## Overview of OIF CEI T10/05-200r0

Mike Lerer<br>Chairman Optical Internetworking Forum<br>Physical Link Layer Working Group

Chief Architect
Rapid Prototypes Inc mlerer@fpga.com

## CEI Reference Model

- Two CEI Links (Ingress and Egress)

Figure 1-6.Reference Model


## CEI-6G Specifications

- Baud Rate 4.976 to 6.375 Gigabaud/second
- NRZ Differential Signaling
- Nominal Impedance 100 Ohm
- Supports Hot Plug
- AC coupling Required
- assumed part of receiver
- DC Coupling Optional
- BER 10-15


## CEI-6G Specifications

- CEI-6G-SR Short Reach
- 0 to 200 mm PCB and up to 1 connector
- Transmitter
- 1 Tap Transmit Emphasis
- T_Vdiff 400 mVppd minimum 750 mVppd maximum
- Receiver
- No equalization
- R_Vdiff 125 mVppd minimum 750 mVppd maximum
- CEI-6G-LR Long Reach
- 0 to $1,000 \mathrm{~mm}$ PCB and up to 2 connectors
- Transmitter
- 1 Tap Transmit Emphasis
- T_Vdiff 800 mVppd minimum 1200 mVppd maximum
- Receiver
- 5 Tap Decision Feedback Equalization or better
- R_Vdiff 1200 mVppd maximum


## CEI-11G Specifications

- Baud Rate 9.95 to 11.1 Gigabaud/second
- NRZ Differential Signaling
- Nominal Impedance 100 Ohm
- Supports Hot Plug
- AC coupling Required
- assumed part of receiver
- DC Coupling Optional
- BER 10-15


## CEI-11G Specifications

- CEI-11G-SR Short Reach
- 0 to 200 mm PCB and up to 1 connector
- Transmitter
- No Transmit Emphasis
- T_Vdiff 360 mVppd minimum and 770 mVppd maximum
- Receiver
- No equalization
- R_Vdiff 110 mVppd minimum 1050 mVppd maximum
- CEI-11G-MR Medium Reach
- Transmitter
- 2 Tap Transmit Emphasis
- T_Vdiff 800 mV ppd minimum 1200 mVppd maximum
- Receiver
- No equalization
- R_Vdiff 110 mVppd minimum 1200 mVppd maximum
- CEI-11G-LR Long Reach
- $\quad 0$ to $1,000 \mathrm{~mm}$ PCB and up to 2 connectors
- Transmitter
- 2 Tap Transmit Emphasis
- T_Vdiff 800 mVppd minimum 1200 mVppd maximum
- Receiver
- 5 Tap Decision Feedback Equalization or better
- R_Vdiff

1200 mVppd maximum

## Compliance

- Transmitter
- Must meet Tx Mask Sets.
- Channel
- S parameters of Channel must demonstrate performance with a simulated worst case Transmitter and Receiver.
- Receiver
- Must operate with any compliant Transmitter and Channel.


## 6G SR Channel Compliance

## Reference Transmitter:

1. A single post tap transmitter, with $\leq 3 \mathrm{~dB}$ of emphasis and infinite precision accuracy.
2. A transmit amplitude of 400 mV ppd
3. Additional Uncorrelated Bounded High Probability Jitter of 0.15Ulpp (emulating part of the Tx jitter)
4. Additional Uncorrelated Unbounded Gaussian Jitter of 0.15Ulpp (emulating part of the Tx jitter)
5. A Tx edge rate filter: simple $20 \mathrm{~dB} / \mathrm{dec}$ low pass at $75 \%$ of baud rate, this is to emulate a $\mathrm{Tx}-3 \mathrm{~dB}$ bandwidth at $3 / 4$ baud rate at the maximum baud rate that the channel is to operate at or $6.375 \mathrm{Gsym} / \mathrm{s}$ which ever is the lowest.
6. Worst case transmitter return loss described as a parallel $R C$ elements, $\mathrm{A} 0=-8 \mathrm{~dB}, \mathrm{~F} 0=100 \mathrm{Mhz}, \mathrm{F} 1=\mathrm{T} \_$Baud $\mathrm{x} 3 / 4, \mathrm{~F} 2=\mathrm{T} \_$Baud, Slope $=16.6 \mathrm{~dB} /$ decade

## Reference Receiver:

1. No Rx equalization and the Rx bandwidth is assumed to be infinite.
2. Worst case receiver return loss described as a parallel $R C$ elements,
 $\mathrm{A} 0=-8 \mathrm{~dB}, \mathrm{~F} 0=100 \mathrm{Mhz}, \mathrm{F} 1=$ R_Baud $\mathrm{x} 3 / 4, \mathrm{~F} 2=$ R_Baud, Slope $=16.6 \mathrm{~dB} /$ decade
3. A BER of $10^{-15}$
4. A sampling point defined at the midpoint between the average zero crossings of the differential signal

## 6G LR Channel Compliance

## Reference Transmitter:

1. A single post tap transmitter, with $\leq 6 \mathbf{d B}$ of emphasis and infinite precision accuracy.
2. A transmit amplitude of 800 mVppd
3. Additional Uncorrelated Bounded High Probability Jitter of 0.15Ulpp (emulating part of the Tx jitter)
4. Additional Uncorrelated Unbounded Gaussian Jitter of 0.15Ulpp (emulating part of the Tx jitter)
5. A Tx edge rate filter: simple $40 \mathrm{~dB} / \mathrm{dec}$ low pass at $75 \%$ of baud rate, this is to emulate both $T x$ and $R x-3 \mathrm{~dB}$ bandwidth at $3 / 4$ baud rate at the maximum baud rate that the channel is to operate at or $6.375 \mathrm{Gsym} / \mathrm{s}$ which ever is the lowest.
6. Worst case transmitter return loss described as a parallel $R C$ elements,
$\mathrm{A} 0=-8 \mathrm{~dB}, F 0=100 \mathrm{Mhz}, \mathrm{F} 1=\mathrm{T} \_$Baud $\mathrm{x} 3 / 4, F 2=\mathrm{T} \_$Baud, Slope $=16.6 \mathrm{~dB} /$ decade

## Reference Receiver:

1. Rx equalization: 5 tap DFE, with infinite precision accuracy and having the following restriction on the coefficient values:
Let W[N] be sum of DFE tap coefficient weights from taps $N$ through $M$ where
$N=1$ is previous decision (i.e. first tap) $M=$ oldest decision (i.e. last tap)
R_Y2 = T_Y2 $=400 \mathrm{mV}$
Y = min(R_X1, (R_Y2 - R_Y1) / R_Y2) $=0.30$
$Z=2 / 3=\overline{0} .66667$
Then $W[N] \leq Y * Z(N-1)$
For the channel compliance model the number of DFE taps $(M)=5$. This gives the following maximum coefficient weights for the taps:
$W[1] \leq 0.2625$ (sum of taps 1 to 5)
W[2] $\leq 0.1750$ (sum of taps 2 to 5)
$W[3] \leq 0.1167$ (sum of taps 3 to 5 )
$W[4] \leq 0.0778$ (sum of taps 4 and 5)
$W[5] \leq 0.0519(\operatorname{tap} 5)$
Notes:

- These coefficient weights are absolute assuming a T_Vdiff of 1 Vppd
- For a real receiver the restrictions on tap coefficients would apply for the actual number of DFE taps implemented (M)

2. Worst case receiver return loss described as a parallel RC elements,
 A0 $=-8 \mathrm{~dB}, \mathrm{~F} 0=100 \mathrm{Mhz}, \mathrm{F} 1=$ R_Baud $\mathrm{x} / 3 / \mathrm{F} 2=$ R_Baud, Slope $=16.6 \mathrm{~dB} /$ decade
3. A BER of $10^{-15}$

## 11G SR Channel Compliance

## Reference Transmitter:

1. A transmitter with no emphasis
2. A transmit amplitude of both 360 mVppd and 770 mVppd
3. Additional Uncorrelated Bounded High Probability Jitter of 0.15 Ulpp (emulating part of the Tx jitter)
4. Additional Uncorrelated Unbounded Gaussian Jitter of 0.15Ulpp (emulating part of the Tx jitter)
5. At the maximum baud rate that the channel is to operate at or $11.1 \mathrm{Gsym} / \mathrm{s}$ which ever is the lowest.
6. A Tx edge rate filter: simple $20 \mathrm{~dB} / \mathrm{dec}$ low pass at $75 \%$ of baud rate, this is to emulate a $T \mathrm{x}-3 \mathrm{~dB}$ bandwidth at $3 / 4$ baud rate.
7. Worst case transmitter return loss described as a parallel $R C$ elements,

$$
\begin{aligned}
& \mathrm{A} 0=-8 \mathrm{~dB}, \mathrm{~F} 0=100 \mathrm{Mhz}, \mathrm{~F} 1=\mathrm{T} \_ \text {Baud } \mathrm{x} 3 / 4, \mathrm{~F} 2=\text { T_Baud } \times 3 / 2 \text {, } \\
& \text { Slope }=16.6 \mathrm{~dB} / \text { decade }
\end{aligned}
$$

## Reference Receiver A:

1. No Rx equalization and the Rx bandwidth is assumed to be infinite.

2. Worst case receiver return loss described as a parallel $R C$ elements,

A0 $=-8 \mathrm{~dB}, F 0=100 \mathrm{Mhz}, \mathrm{F} 1=$ R_Baud $\mathrm{x} 3 / 4, F 2=$ R_Baud $x 3 / 2$, Slope $=16.6 \mathrm{~dB} /$ decade
3. A BER of $10^{-15}$
4. A wander divider equal to 10
5. A sampling point defined at the midpoint between the average zero crossings of the differential signal Reference Receiver B (Jitter Transparent XFP/XFI):

1. A receiver with a single zero single pole filter (as per Annex 2.B.8) and the Rx bandwidth is assumed to be infinite.
2. Worst case receiver return loss described as a parallel $R C$ elements,

A0 $=-8 \mathrm{~dB}, \mathrm{~F} 0=100 \mathrm{Mhz}, \mathrm{F} 1=$ R_Baud $\mathrm{x} 3 / 4, \mathrm{~F} 2=$ R_Baud $x 3 / 2$, Slope $=16.6 \mathrm{~dB} /$ decade
3. A BER constained by the optical specification
4. A wander divider equal to 10
5. A sampling point defined at the midpoint between the average zero crossings of the differential signal

## 11G LR Channel Compliance

## Reference Transmitter:

1. Maximum Transmit Pulse, as per 2.D.7, of T_Vdiff min. of Table 9-1
2. A TX edge rate filter simple $40 \mathrm{~dB} / \mathrm{dec}$ low pass at $75 \%$ of Baud Rate
3. Effective Driver UUGJ, UHBHPJ and DCD as in Table 9-3
4. Equalizing Filter with 2 tap baud spaced emphasis no greater than a total of 6 dB with finite resolution no better than 1.5 dB .
5. Worst case Transmitter return loss described as a parallel RC element,

A0 $=-8 \mathrm{~dB}, \mathrm{FO}=100 \mathrm{Mhz}, \mathrm{F} 1=$ T_Baud x 3 3 4, F2 $=$ T_Baud, Slope $=$ $16.6 \mathrm{~dB} /$ decade
6. Maximum baud rate that the channel is to operate at or $11.1 \mathrm{Gsym} / \mathrm{sec}$ whichever is the lowest,


## 11G LR Channel Compliance

Reference Receiver A:1.
4-tap baud spaced Non-Linear Discrete Inverse Channel Filter (DFE), with infinite precision accuracy and having the following restrictions: Let $W[N]$ be sum of DFE tap coefficient weights from taps $N$ through $M$ where
$\mathrm{N}=1$ is previous decision (i.e. first tap)
M = 4
R_Y2 $=\mathrm{T}_{\text {_ }} \mathrm{Y} 2=400 \mathrm{mV}$
$\mathrm{Y}^{-}=\min \left(\mathrm{R}_{-}^{-} \mathrm{X} 1,\left(\mathrm{R}_{-} \mathrm{Y} 2-\mathrm{R}_{-} \mathrm{Y} 1\right) / \mathrm{R}_{-} \mathrm{Y} 2\right)=0.2625$
$\mathrm{Z}=2 / 3=0.66667$
Then $W[N] \leq Y * Z(N-1)$
For the channel compliance model the number of DFE taps $(M)=4$. This gives the
following maximum coefficient weights for the taps:
$\mathrm{W}[1] \leq 0.2625$ (sum of absolute value of taps 1 and2)
$W[2] \leq 0.1750$ (sum of absolute value of taps 2,3 and 4 )
$\mathrm{W}[3] \leq 0.1167$ (sum of absolute value of taps 3 and 4 )
$\mathrm{W}[4] \leq 0.0778$ (sum of absolute value of tap 4)
Notes:


- These coefficient weights are absolute assuming a $T_{-}$Vdiff of 1 Vppd
- For a real receiver the restrictions on tap coefficients would apply for the actual number of DFE taps implemented (M)

2. Worst case receiver return loss described as a parallel $R C$ elements,
A0 $=-8 \mathrm{~dB}$, F0 $=100 \mathrm{Mhz}, \mathrm{F} 1=$ R_Baud $\mathrm{x} 3 / 4$, F2 $=$ R_Baud, Slope $=16.6 \mathrm{~dB} /$ decade
A BER of $10^{-15}$

## Reference Receiver B:

1. A continuous-time equalizer with 3 zeros and 3 poles in the region of baudrate/100 to baudrate. Additional parasitic zeros or poles must be considered part of the receiver vendor's device and be dealt with as they are for reference receiver A. Pole and Zero values have infinite precision accuracy. Maximum required gain/ attenuation shall be less than or equal to 20 dB .
The pole-zero algorithm takes the SDD21 magnitude response for the through channel and inverts it to produce a desired CTE filter response curve.
The input to pole-zero determination shall be the SDD21 magnitude at the following frequencies or nearest calculated frequencies: baudrate/100, baudrate/50, baudrate/20, baudrate/10, baudrate/5, baudrate/3, baudrate/2.
The algorithm is a least square fit of poles and zeros to the inverse of the magnitude of SDD21 at the 7 frequencies see 2.B.7.1.
The pole-zero determination shall be used to calculate the equalized SDD21.
Worst case Receiver return loss described as a parallel RC,

A0 $=-8 \mathrm{~dB}, \mathrm{~F} 0=100 \mathrm{Mhz}, \mathrm{F} 1=$ R_Baud $\mathrm{x} 3 / 4, \mathrm{~F} 2=$ R_Baud, Slope $=16.6 \mathrm{~dB} /$ decade

## Interop Results at 6G

- Altera
- Flextronics
- Molex
- Northrop Grumman
- Tyco Electronics
- Vitesse
- Xilinx

| 6 G Interop Results |  | Silicon Source A | Sticon Source B | Silicon Source C |
| :---: | :---: | :---: | :---: | :---: |
| Backplane F Nelco N4000-13SI | Sticon Target A |  | $21^{\prime \prime}(0.53 \mathrm{~m})$ | $31^{\prime \prime}(0.79 \mathrm{~m})$ |
|  | Sticon Target B | $21^{\prime \prime}(0.53 \mathrm{~m})$ | $21^{\prime \prime}(0.53 \mathrm{~m})$ | $21^{\prime \prime}(0.53 \mathrm{~m})$ |
|  | Silicon Target C | $31^{\prime \prime}(0.79 \mathrm{~m})$ | $21^{\prime \prime}(0.53 \mathrm{~m})$ |  |
| Backplane G Nelco N4000-13SI | Sticon Target A | 49" (1.25 m) | $25^{\prime \prime}(0.63 \mathrm{~m})$ | $\begin{aligned} & \hline 30^{\prime \prime}-49^{\prime \prime} \\ & (0.76 \mathrm{~m}-1.25 \mathrm{~m}) \end{aligned}$ |
|  | Slicon Target B | $25^{\prime \prime}(0.63 \mathrm{~m})$ |  | $\begin{aligned} & 30^{\prime \prime-}-49^{\prime \prime} \\ & (0.76 \mathrm{~m}-1.25 \mathrm{~m}) \end{aligned}$ |
|  | Sticon Target C | $\begin{array}{ll} \hline 30^{\prime \prime}-49^{\prime \prime}(0.76 & \mathrm{m}- \\ 1.25 \mathrm{~m}) & \\ \hline \end{array}$ | $\begin{array}{\|l\|} \hline 30^{\prime \prime}-49^{\prime \prime} \\ (0.76 \mathrm{~m}-1.25 \mathrm{~m}) \end{array}$ |  |
| Backplane H Isola FR408 | Silicon Target A | 39" (1 m) |  | 39 Cl ( m) |
|  | Silicon Target B |  |  | 39" (1 m) |
|  | Silicon Target C | 39" (1 m) | $39^{\prime \prime}(1 \mathrm{~m})$ |  |
| Backplane I Nelco N4000-13 | Silicon Target A |  | $36^{\prime \prime}(0.91 \mathrm{~m})$ |  |
|  | Sticon Target B | $36^{\prime \prime}(0.91 \mathrm{~m})$ |  | $36^{\prime \prime}(0.91 \mathrm{~m})$ |
|  | Sticon Target C |  | $36^{\prime \prime}(0.91 \mathrm{~m})$ |  |
| Backplane J Nelco N4000-6 | Slicon Target A |  | $35^{\prime \prime}(0.89 \mathrm{~m})$ |  |
|  | Stlicon Target B | $35^{\prime \prime}(0.89 \mathrm{~m})$ |  | $35^{\prime \prime}(0.89 \mathrm{~m})$ |
|  | Silicon Target C |  | $35^{\prime \prime}(0.89 \mathrm{~m})$ |  |
| Backplane K <br> Rogers Laminate | Sticon Target A | $\begin{aligned} & 37^{\prime \prime-53^{\prime \prime}} \\ & (0.94 \mathrm{~m}-1.35 \mathrm{~m}) \end{aligned}$ |  |  |
| Backplane L Rogers Laminate SMT comector | Sticon Target A | 53 "(1.35 m) |  | $\begin{array}{\|l\|} \hline 45^{\prime \prime}-53^{\prime \prime} \\ (1.14 \mathrm{~m}-1.35 \mathrm{~m}) \\ \hline \end{array}$ |
|  | Sticon Target C | $\begin{aligned} & 45^{\prime \prime}-53^{\prime \prime}(1.14 \mathrm{~m}- \\ & 1.35 \mathrm{~m}) \end{aligned}$ |  |  |

## Interop Results at 11G

- AMCC
- Flextronics
- Molex
- Northrop Grumman
- Tyco Electronics
- Xilinx.

| 11G Interop Results |  | Mhiron Sorice D | Stligon Soure E |
| :---: | :---: | :---: | :---: |
| Bachplane . II Neloo 400:-135I | Sthou Thred D | 22"(0.6m) | $22^{\prime 2} 31^{10.0 .6 m-0.79 m)}$ |
|  | Sticou Thygt E | $22^{1 \prime} .31^{\prime \prime}(0.56 \mathrm{~m} \cdot 0.79 \mathrm{~m})$ |  |
| Bachplane.. <br> Nelo 4000-135I | Sthou Thred D | 25' $(0.63 \mathrm{~m})$ | $30^{\prime \prime}(0.76 \mathrm{~m})$ ) |
|  | Stiron Target | $30^{\prime \prime}(0.76 \mathrm{~m})$ |  |
| $\begin{array}{\|l} \hline \text { Bacliplane } 0 \\ \text { Isola FRRO8 } \end{array}$ | Slicon Target D | $25^{\prime \prime}(0.63 \mathrm{~m})$ | $30^{\prime \prime}(0.76 \mathrm{~m})$ |
|  | Stion Thyet E | 300400'0.76mm-1.00m) |  |
| Bacliplane P <br> Neloo 4000-135I | Stiron Inyet ${ }^{\text {D }}$ |  | 22"-31 ${ }^{17}(0.56 \mathrm{~mm}-0.79 \mathrm{~m})$ |
|  | Sthou Thugt E | $22^{\prime \prime} .31^{\prime \prime}(0.56 \mathrm{~m} \cdot 0.79 \mathrm{~m})$ |  |
| $\begin{array}{\|l\|} \hline \text { Bacliplane Q } \\ \text { Rogers Laninate } \\ \text { Surfice Mour Comector } \end{array}$ | Sthou Thygt D | $33^{\prime \prime}(0.84 \mathrm{~m})$ | $33^{\prime \prime}-45^{\prime \prime}(0.84 \mathrm{~m}-1.14 \mathrm{~m})$ |
|  | Stion Tanget E | $33^{\prime \prime} \cdot 45^{\prime \prime}(0.84 \mathrm{~m} \cdot 1.14 \mathrm{~m})$ |  |

