



Epsilon Point Proposal T11/07-399v0

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Contributors and Supporters

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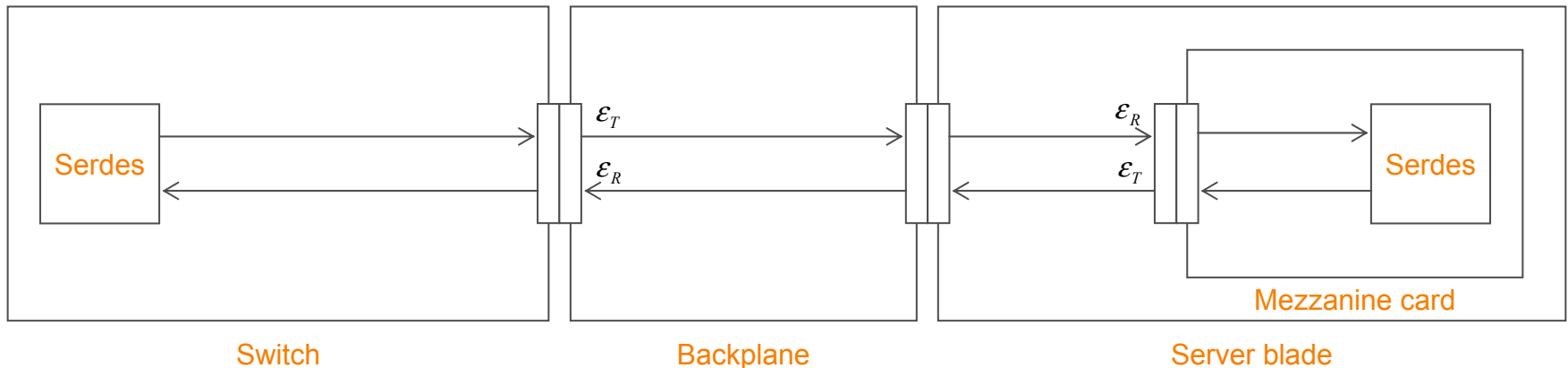
Executive summary

- Proposal defines the operation of 8.5 Gb/s Fibre Channel in the server blade environment
 - [Enhanced] TWDP-based transmitter device compliance methodology
 - [Enhanced] WDP-based receiver device signal tolerance input
 - Reference receiver with 1 feed-forward, 3 feedback taps (ie. A 3-tap DFE)
- Comprehensive channel analysis, loss and jitter budgets presented to support proposed specifications
- Relevant test procedures from SFF-8431, tailored to 8.5 Gb/s Fibre Channel applications, to be included in Annex A
 - Described in detail in companion document
- Additional detailed modifications to the FC-P1-4 draft also described in companion document T11/07-398v0.

Assumptions

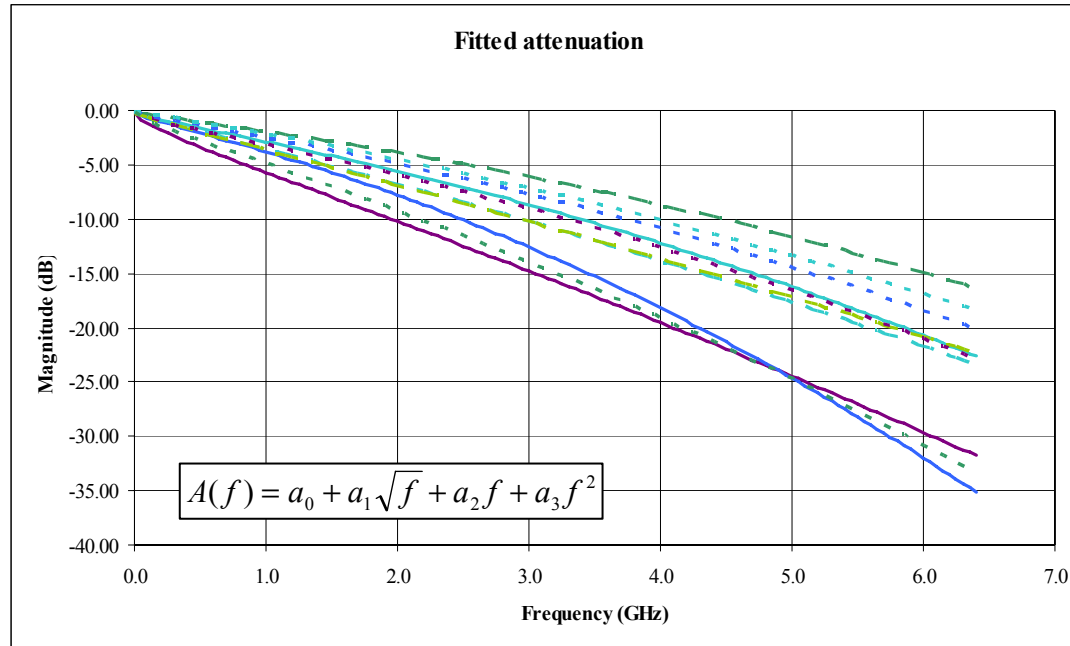
- Epsilon point specifications describe point-to-point links traversing a passive electrical backplane in a modular platform environment
- The Epsilon point differs from the Beta point in that:
 - It considers only fabric topologies (not arbitrated loop)
 - It has more aggressive performance targets (links span longer distances, include more connectors, higher density, e.g. higher loss and crosstalk)
 - Blade server versus JBOD and RAID
- It is desirable to leverage IEEE 802.3ap™-2007 (Backplane Ethernet) and OIF Common Electrical Interface
 - However, these are serdes (Alpha point) specifications
 - Work is required to project the methodologies and requirements to Epsilon point

Epsilon Point Reference Model



- Links spans up to 33” of differential trace on FR-4 printed circuit boards with up to three connectors [1]
 - It is an objective to support up to 20 dB of loss, at 4.25 GHz, between ϵ_T and ϵ_R [2]
- Interoperability points are the separable connectors closest to the serdes
 - A variety of connectors are currently employed at the mezzanine card and backplane interfaces, so a specific connector is not defined
- The link is assumed to be AC-coupled (may be implemented in the serdes, or on the mezzanine/switch card)

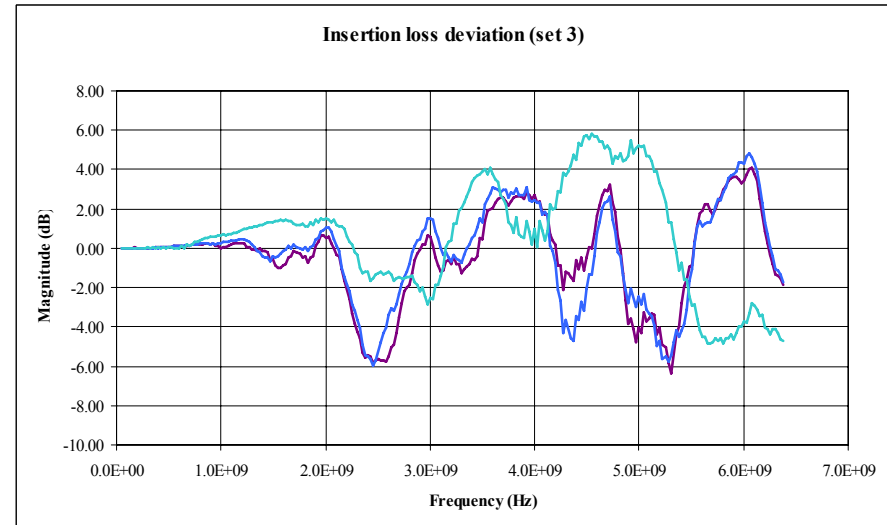
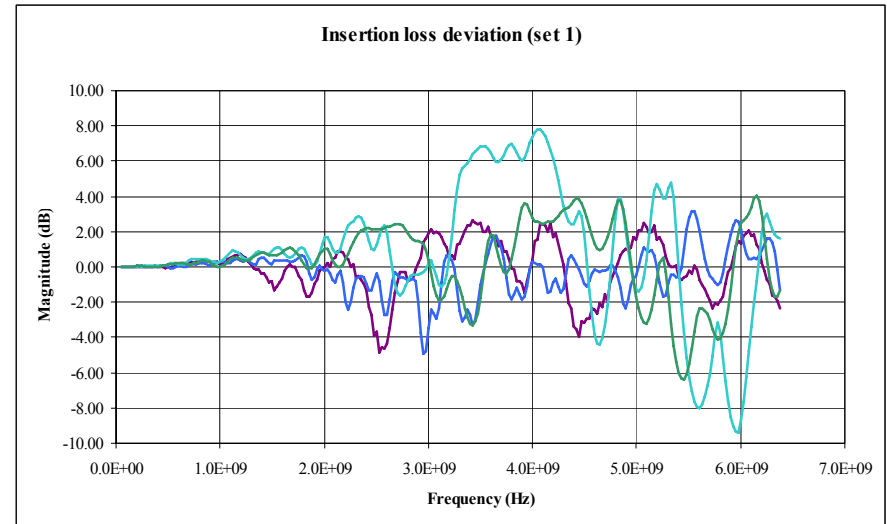
Channel considerations – fitted attenuation



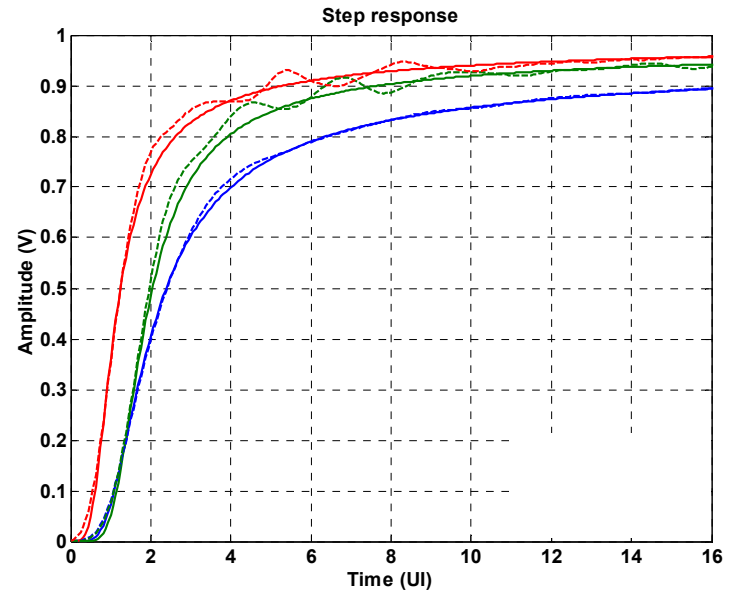
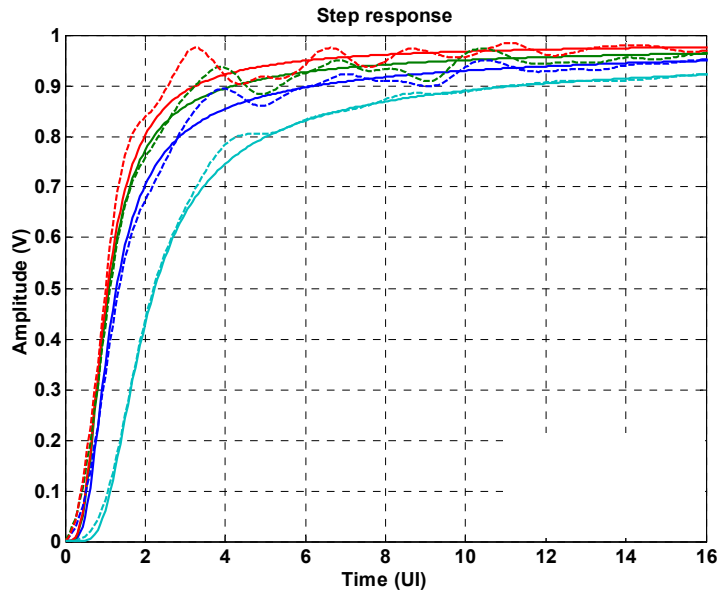
- The fitted attenuation, $A(f)$, is the least mean squares fit of the insertion loss, expressed in dB, to a polynomial function
- The fit is limited to the frequency range DC to 6.375 GHz

Channel considerations – insertion loss deviation

- Insertion loss deviation (ILD) is the error relative to the polynomial fit
- ILD corresponds to tail ripple in the channel impulse response
- The terminations presented by the transmitter and receiver devices will modify ILD

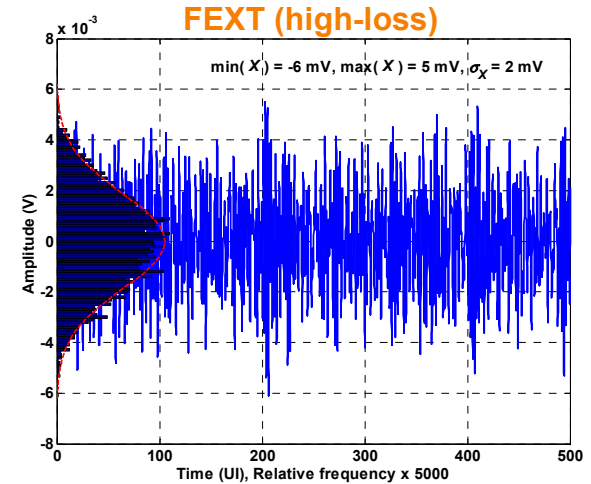
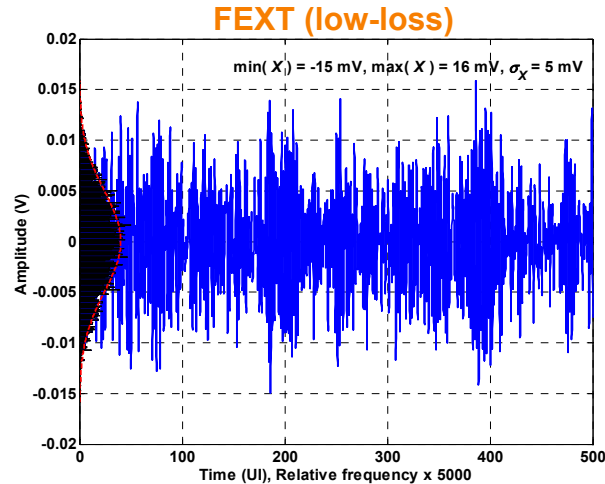
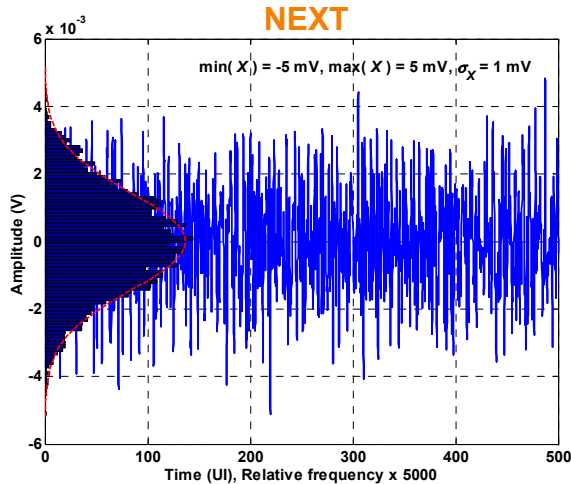


Channel considerations – step response



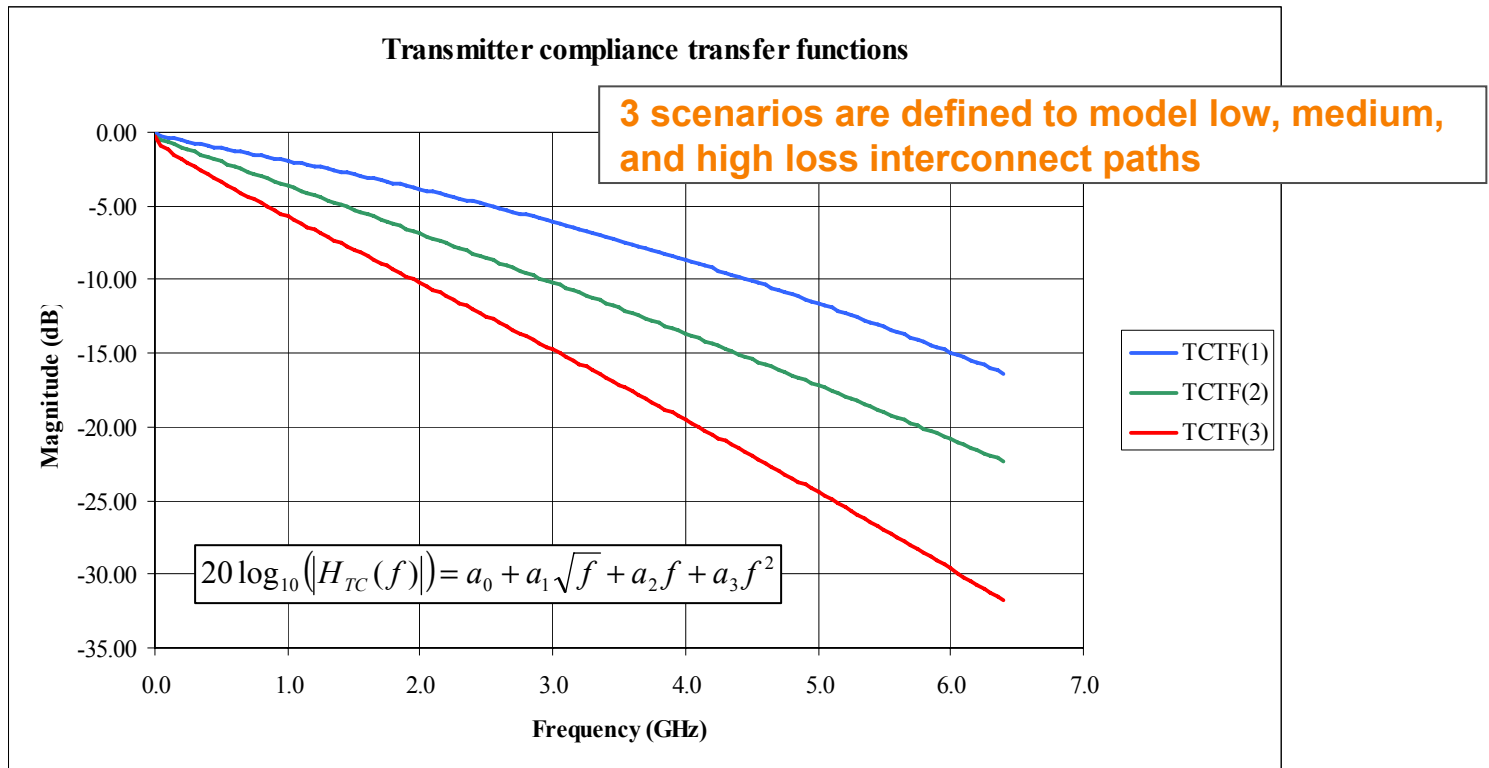
- Comparison between the step response generated from the fitted attenuation and the original step response illustrates the impact of ILD
- Much of ripple in the step response can not be compensated by the reference receiver, e.g. more than 3 UI away
- Such ripple is “anecdotal” in nature, e.g. variation in the path delay alters the arrival time of reflections and impacts the performance
- Stressors will be based on the fitted attenuation and the impact of ILD will be rendered as a term in the loss budget

Channel considerations – crosstalk



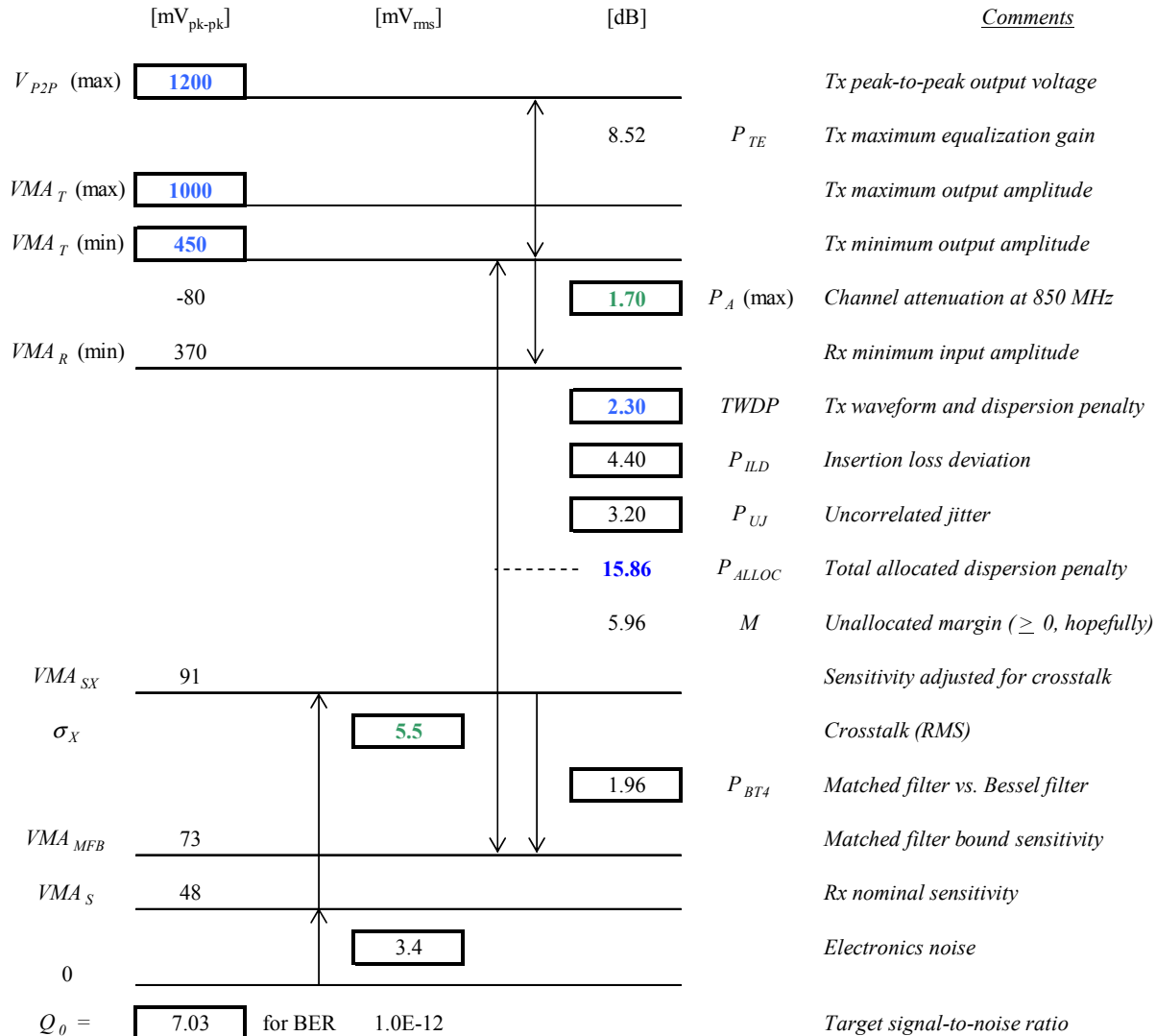
- Test pattern is JSPAT with $VMA_T = 960 \text{ mV}$ and $T_{r,f} = 40 \text{ ps}$ (20-80%)
- Amplitude histograms indicate that the crosstalk amplitude may be reasonably assumed to have Gaussian statistics
 - Truncated of course, with crest factor varying per the aggressor being studied
- It can also be shown that ARBff is only weakly correlated to JSPAT, and that JSPAT itself is “relatively white”
- Observations validate the inclusion of crosstalk as an additive white Gaussian noise term in the TWDP analysis

Transmitter compliance transfer functions



	Units	TCTF index		
		1	2	3
a_3	dB/GHz ²	-0.19	-0.06	-0.14
a_2	dB/GHz	-1.09	-2.91	-3.16
a_1	dB/root-GHz	-0.62	-0.42	-2.22
a_0	dB	-0.04	-0.23	-0.20

Scenario 1 – Low loss channel: Loss budget

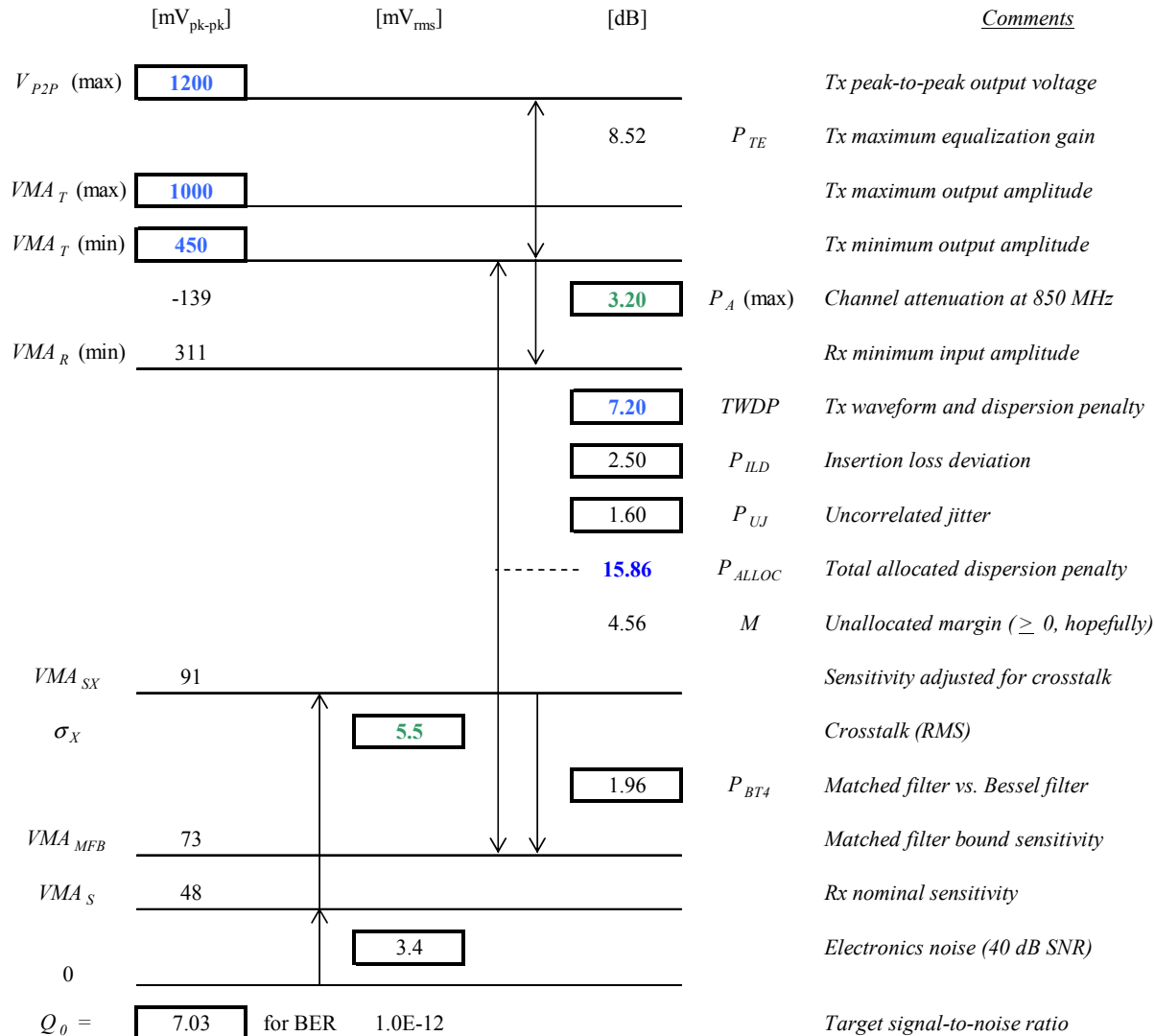


Scenario 1 – Low loss channel: Jitter budget

		[mUI]					
	NC-DDJ (pk-pk)	BUJ (pk-pk)	RJ (pk-pk)	UJ (RMS)	TJ (pk-pk)	<u>Comments</u>	
ϵ_T		35	140	10	20	<i>Tx output jitter</i>	
	130					<i>Tx waveform and dispersion</i>	
	260					<i>Insertion loss deviation</i>	
				15		<i>Crosstalk</i>	
ϵ_R		200	140	10		<i>Rx clock and data recovery</i>	
Total	390	235	288	20	913	<i>Total jitter (≤ 1 UI, hopefully)</i>	
					969	<i>What if RJ = UJ (e.g. BUJ = 0)?</i>	

NOTE – for link analysis purposes only, not intended to populate FC-PI-4 jitter output or tolerance tables

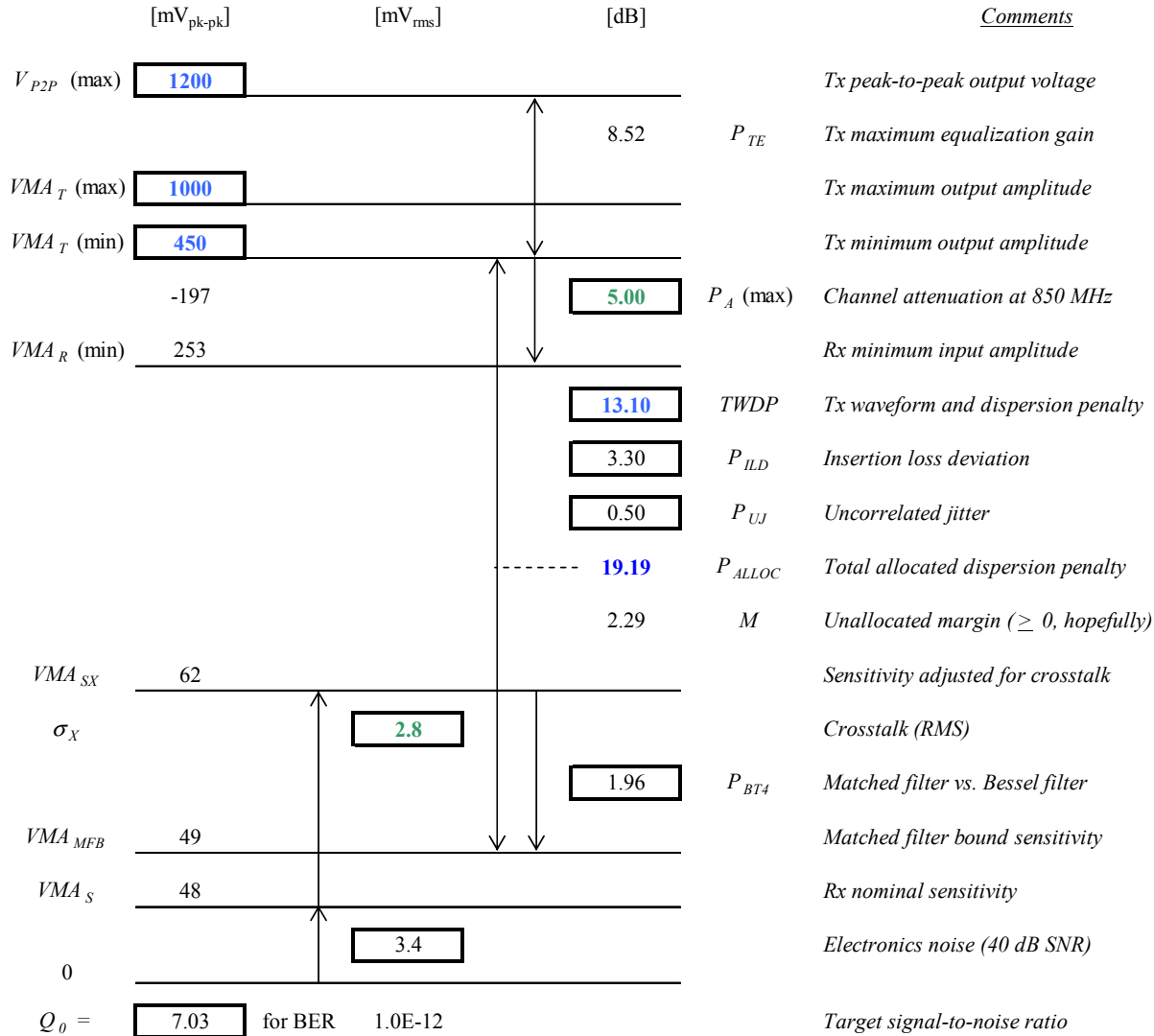
Scenario 2 – Medium loss channel: Loss budget



Scenario 2 – Medium loss channel: Jitter budget

		[mUI]					
	NC-DDJ (pk-pk)	BUJ (pk-pk)	RJ (pk-pk)	UJ (RMS)	TJ (pk-pk)	<u>Comments</u>	
\mathcal{E}_T		35	140	10	20	<i>Tx output jitter</i>	
	180					<i>Tx waveform and dispersion</i>	
	180					<i>Insertion loss deviation</i>	
				18		<i>Crosstalk</i>	
\mathcal{E}_R		200	140	10		<i>Rx clock and data recovery</i>	
Total	360	235	318	23	913	<i>Total jitter (≤ 1 UI, hopefully)</i>	
					962	<i>What if RJ = UJ (e.g. BUJ = 0)?</i>	

Scenario 3 – High loss channel: Loss budget



Scenario 3 – High loss channel: Jitter budget

		[mUI]					
	NC-DDJ (pk-pk)	BUJ (pk-pk)	RJ (pk-pk)	UJ (RMS)	TJ (pk-pk)	<u>Comments</u>	
\mathcal{E}_T		35	140	10	20	<i>Tx output jitter</i>	
	230					<i>Tx waveform and dispersion</i>	
	120					<i>Insertion loss deviation</i>	
				11		<i>Crosstalk</i>	
\mathcal{E}_R		200	140	10		<i>Rx clock and data recovery</i>	
Total	350	235	252	18		837 <i>Total jitter (≤ 1 UI, hopefully)</i>	
					902	<i>What if RJ = UJ (e.g. BUJ = 0)?</i>	

Modifications to the TWDP methodology

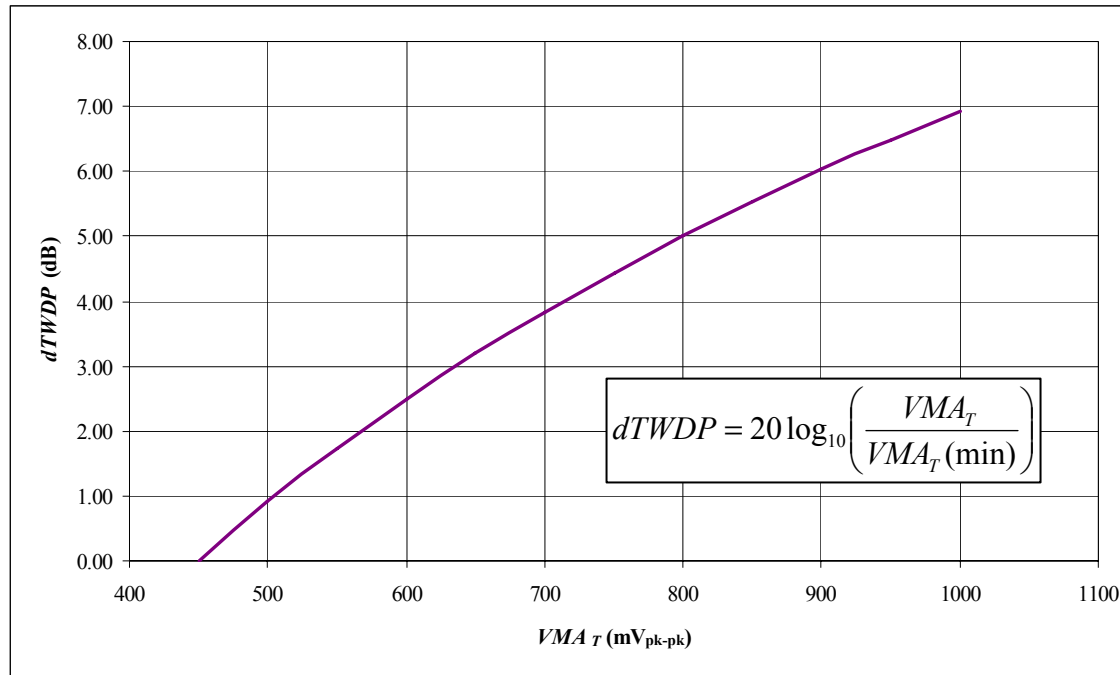
- Enhancements introduced in T11/07-344v0, e.g. spectral line timing recovery and horizontal eye opening evaluation (NC-DDJ) [3]
- Electrical stressors described by the transmitter compliance transfer functions
- Assignment of an independent TWDP limit for each stressor
- Assignment of an independent P_{ALLOC} value for each stressor
- Adjustment of P_{ALLOC} based on the calculated VMA
- Electrical signals vs. optical signals, e.g. dB calculated as $20 \log_{10}(x)$ as opposed to $10 \log_{10}(x)$
- Anti-aliasing filter bandwidth scaled to 75% of the signaling speed in contrast to the static 7.5 GHz bandwidth in the current version
- It is expected that transmitter emphasis (pre-cursor and post-cursor) will be necessary to satisfy the requirements
 - For each stressor, the corresponding TWDP limit shall be satisfied for at least one equalization setting of the transmitter device under test

Epsilon T – signal requirements

- Section 9.6, add Table XX - Signal requirements at Epsilon T for 800-DF-EA-S variants

		Units	TCTF index		
			1	2	3
Peak-to-peak differential output voltage	Max	mV	1200		
VMA (note 1)	Max	mV	1000		
	Min	mV	450		
UJ, RMS (note 2)	Max	UI	0.020		
P _{ALLOC} (note 3)	–	dB	15.9	15.9	19.2
TWDP (note 3)	Max	dB	2.3	7.2	13.1
NC-DDJ (note 3)	Max	UI	0.130	0.180	0.230
Notes:					
1 Voltage modulation amplitude is measured using the procedure described in annex A.x.					
2 Uncorrelated jitter is measured using the procedure described in annex A.y.					
3 TWDP and NC-DDJ are measured using the procedure described in annex A.z and defined using a reference receiver with 1 feed-forward and 3 feedback taps.					

Trade-off between TWDP and VMA_T



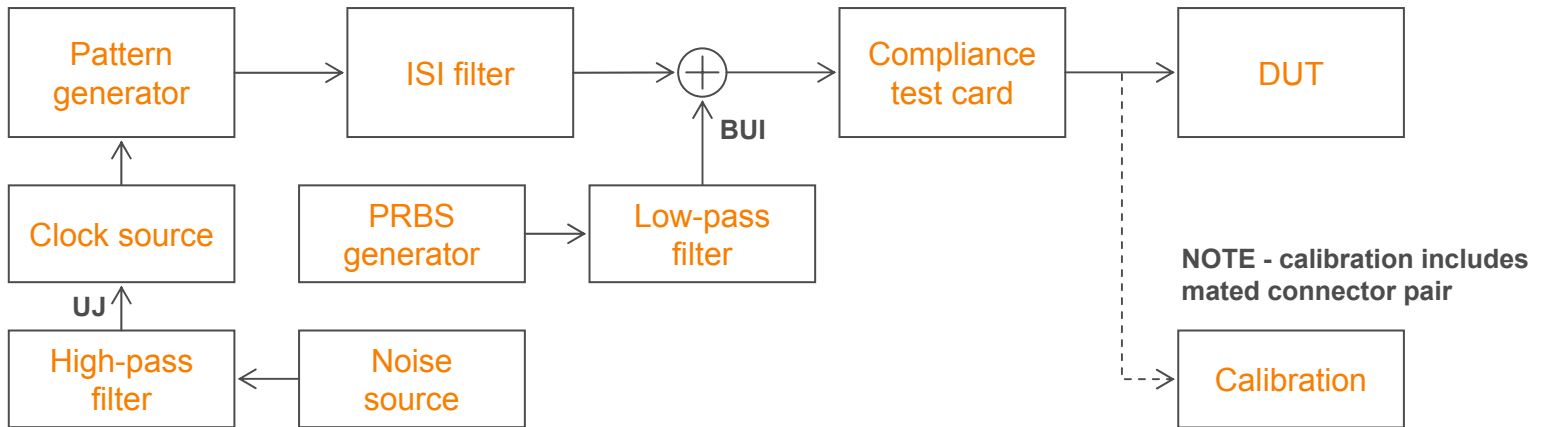
- Since the noise environment is not a function of VMA_T , VMA_T in excess of the minimum results in a larger P_{ALLOC}
 - An increase in P_{ALLOC} implies an increase in the permissible TWDP
- Given the measured (estimated) VMA_T , P_{ALLOC} may be adjusted in the TWDP test script, and the TWDP result compared to a limit adjusted by the function shown above

Epsilon R – jitter tracking

- Section 9.4.1, modify table 30 as shown...

	Units	...	800-DF-EA-S	
Epsilon R Point				
Rx jitter tracking test, VMA (note 6)	Max	mV	...	250
Rx jitter tracking test, jitter freq. and pk-pk amplitude (note 6)		(kHz, UI)	...	(510, 1) (100, 5)

Epsilon R – signal tolerance



- The ISI filter shall be constructed in such a way that it accurately represents the insertion loss and group delay characteristics of differential traces on an FR-4 printed circuit board
- The objective of bounded uncorrelated interference (BUI) is to emulate the truncated Gaussian amplitude distribution observed from crosstalk analysis
- Block diagram intended for illustrative purposes and other implementations possible

Interference generation

- Amplitude impairment that is analogous to bounded uncorrelated jitter
- The PRBS generator should use a polynomial between 7 and 11
- Signaling speed of the PRBS generator should be between 1/10 to 1/3 of the signaling speed of the DUT
- A first order low pass filter is used to filter the PRBS sequence
- The filter should have a bandwidth between 1/20 to 1/10 of the PRBS signaling speed

Epsilon R – signal tolerance requirements

- Section 9.6, add Table YY - Signal requirements at Epsilon R for 800-DF-EA-S variants

		Units	Test index		
			1	2	3
VMA (note 1)	Max	mV	370	310	250
UJ (note 2)	RMS	UI	0.020		
BUI (note 3)	RMS	mV	13.1	11.7	6.9
P _{ALLOC} (note 4)	–	dB	15.9	15.9	19.2
WDP (note 4)	Min	dB	2.3	7.2	13.1
NC-DDJ (note 4)	Max	UI	0.130	0.180	0.230

Notes:

1 Voltage modulation amplitude is measured at the input to the receiver device under test using the procedure defined in annex A.x.

2 Uncorrelated jitter is measured at the input to the ISI filter using the procedure defined in annex A.y.

3 Bounded uncorrated interference is applied at the receiver device input per the signal tolerance procedure defined in annex A.z.

4 WDP and NC-DDJ are measured using the procedure described in annex A.z and defined using a reference receiver with 1 feed-forward and 3 feedback taps.

Conclusions

- Loss and jitter budgets close for each scenario with significant margin
 - Budgets linked through P_{UJ} and “enhanced” TWDP via NC-DDJ
- A portion of this margin will be consumed by the enhancement of ILD caused by the imperfect terminations presented by the transmitter and receiver devices
 - An effect not explicitly included in this study due to time constraints

Future work

- Channel requirements not included, but implied by the TCTF, following the example provided by legacy Beta point specifications
 - However, guidelines on how to verify that a channel has P_{ILD} within the link budget, insertion loss vs. crosstalk trade-offs, etc. may be useful
- This proposal provides a framework that may be leveraged for Beta and Delta point (e.g. SFP+ direct attach copper) specifications
 - In fact, Beta point requirements may be based on Epsilon omitting the high-loss scenario 3
- Fine tuning of parameters will be required in August after additional study

References

1. Koenen, “Channel Model Requirements for Ethernet Backplanes in Blade Servers”, May 2004
http://ieee802.org/3/ap/public/may04/koenen_01_0504.pdf
2. Wallace et al., “Epsilon Point Document”, T11/07-312v1, April 2007
3. Healey and Marlett, “Enhancing WDP”, T11/07-344v0, April 2007