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Issues with Implementing Transmitter Pre-Compensation

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- Amplitude sensitivity to common-mode voltage.
- Effects on driver Z_{out} and common-mode operating point.
- Feasibility of driving output stages harder.
- Feasibility of larger output stages.
- Slew rate issues.
- Effects on NEXT and FEXT.
- Power dissipation concerns.
- Power efficiency of a boost driver strategy.



- It's difficult to drive more current with existing currentmode drivers
- Simulation circuit for observing differential V_{swing} and \mathbf{I}_{cm}
 - Without terminator, negation swings smaller by 115mV



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V_{swing} versus swept V_{cm}

- LVD V_{swing} for V_{cm} swept from 0V to 3.0V
- Currents are highly variable outside of the allowed common-mode range.



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- LVD I_{cm} for V_{cm} swept from 0V to 3.0V
- Currents are highly variable outside of the allowed common-mode range



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Isues with Implementing Transmitter Pre-compensation

Quantum_M V_{swing} across common mode range

- Usable range (0.855V 1.645V) V_{swing} versus V_{cm}
- Linearity degrades with increasing signal amplitude



I_{cm} across common mode range

- Usable range (0.855V 1.645V) I_{cm} versus V_{cm}
- Linearity degrades with increasing signal amplitude



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Quantum Issues Using Existing Structures

- Differential V_{swing} becomes a strong function of V_{cm} .
- D.C. common-mode current increases (lower Z_{out} for LVD current mode driver).
- Current sources are more problematic.
- Common-mode noise from 3.3V supply increases.
- Turning on and off a "boost driver" will result in common-mode glitches during driver enable and disable.
- Turning on and off a "boost driver" will result in a high frequency common-mode pulses on the bus.

Quantum Issues Using Existing Structures

- Consider a 11001100 data pattern, on a driver with 1.0mA of common-mode mismatch.
- An 80Mhz common-mode signal will be present on the bus, with levels 1.0mA and 1.8mA.
- Common-mode voltage waveform depends on the local common-mode line impedance and on common-mode reflections off of the terminator.



Quantum Issues Using Existing Structures

- A 68 wire cable can have up to 32 wires with identical common mode waveforms.
- Common-mode cross-talk is not helped by twisting wires.
- EM Radiation is a concern.
- At 80MHz a 2 meter cable is an efficient antenna.

• Die area increases

SCSI pads already a large fraction of ASIC die area



- Capacitance would increase for an "off" driver
 - Estimate an increase of 1.2 to 2.5pF to ground on bus- and bus+.
 - Possible problem with 15pF limit in standard for some vendors.
 - Very likely problem with the tighter capacitance limits in some customer purchase specs for most vendors.
 - Backward compatibility problem (Fast-40 or Fast-80) for back-planes which were marginal with current generation drives.
 - More capacitance would invalidate all eye-diagram data taken to date.
- Some back-plane impedance would drop below 85 Ω with added capacitance.

- Chip heating will be greater as average drive power is increased.
- Power delivered to bus increases by the product of the boost factor (1.5, 1.8, ...) and the transition density (100% for a 101010 pattern).
- Larger thermal gradients across die, making line to line timing de-skew less accurate.
- Larger delta temperature between first bits in data transfer and those driven after thermal equilibrium is reached.
- In SCSI targets, LVD power already over half of die power.
- More elaborate thermal management on target PCBs?
- Added power in the pad ring will undermine the chip's timing performance.

- When LVD drivers are enabled on the bus, it takes over a millisecond to reach thermal equilibrium.
- Driver temperature also depends on adjacent heat sources (other enabled drivers).
- The temperature difference between REQ/ACK and Data will change over time.





- CAD tools cannot cope with elements at different temperatures.
- Adding more heat to the pad ring makes timing optimization harder.



- The higher swings must be obtained with the same rise and fall times as in U160 products.
- Higher slew rates result, and will result in increased ringing at the transmitter.
- Higher slew rates will increase the number of stubs which cause problem reflections.
- Currently, any misalignment of pull-up and pull-down pre-drivers leads to a common-mode glitch during a data transition. With a "boost driver", there are 4 predrivers to align instead of the current 2 pre-drivers.
- Sensitivity of common mode transition noise to the ASIC chip package and board mismatches (between bus+ and bus-) will increase.

- Near End Cross-Talk (NEXT) will increase due to the greater ∂i / ∂t on the driven wire pairs.
- Far End Cross-Talk (FEXT) will increase due to the larger voltage swings being driven.
- Ratio of coupled cross talk signal to quiescent signal will increase by the boost ratio.
- Increased intra-chip coupling through power and ground rails from non-constant current driver.

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- Worst case buses have substantial series resistance.
- Net load R is 58 Ω .
- Adding 1.0mA to driver, adds 58mV to driver (cross-talk source)
- Adding 1.0mA to driver adds only 41mV at far terminator.
- Adding energy at the transmitter is inefficient.



Quantum Summary of Circuit Design Issues

- Ourrent source non-linearity versus drive current.
- 2 Added common mode signals and noise.
- **B** EM radiation issues.
- 4 Limits for cables with substantial in-phase common mode signal.
- **5** Additional capacitance needed.
- Over increases resulting in increases in local junction temperatures.
- Temperature profile issues relative to timing budget.
- Optimal transmitter pre-comp drive levels not yet determined.
- **9** No proposals yet for transmitter pre-comp algorithms.

- A transmitter pre-comp design which helps ISI without causing significant new problems is not trivial.
- 2 The high multipliers (1.5x 1.8x) are a major departure from existing LVD technology, and add a lot of risk to U320.
- Side effects of high ratio transmitter pre-comp will cause problems with backward compatibility and multi-vendor interoperability.
- **4** We should consider other alternatives.