

08-027r2

Toward SSC Modulation Specs and Link Budget

(Spreading the Pain)

Guillaume Fortin, Rick Hernandez & Mathieu Gagnon
PMC-Sierra



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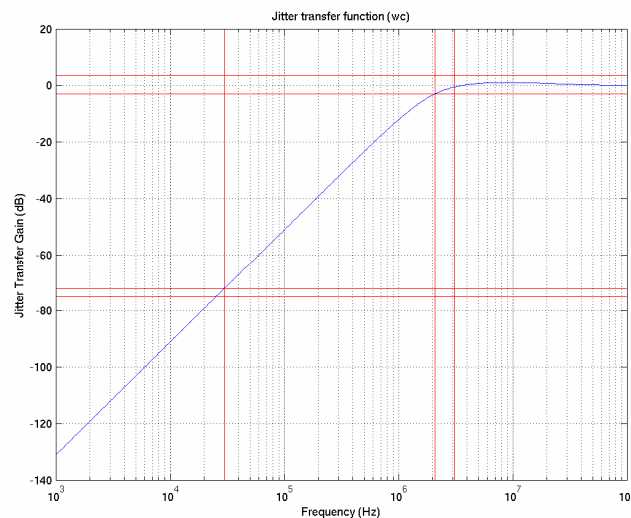
Note: additions or changes vs. previous versions are marked in blue.

The JTF as a model of CDR performance

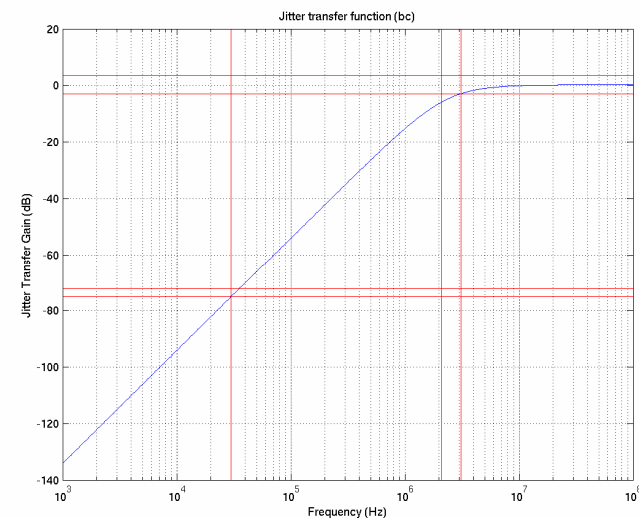
- When measuring jitter on the transmitter signal, the main objective should be to verify that this jitter is low enough to guarantee a robust link.
- Applying the jitter transfer function (JTF) on the transmitter jitter removes jitter components.
- The underlying assumption is that the jitter components that are removed do not impact link robustness
 - In other words, *the JTF represents the assumed performance of a CDR in a SAS-2 system.*

Using the JTF to qualify SSC modulation

- Use the JTF to calculate the residual SSC jitter seen by a baseline SAS-2 CDR
- Simulate with worst-case and best-case matlab models of the JTF



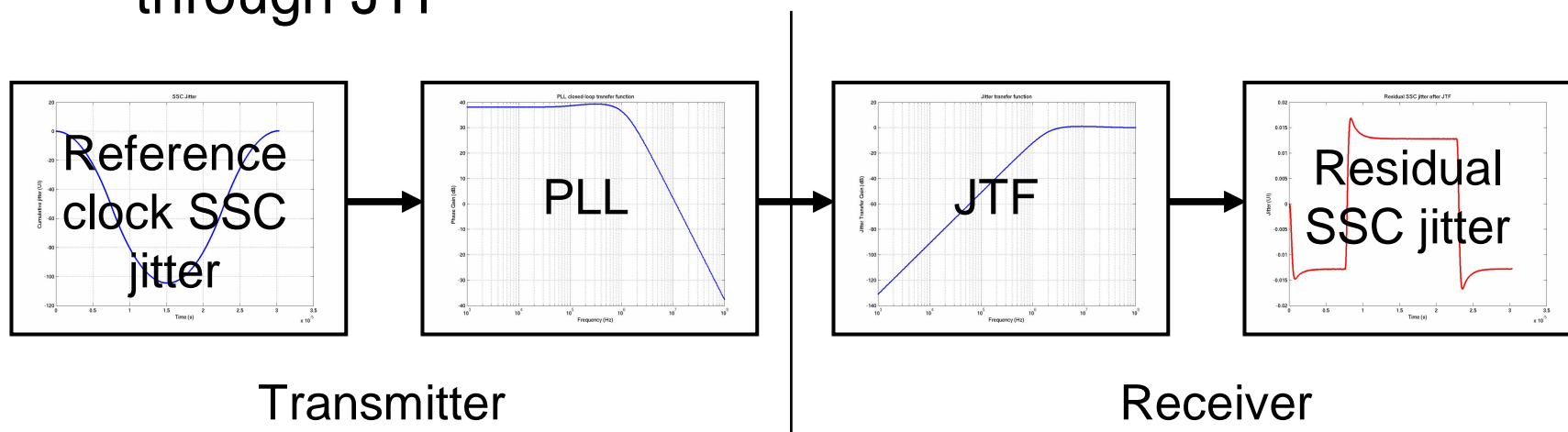
Worst-case JTF (-72dB @30kHz)



Best-case JTF (-75dB @30kHz)

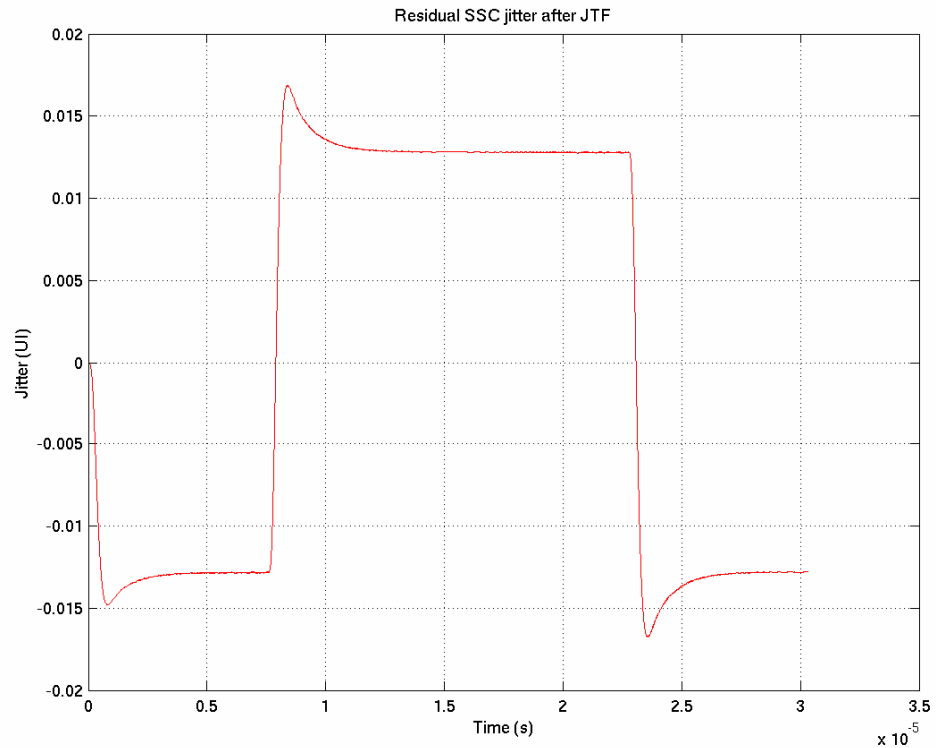
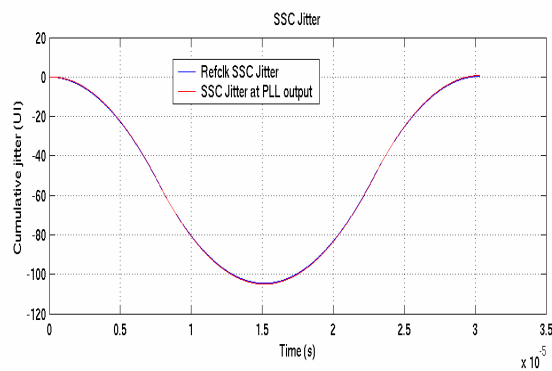
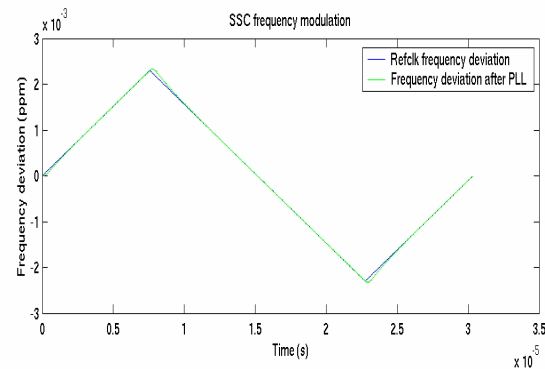
Simulation Methodology

- Created SSC jitter profiles for Triangular, Hershey Kiss and Square Wave modulations.
- SSC-modulated 75MHz reference clock is passed through PLL with $\sim 1.2\text{MHz}$ bandwidth, 40dB/decade roll-off and $\sim 1.3\text{dB}$ peaking.
- Residual jitter is obtained by passing SSC jitter through JTF



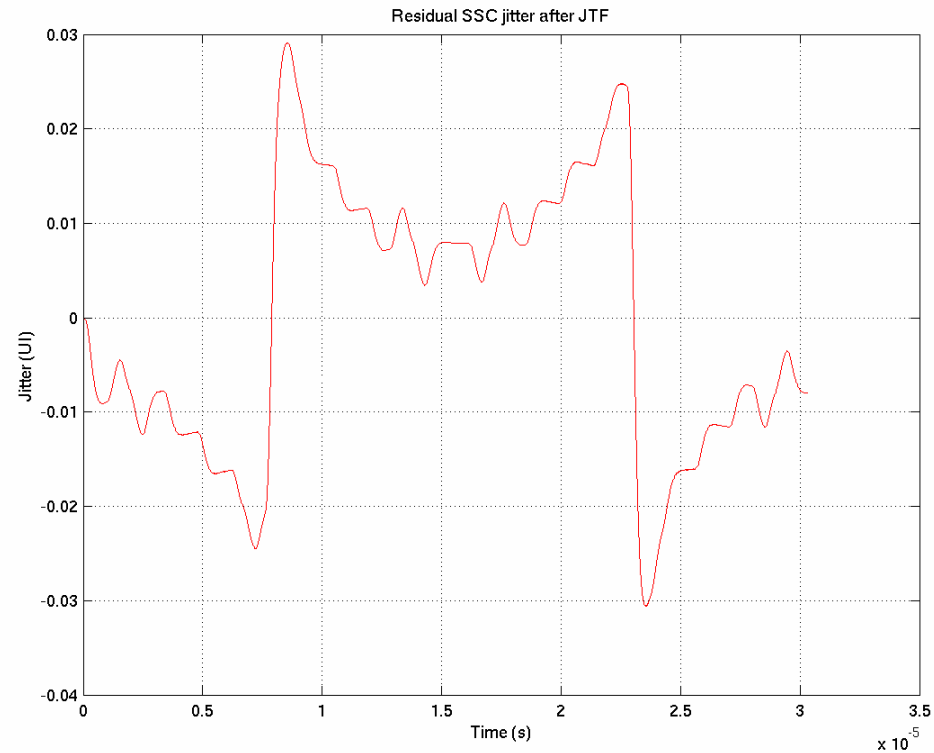
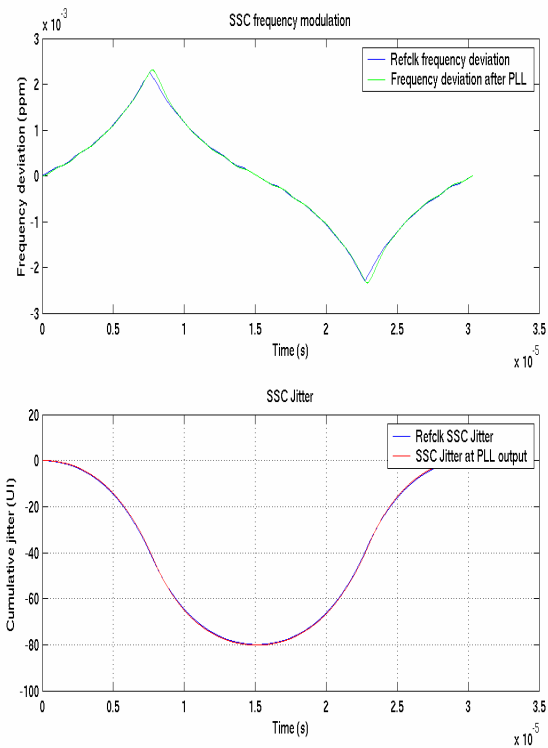
Triangular SSC Frequency Modulation and Jitter

- Results for worst-case JTF with triangular modulation



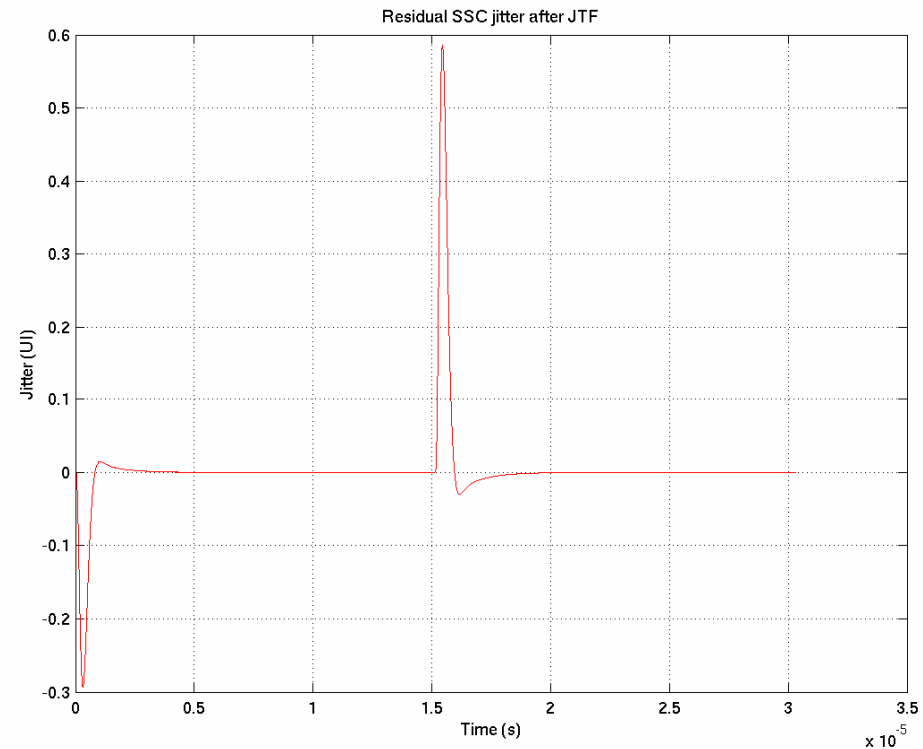
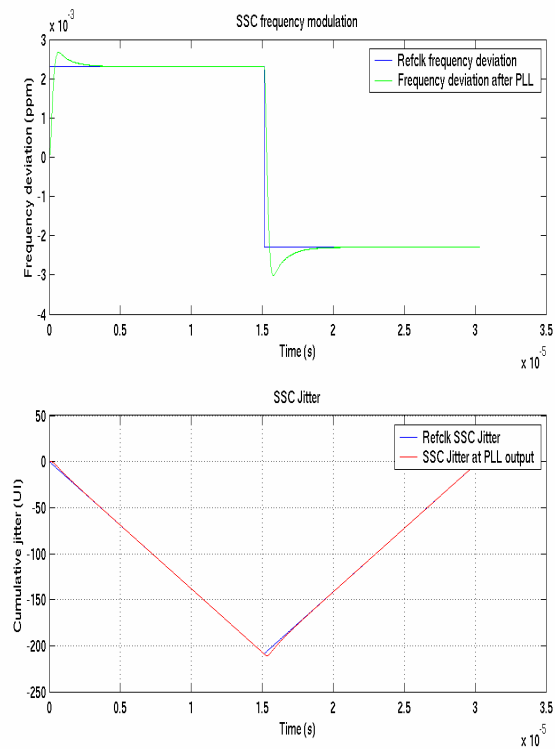
Hershey Kiss SSC Frequency Modulation and Jitter

- Results for worst-case JTF with HK modulation



Square Wave SSC Frequency Modulation and Jitter

- Results for worst-case JTF with square modulation

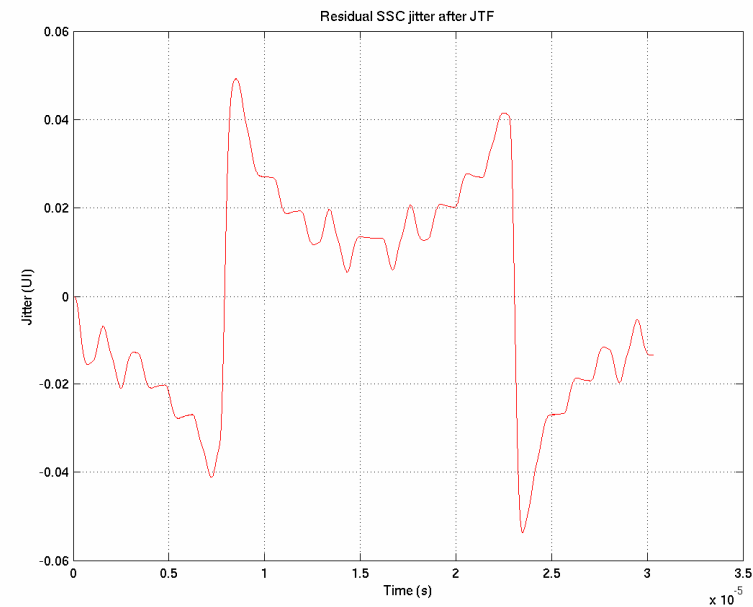
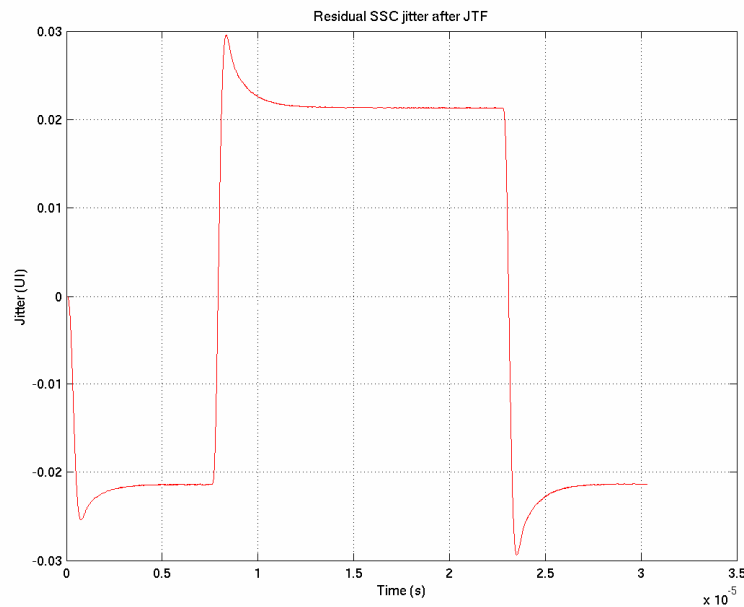


Limitation of the JTF as CDR model

- According to the 6G PHY spec (07-339r7), the JTF must be calibrated using D24.3 pattern (110011...). This corresponds to a transition density of 0.5.
- When testing with CJTPAT, the transition density drops to 0.3 in the long low frequency sequences (repeated D30.3)
- In most CDR architectures, gain is proportional to the transition density
 - A CDR that matches the JTF response with D24.3 will have its gain reduced by 40% when receiving D30.3
 - SSC residual jitter will increase by ~70% for CJTPAT

Limitations of the JTF as model of CDR

- Impact of reduced gain on CDR residual jitter
 - Residual jitter increases by 70% pattern density of 0.3
 - Illustrated for triangular and Hershey Kiss modulations



Residual SSC Jitter Summary

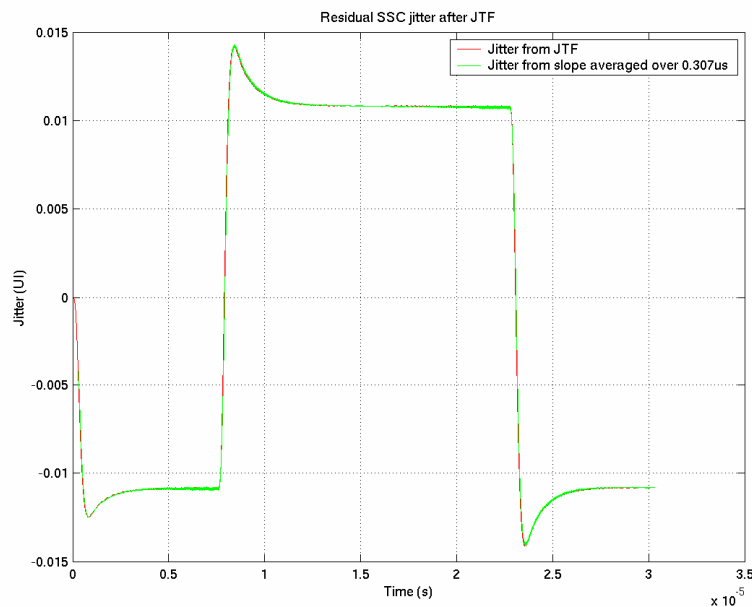
- Summary of SSC residual jitter results
 - When taking transition density into account, residual jitter from Hershey Kiss modulation eats up a fair part of the link jitter budget

Pattern	Peak-to-Peak Residual SSC Jitter (UI)		
	Best-case JTF	Worst-case JTF	Worst-case JTF with transition density = 0.3 (to emulate CDR with CJTPAT)
Triangular	0.024	0.034	0.059
Hershey Kiss	0.043	0.061	0.107
Square Wave	0.82	1.17	2.02

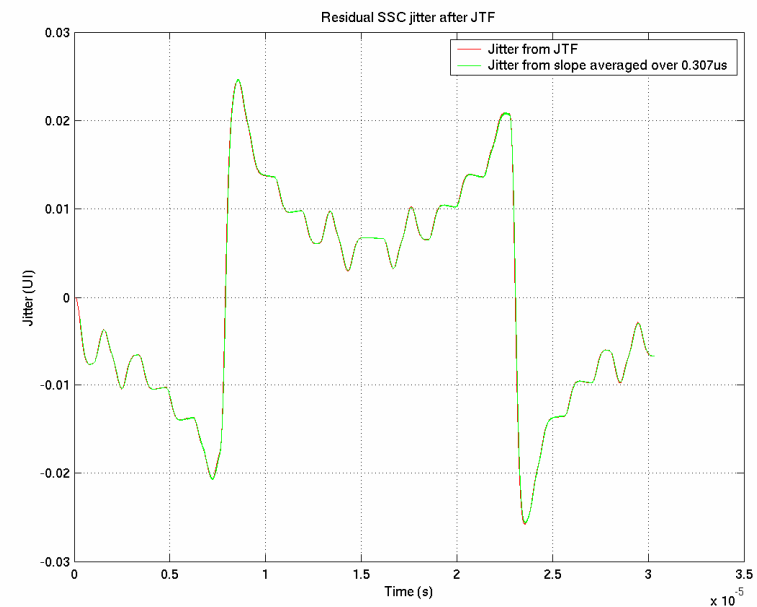
**Should we change the JTF
to reflect CDR performance with a worst-case pattern?**

Value of Residual Jitter From SSC Slope (2)

- Comparing residual jitter for Triangular and Hershey Kiss SSC profiles
 - Response from typical JTF with $f_c=2.6\text{MHz}$ and -73.5dB gain at 30kHz (red)
 - Response from frequency deviation rate (slope) averaged over $0.307\mu\text{s}$ (green)



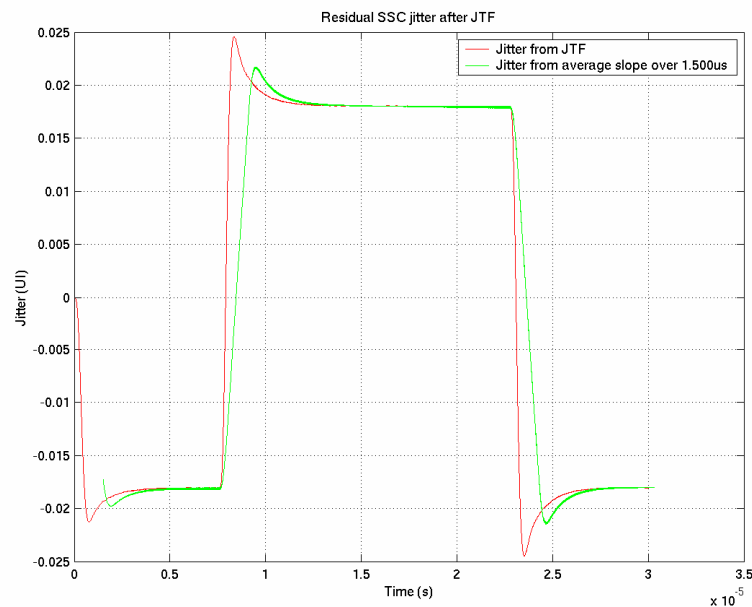
Residual Jitter from Triangular SSC Profile



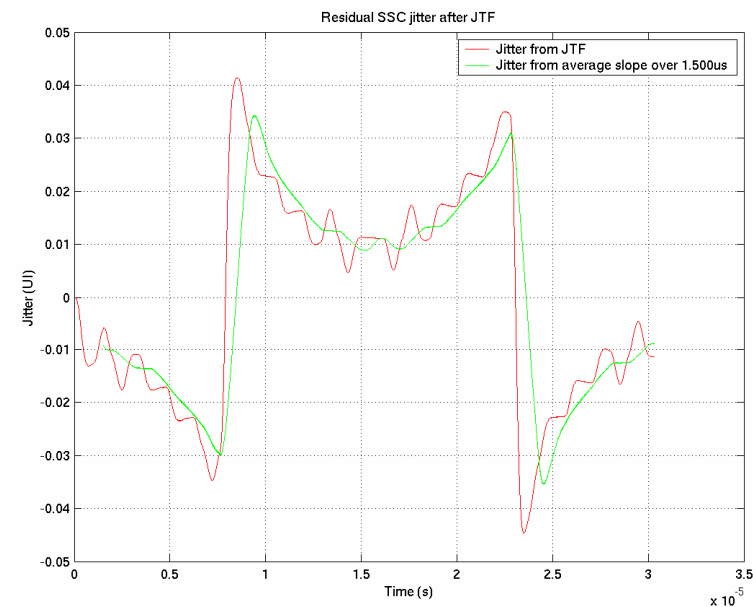
Residual Jitter from Hershey Kiss SSC Profile

Value of Residual Jitter From SSC Slope (3)

- Using the average slope over 1.5 μ s underestimates residual jitter by 10% to 20% for triangular and Hershey Kiss patterns
 - Response from typical JTF with $f_c=2.6$ MHz and -73.5dB gain at 30kHz (red)
 - Response from frequency deviation rate (slope) averaged over 1.5 μ s (green)



Residual Jitter from Triangular SSC Profile



Residual Jitter from Hershey Kiss SSC Profile

Tentative Link Budget For Discussion (1)



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- Definition of Terms
 - Data Dependent Jitter (DDJ): Inter-Symbol Interference
 - Non-Compensable Jitter (NCJ): jitter that cannot be corrected by the receiver
 - Data Dependent Non Compensable Jitter: in this link budget, this is specifically the ISI that cannot be corrected by the SAS-2 reference receiver.
 - Since the SAS-2 reference receiver is a 3-taps DFE, this corresponds to ISI from the pre-cursor taps as well as all post-cursors taps after and including the 4th.
 - It is split from the rest of the non-compensable jitter since it can be controlled by changing tx pre-emphasis.

Tentative Link Budget For Discussion (2)

- How much SSC jitter is too much jitter?

	Source Transmitter & PLL	Reference Channel	Target Receiver & PLL	Total	Comments
Random Jitter (RJ)	0.15		0.15	0.21	Total calculated as root sum of squares
Bounded Non-Compensable Jitter (BNCJ)	0.15	0.05		0.2	Includes: - Residual SSC jitter - Duty-cycle distortion - Periodic Jitter (from supply noise, etc.) - Crosstalk - Common-mode to differential conversion Excludes: - Data Dependent Jitter, which is accounted for on the next line
Data-Dependent Non-Compensable Jitter (DDNCJ)			0.3	0.3	ISI and reflections that can't be corrected by 3-taps DFE Simulated with stateye v5: - SAS-2 reference channel - 2dB pre-emphasis - No DJ or RJ - 8b10b encoding
Receiver Margin (RMJ)			0.3	0.3	Includes: - Samplers sensitivity - Quantization effects - Device mismatches
Total Jitter	0.3	0.35	0.45	1.01	

Note: Transmitter jitter measured at near end

Tentative link budget considerations

- Is 0.05 UI (8 ps) a good number for channel non-compensable jitter (BNCJ)?
 - Crosstalk
 - Common-mode to differential conversion
 - Reflections
- Is 0.30 UI (50 ps) a sufficient margin for the receiver?
 - Should we tighten other specs for more receiver margin?
- Are the stateeye results reliable (071210 version)?
 - With 0.2UI DJ and 0.21UI/17 RJ, total far end jitter only adds up to 0.64UI instead of 0.71UI (for 2dB and 3 taps)
- Can we gain margin by increasing pre-emphasis?

Tx Pre-Emphasis (dB)	DDNCJ for 3 taps DFE (UI)
0	0.3
2	0.3
3	0.29
6	0.29
9	0.22

Tentative SSC Specifications

- CDR considerations
 - SSC modulation shall not exceed the +/-2300ppm range
 - The slope of the frequency deviation shall not exceed 610ppm/ μ s when averaged over any 0.3 μ s (\pm 0.01 μ s) window of the SSC modulation profile
 - This limit is based on a maximum residual jitter of 0.075UI for a nominal JTF (fc=2.6MHz, gain(30kHz)=-73.5dB) that has its gain scaled by 60% to emulate the effect of a pattern density of 0.3 on a typical CDR
 - This limit excludes the Hershey Kiss profile for modulation magnitudes in excess of \pm 2000ppm
 - SSC modulation shall not cause the transmit jitter to exceed the jitter spec when filtered through the JTF
 - Activation or deactivation of SSC on an active link shall be done when the instantaneous frequency of the SSC profile is within 100ppm of the non-SSC modulated frequency. The jitter introduced by this transition shall meet the transmit jitter specifications when filtered through the JTF.
- Average frequency deviation due to asymmetry in the SSC profile shall be within 288 ppm
 - Based on max ALIGNs insertions/deletions in previous versions of SAS (1/2048) minus the max frequency offset between the local and far end crystals (200ppm)
- Average frequency deviation over any 16.67us period is not an issue
 - FIFO depth larger than 14 D-Words (~5600ppm)