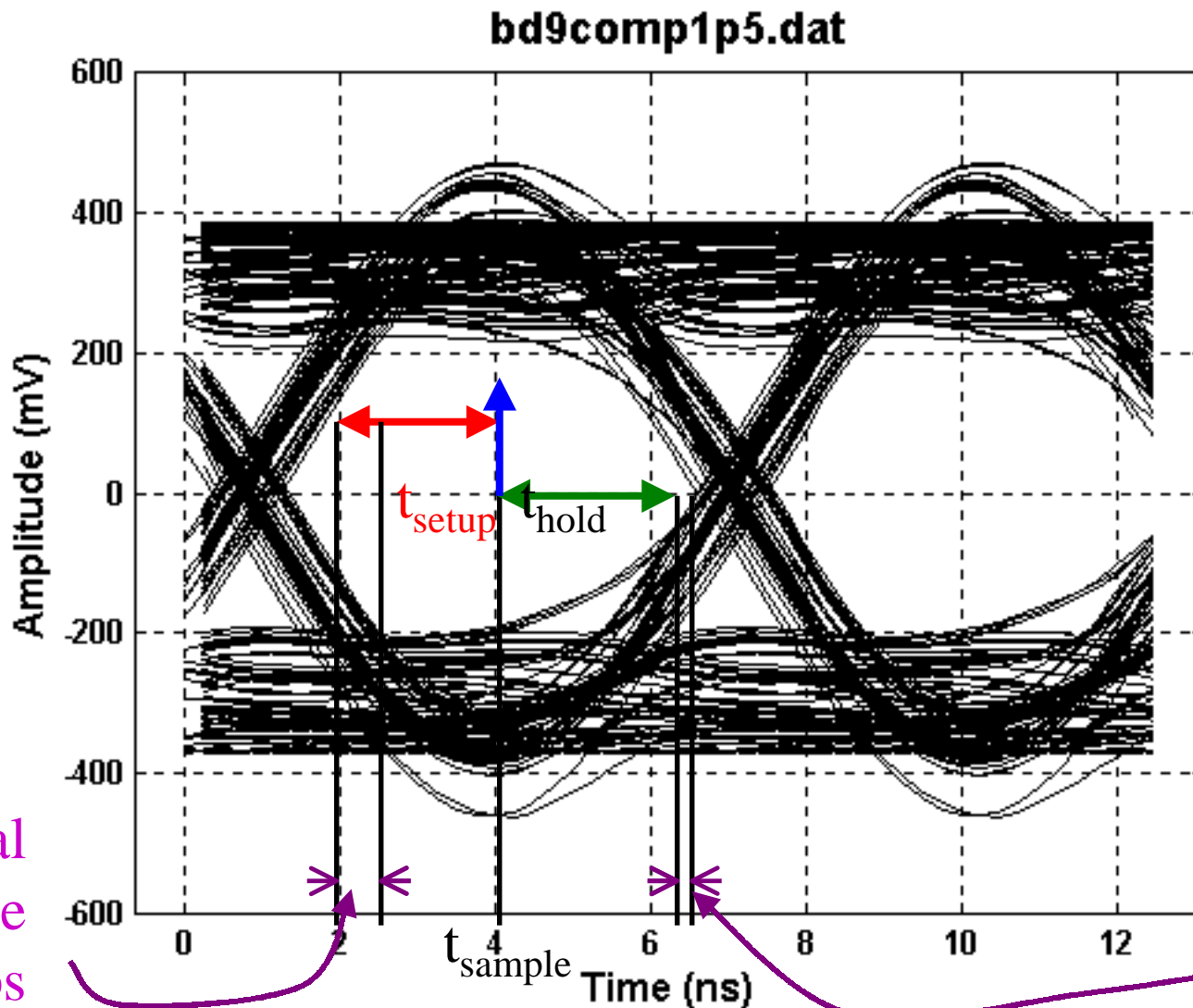




Additional  
set-up time  
~200ps

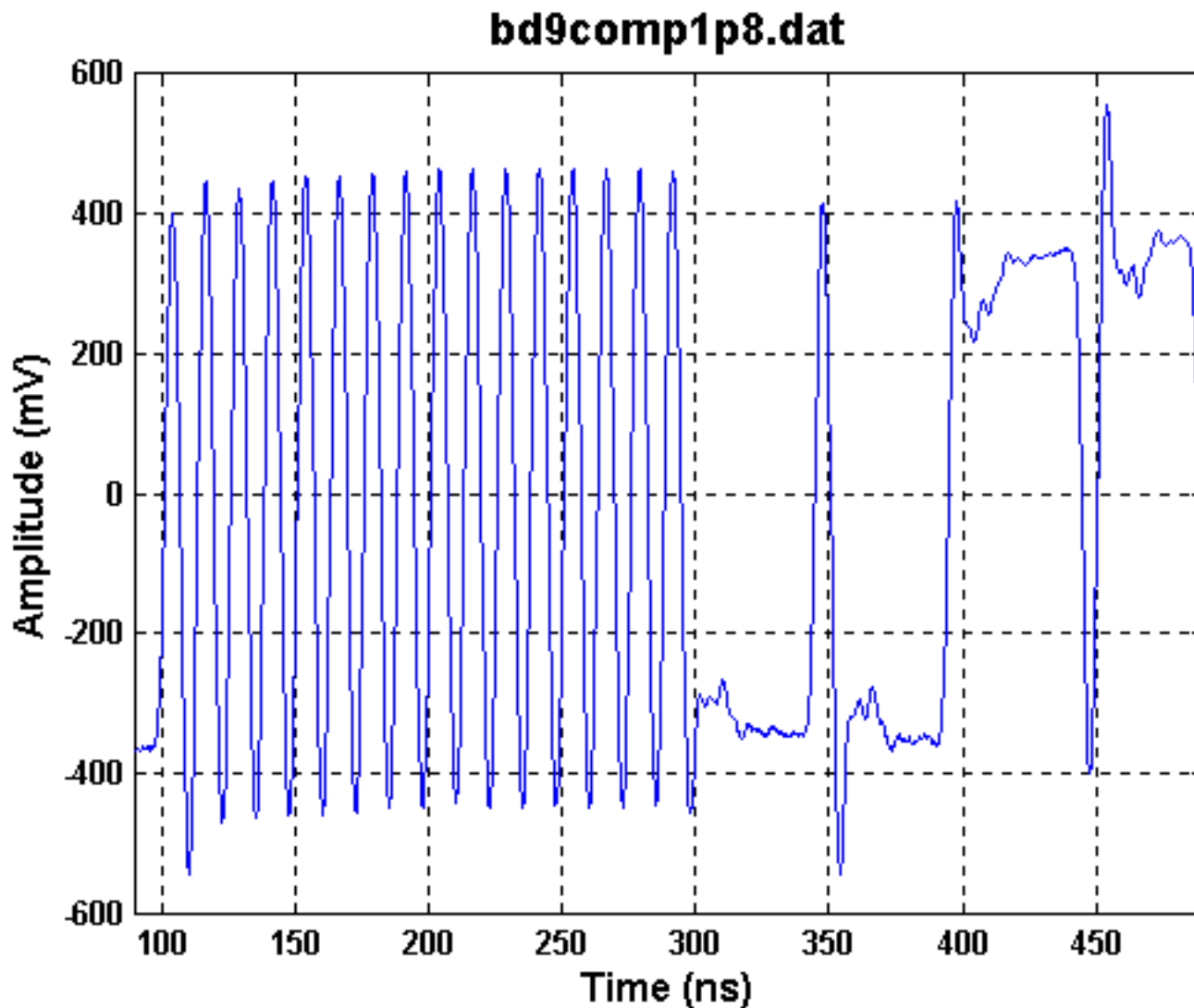
Additional  
hold time  
~0ps

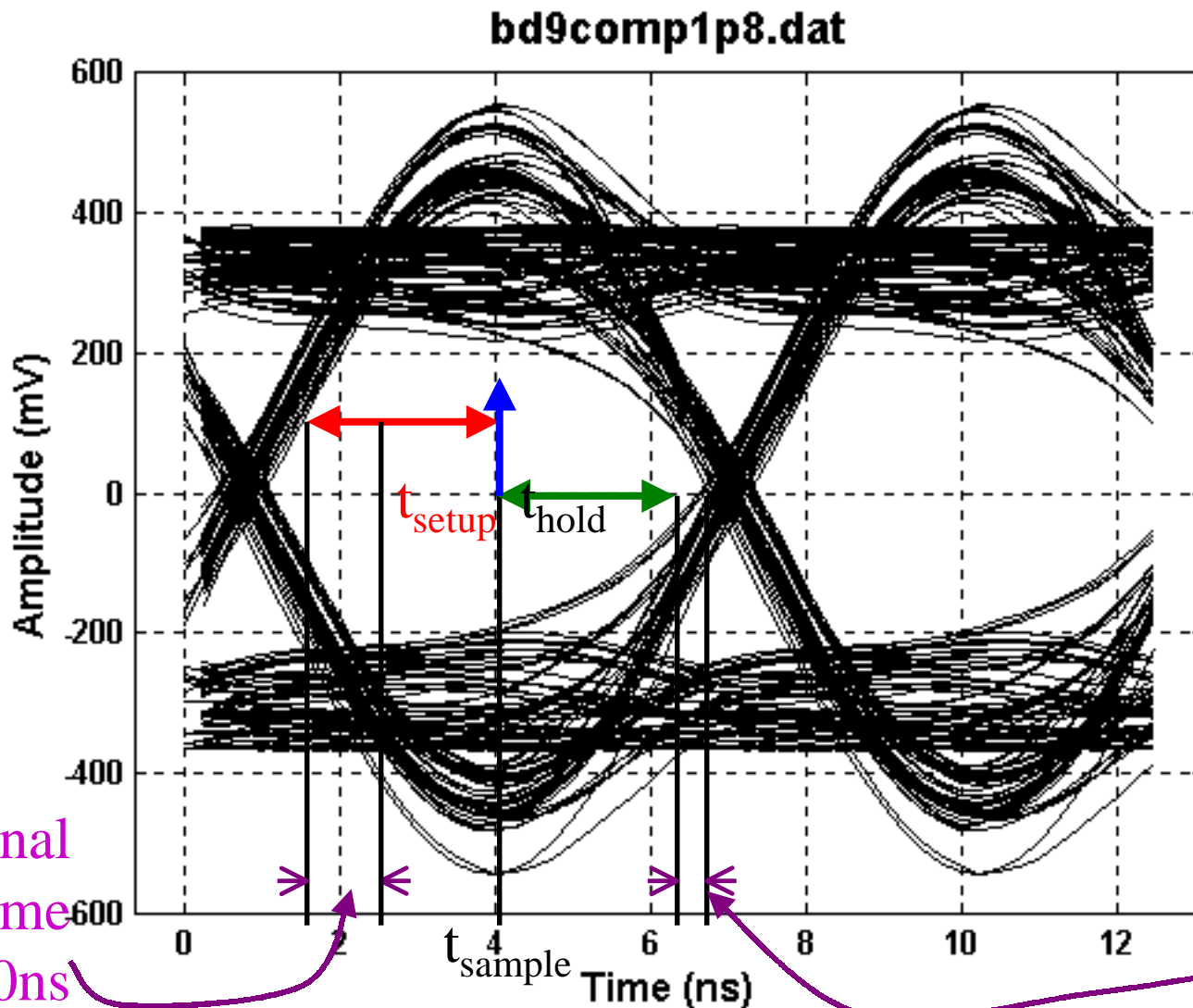




Additional  
set-up time  
~600ps

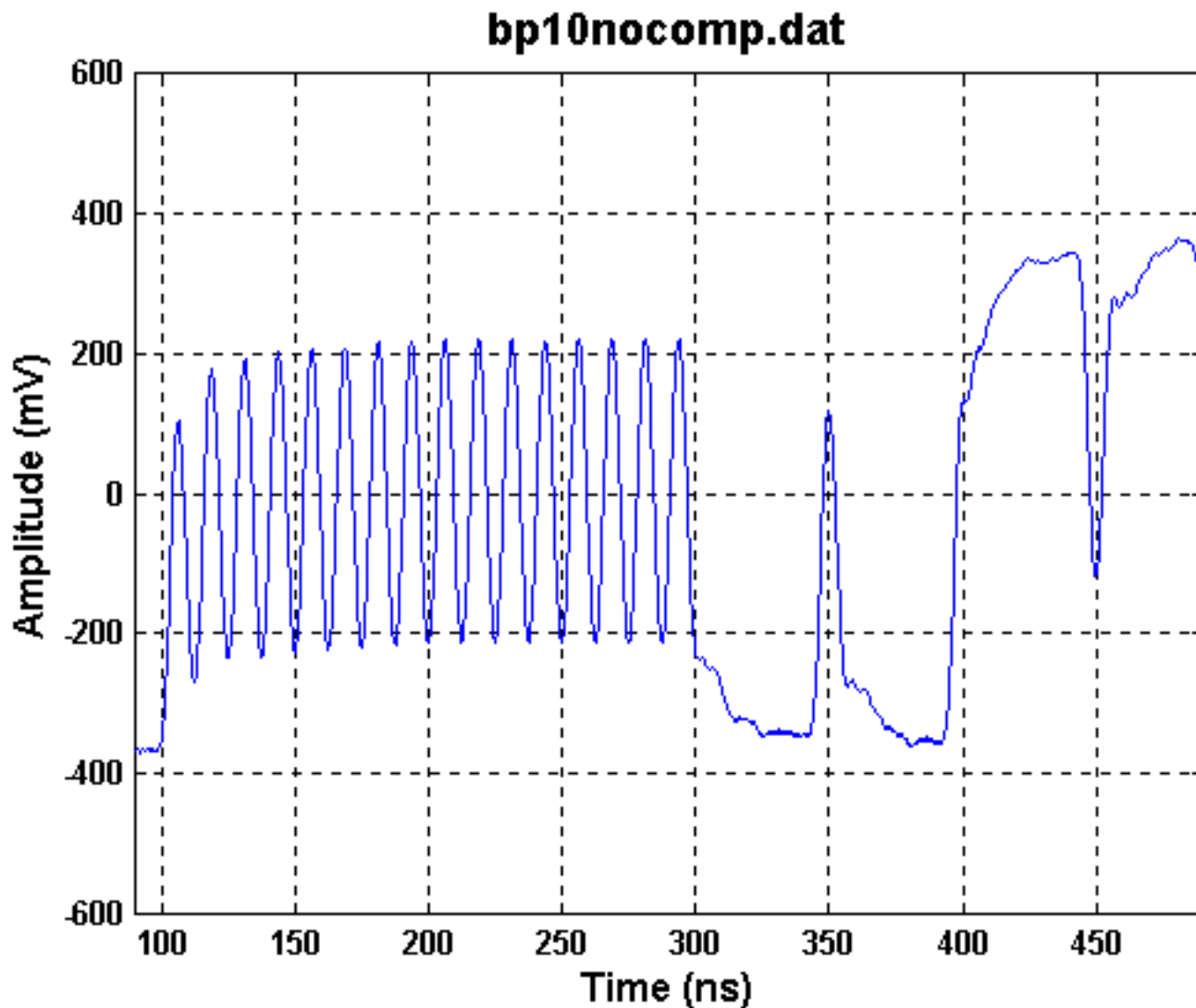
Additional  
hold time  
~200ps



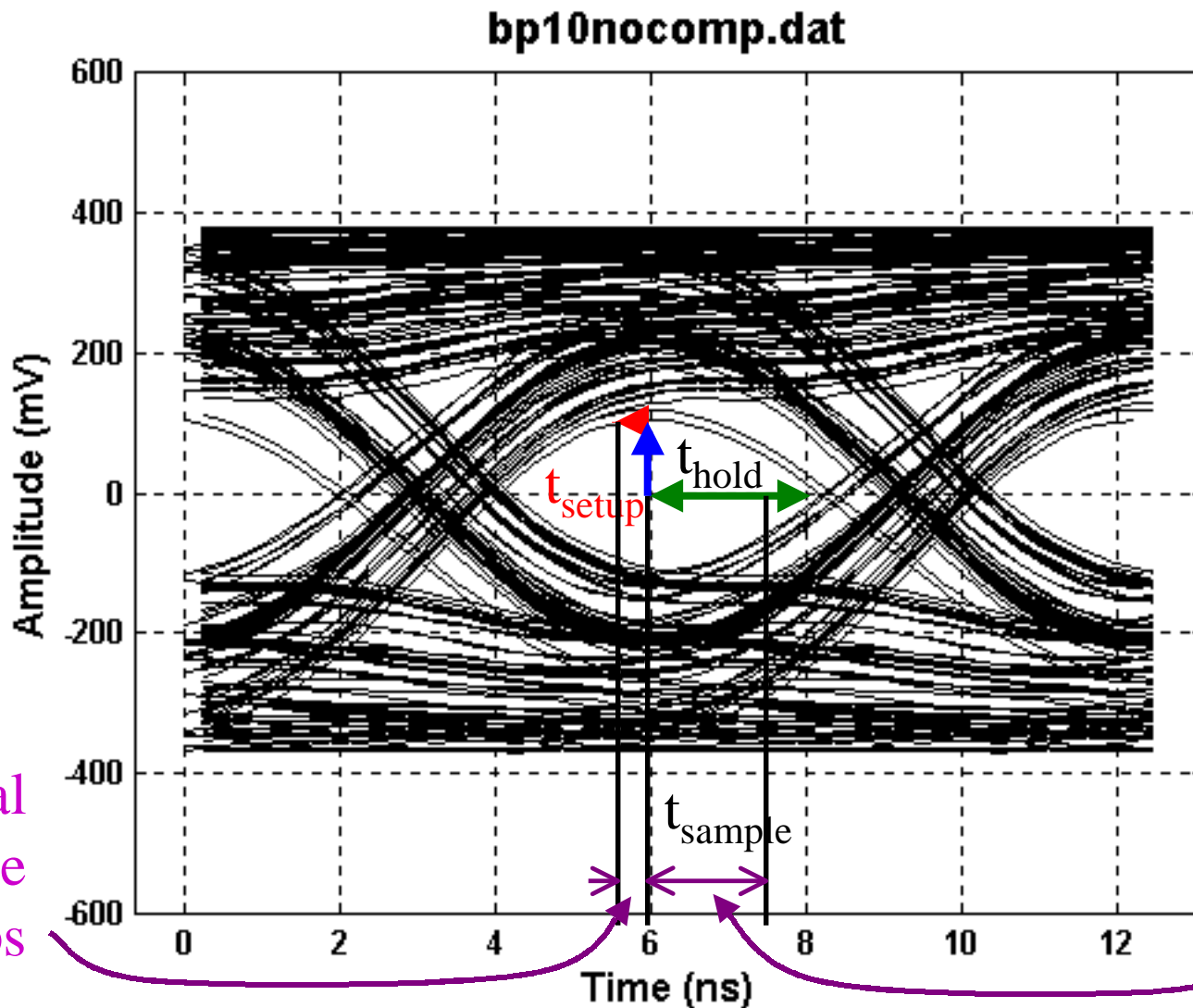


Additional  
set-up time  
~1.0ns

Additional  
hold time  
~400ps

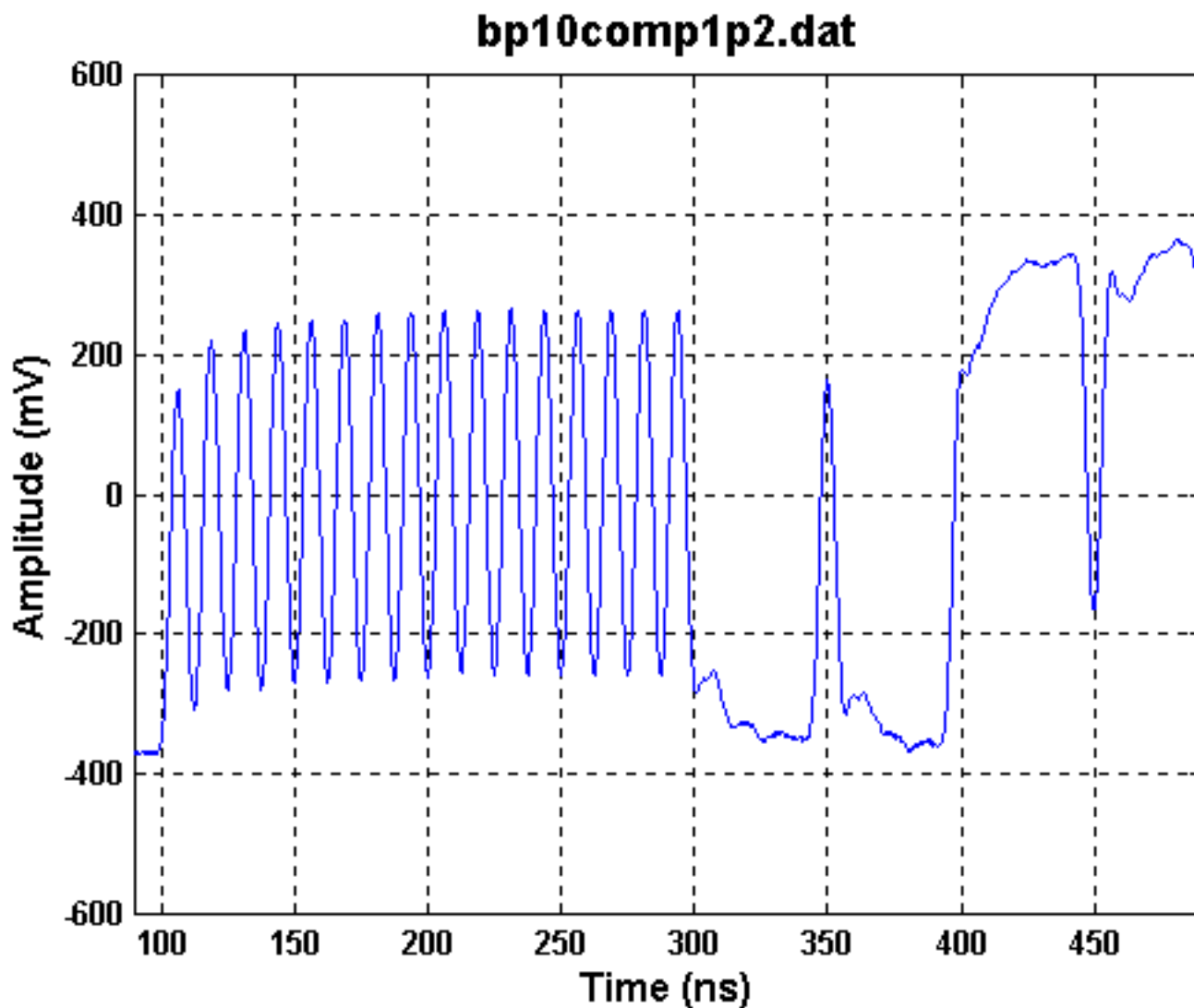


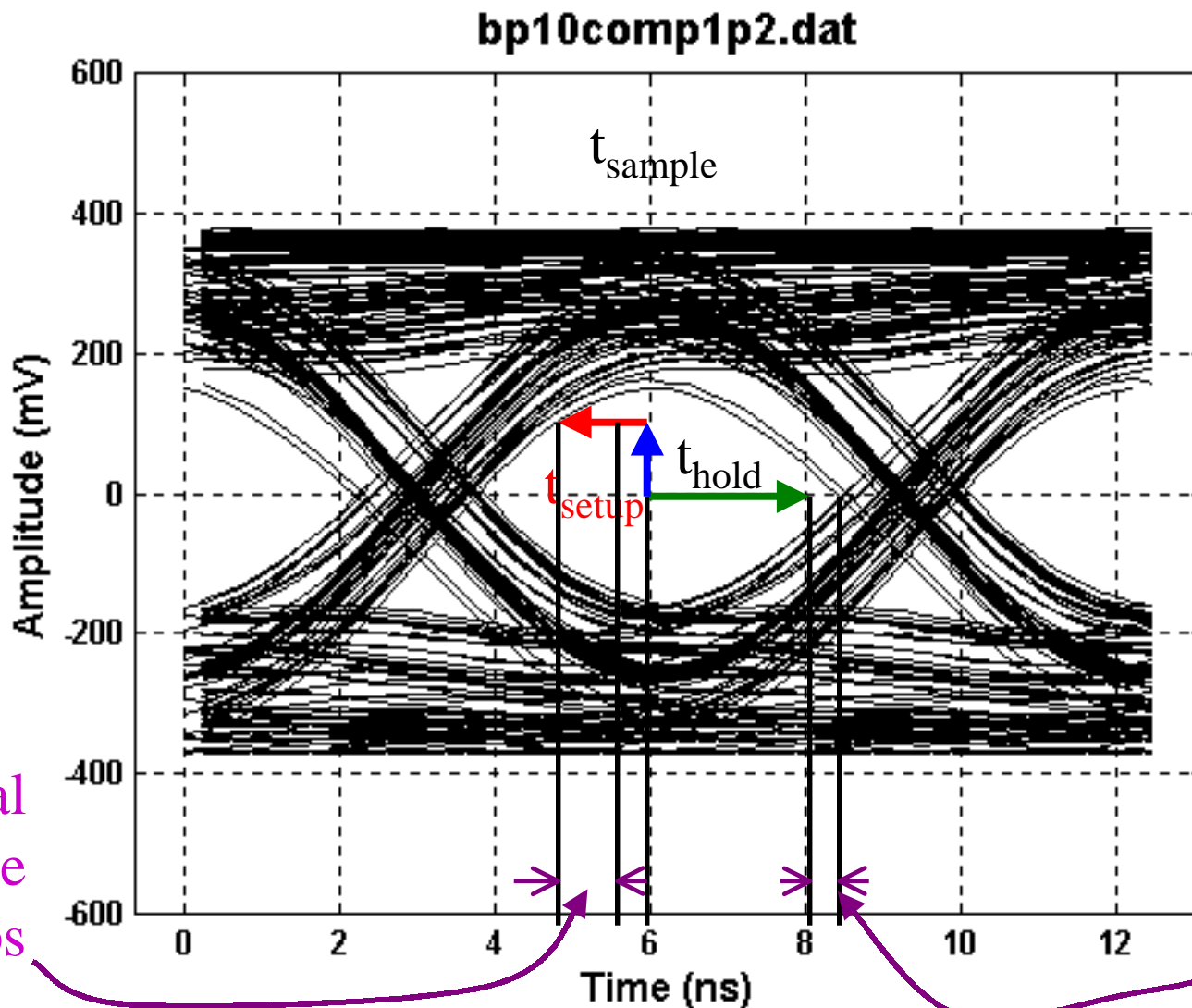


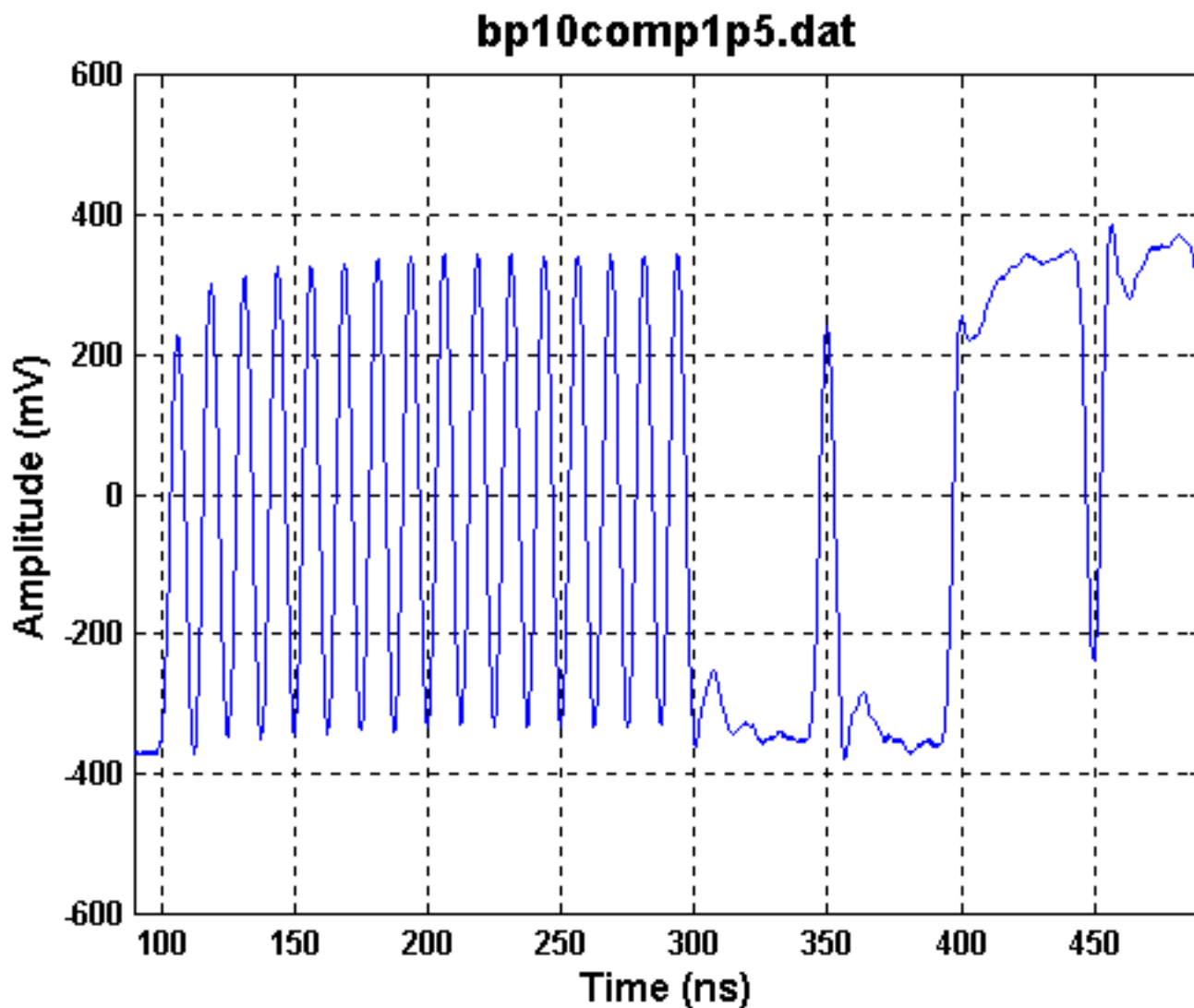


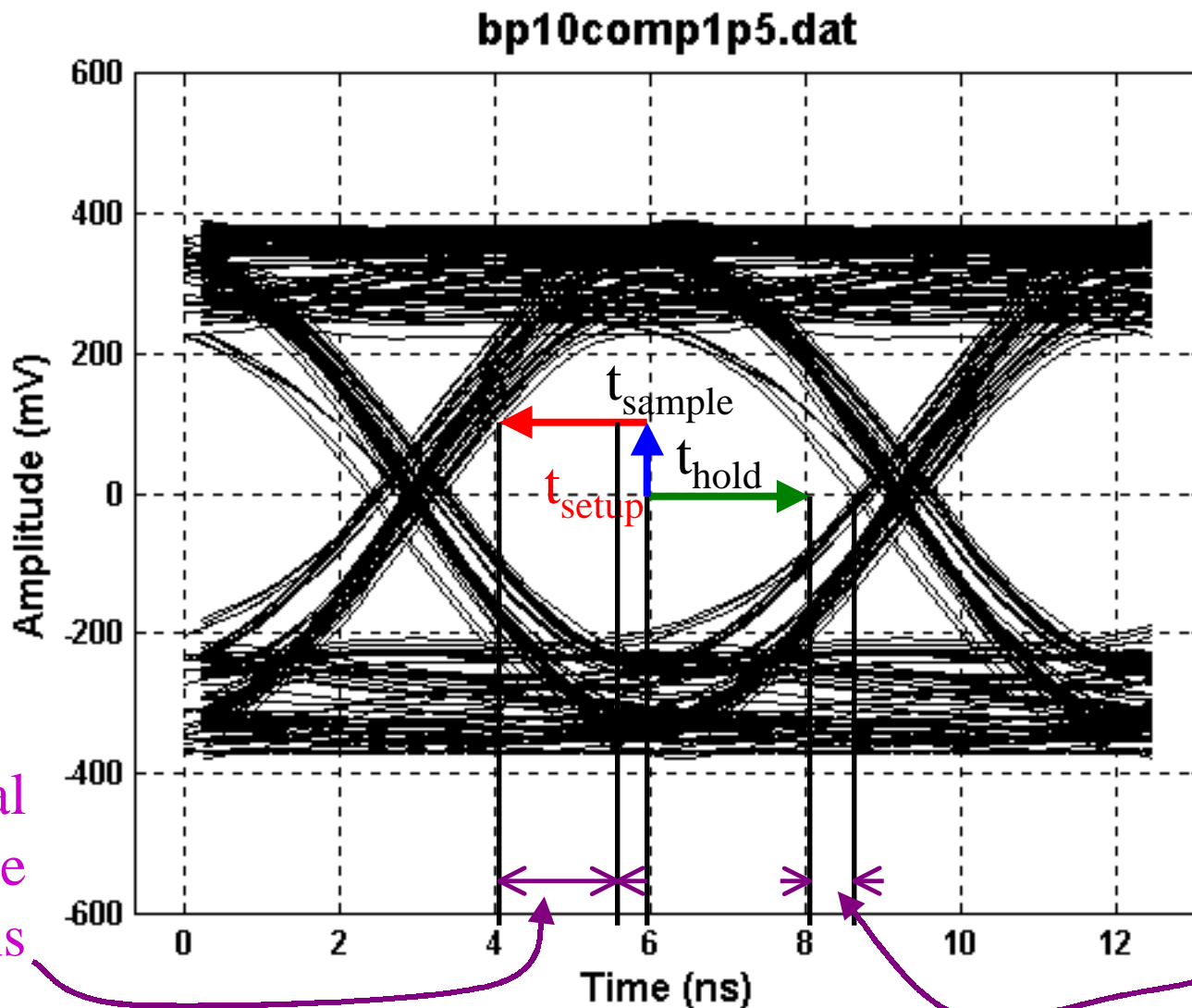
Nominal  
set-up time  
~400ps

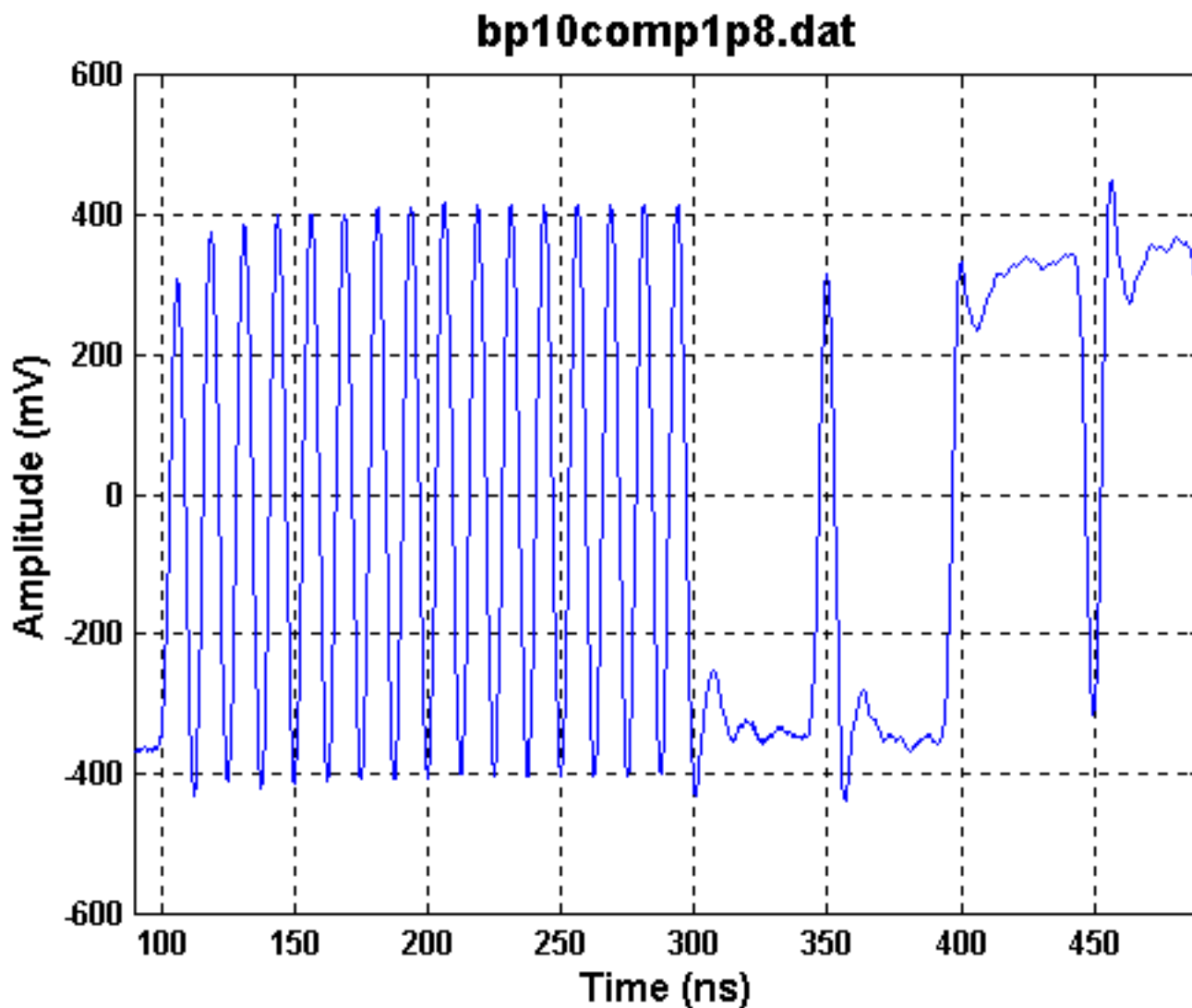
Nominal  
hold time  
~1.6s

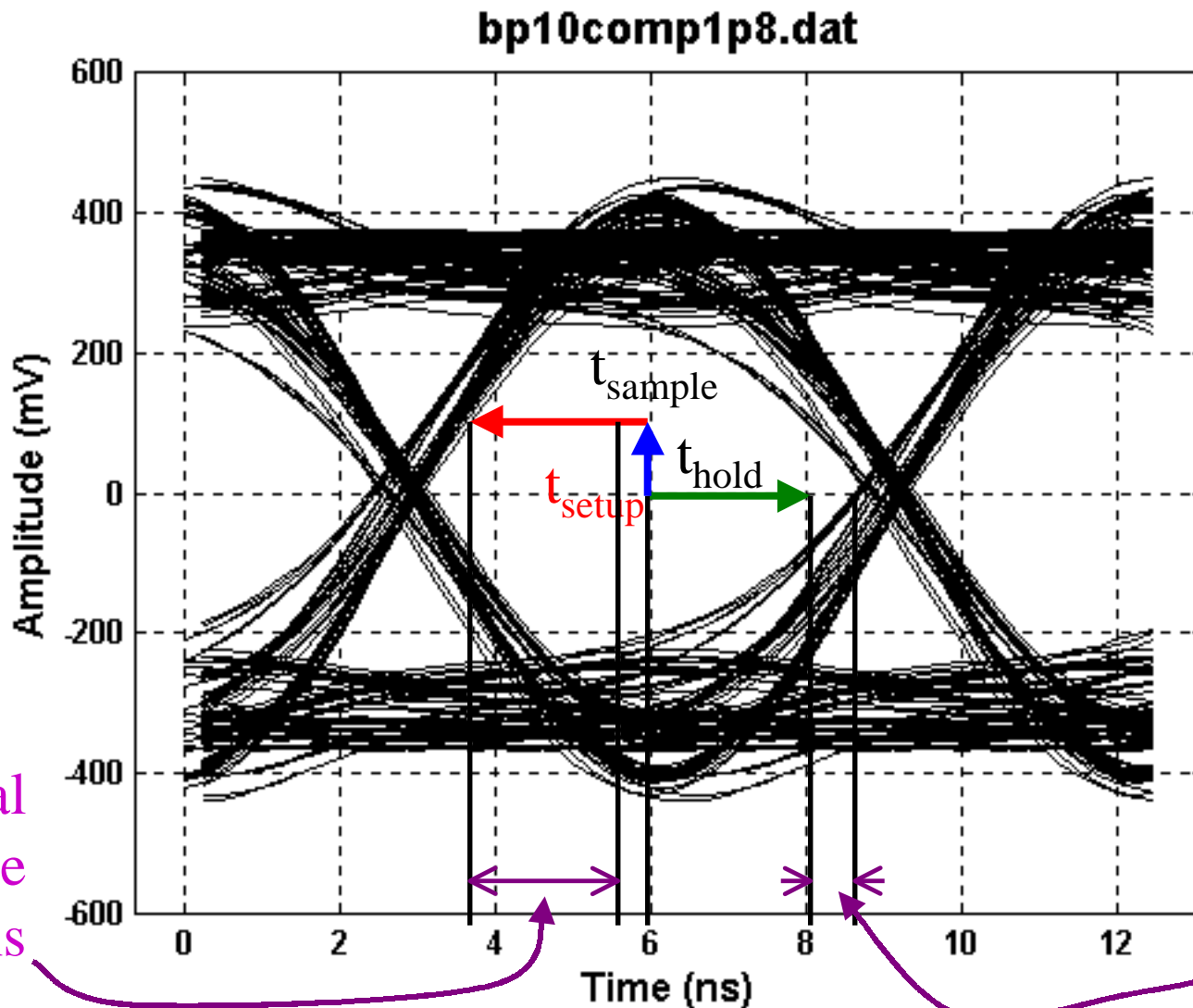




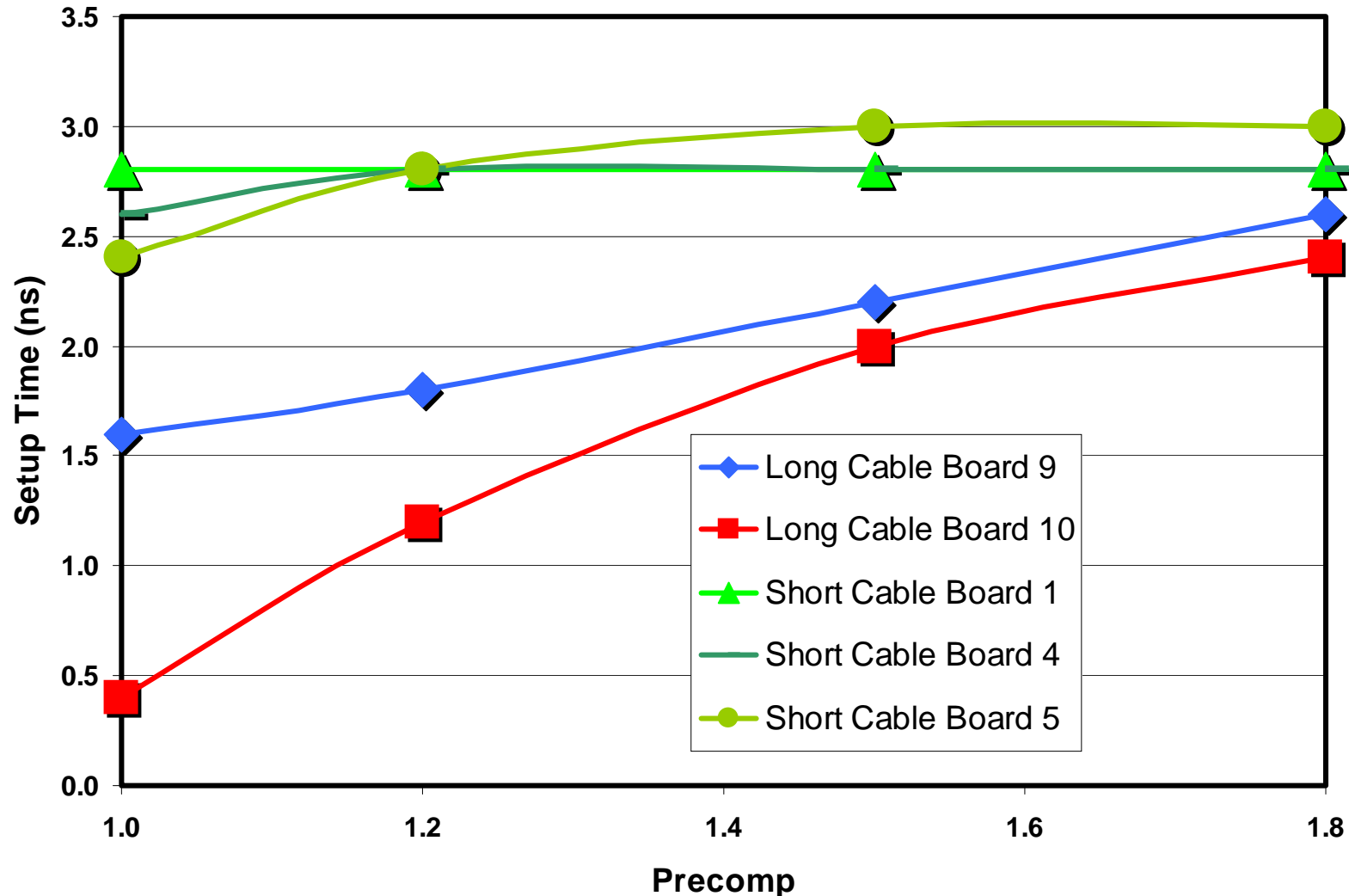






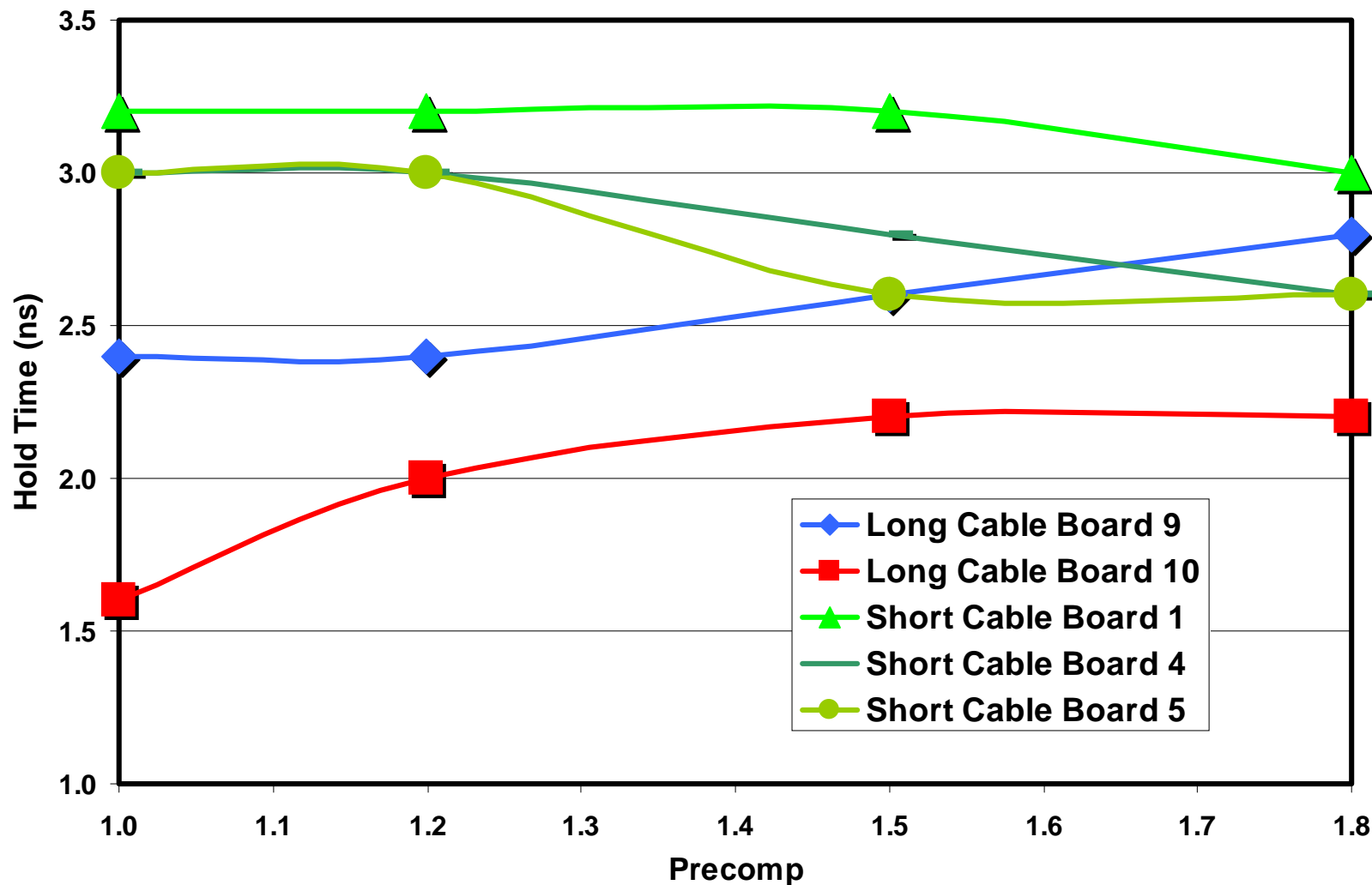


## Amplitude Precomp Vs Setup Time





## Amplitude Precomp vs Hold Time



<b>Timing Budget (ns)</b>	<b>.</b>
Basic Period	12.50
DT-Period	6.250
Period Tolerance	0.700
<b>Deterministic Errors</b>	<b>.</b>
Silicon TX Driver Skew	1.000
Package Skew (Initiator)	0.065
PCB Layout Skew (Initiator)	0.200
Cable Skew (@25ps/ft)	2.500
PCB Layout Skew (Target)	0.200
Package Skew (Target)	0.065
Silicon Rx Routing Skew	1.000
HL vs LH Matching	0.500
<b>Non-Deterministic Errors</b>	<b>.</b>
Low Vt vs Substrate Noise	0.200
PLL Jitter	0.250
Cross Talk Induced Jitter	0.500
<b>Cable Period Distortion ISI</b>	<b>2.000</b>
Input Slew Rate Dependent Skew	0.200
Receiver Amplitude Dependant Skew	0.200
Self Cal Accuracy ( $\pm 100$ ps)	0.200
<b>Data Valid Window</b>	<b>1.850</b>
<b>Data Setup/Hold</b>	<b>0.925</b>

- Amplitude pre-comp appears to work for long cables and for closely-spaced loads (i.e., set-up time improves, amplitude margin improves).
  - Without it (or something else) certain configurations will fail: zero set-up time, no amplitude margin.
  - Optimum value for pre-comp amplitude is between 1.5 and 1.8.
  - This value depends on the configuration.
- Amplitude pre-comp does not improve signal integrity for short cables:
  - Extra signal amplitude contributes to ringing and overshoot;
  - Amplitude pre-comp can even slightly decrease available hold time.
- Unsolved issues with EMI, Power, cross-talk, and capacitance.

- Data presented is for various pre-comp boost values over a 'low frequency' drive level of 400mV peak differential
- Driver and terminators are ideal
  - Other errors due to driver/terminator mismatch and interconnect resistance, requires an addition of approximately 70mV in the receiver margin above the 100mV in Figs 47,48 of SPI-3
- Only 1 line is driven, no cross-talk components are included
- Setup & hold measurements must include a timing error for residual skew.
- Transmit pre-comp appears able to meet the present interconnect configuration range, but:
  - fixed value of pre-comp is non-optimum at many drops
  - meeting the 12m / 15 drop configuration stresses available driver output signal capabilities
  - little or no range left to accommodate speed increase to 640

- Driver Issues for Amplitude Pre-comp
  - Data shows that a Pre-comp boost of 1.5 to 1.8 is required to handle 12m cable / 15 load case
  - Expect bus DC errors similar to U160
  - Expect cross-talk and reflection problems with pre-comp boost to be worse than with U160
    - **There is no reason to expect that a minimum (un-boosted) transmit signal lower than the 360mV min in SPI-3 is workable.**
  - Taking the SPI-3 360mV minimum, and +/-20% driver tolerance → 400mV nominal un-boosted level
  - 1.8x boost → 720mV nominal boosted level
  - + 20% driver tolerance → 864mV peak differential boosted signal
    - ***These signal ranges exceed the present SPI-3 min/max limits and will present driver design difficulties and increased power dissipation.***

- We will collect more data on different configurations:
  - heavily and lightly loaded busses
  - typical and atypical
  - point-to-point
- We will investigate:
  - can lower amplitudes be used to address large chip power requirements?
  - how bad will common-mode degrade for large amplitudes?
  - would receiver compensation work?
  - how much capacitance will be added by larger drivers?
  - how much capacitance is acceptable?
  - could we use a different terminator scheme?